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**SHORT CIRCUIT STUDY
PROTECTIVE DEVICE COORDINATION STUDY
ARC FLASH HAZARD ANALYSIS
FOR
PORTLAND STATE UNIVERSITY
NON-WEST CAMPUS LOOP
PORTLAND, OR**

FEBRUARY 2013

1.0	EXECUTIVE SUMMARY	1-1
1.1	Objectives.....	1-1
1.2	Results	1-2
1.3	Recommendations.....	1-5
2.0	SHORT-CIRCUIT ANALYSIS.....	2-1
2.1	Short-Circuit Objectives.....	2-4
2.2	System Modeling.....	2-4
2.3	Short-Circuit Results.....	2-7
2.4	Equipment Evaluation.....	2-7
3.0	PROTECTIVE DEVICE COORDINATION STUDY	3-1
3.1	General Description and Protection Philosophy	3-1
3.2	Codes and Standards.....	3-2
3.3	Coordination Objectives	3-3
3.4	Coordination Results	3-3
3.5	Coordination Recommendations	3-4
3.6	Time-Current Characteristic Plots.....	3-4
4.0	RECOMMENDED PROTECTIVE DEVICE SETTINGS	4-1
5.0	ARC FLASH HAZARD ANALYSIS	5-1
5.1	Introduction.....	5-1
5.2	Study Procedure.....	5-2
5.3	Arc Flash Hazard Analysis Results.....	5-4
5.4	Arc Flash Summary Table Heading Descriptions	5-6
5.5	Arc Flash Hazard Analysis Recommendations.....	5-8
A.	APPENDIX A – SHORT-CIRCUIT INPUT REPORT	A-1
B.	APPENDIX B – SHORT-CIRCUIT RESULTS	B-1
C.	APPENDIX C – UTILITY FAULT CURRENT INFORMATION	C-1
D.	APPENDIX D – ONE-LINE DIAGRAMS.....	D-1

1.0 EXECUTIVE SUMMARY

This report contains the results of analysis performed on the electrical distribution system for all buildings not supplied by the West Campus Loop at the Portland State University in Portland, Oregon. The purpose of this study is to evaluate the existing electrical system, as detailed below.

The executive summary contains the description and guide to the rest of the report. In addition, it also contains the recommendations of the entire study.

1.1 Objectives

1. Short-Circuit Study

Perform a short-circuit study on buildings not included in the existing electrical distribution system shown in order to determine the available fault current at pertinent locations throughout the distribution system. The scope of the study includes:

- For most locations, analysis begins at the incoming 12.47 kV utility service and continued to the main service entrance disconnect or disconnects. Exceptions to this statement are noted below.
 - i. For the Fourth Avenue / Engineering Building (EB), analysis began at the primary metered service (12.47 kV) supplying Medium Voltage Switchgear 52-U1 and 52-U2 and continued through the medium voltage distribution system to low voltage substations USB-1, USB-2, USB-3, USB-5, USB-6, and USB-7.
 - ii. For the Market Center Building, analysis began on the secondary side (480 V) of each of the PacifiCorp owned utility transformers and continued downstream to the first disconnect at each service entrance.

The available fault currents determined by the short-circuit study will be used in the coordination and device evaluation analysis.

2. Equipment Evaluation

Evaluate the short-circuit ratings of the service entrance protective devices found at the locations shown listed above.

3. Coordination Study

Review the existing system overcurrent protection and coordination. Where applicable, provide suggestions for improvement.

4. Arc Flash Analysis

Perform an arc flash hazard analysis per NFPA 70E on the electrical distribution system described in item #1 above.

5. Recommendations

Provide specific recommendations for improving the electrical distribution system performance and correcting any deficiencies found by the studies.

1.2 **Results**

1. Short-Circuit Study

Short-circuit currents were calculated for each bus shown on the one-line diagrams in Appendix D.

Utility transformer and source impedance information was provided by Tom Riddle with Portland General Electric (PGE) on 1/10/2013 via email. Information for all PGE utility sources is summarized in Appendix C.

The Market Center Building is not supplied by PGE, but is supplied by PacifiCorp. It was not possible to obtain fault current information from PacifiCorp at the time of this study. To ensure conservative results, an infinite bus was assumed on the primary side (12.47 kV) of utility transformers TX-MCB UTIL-A, TX-MCB UTIL-B and TX-MCB BSMT UTIL. The following values were calculated on the secondary side (480 V) of each transformer based on transformer nameplate information gathered during data collection:

TX-MCB UTIL-A

- Three-phase fault current: 15,826.5 A

TX-MCB UTIL-B

- Three-phase fault current: 16,705.7 A

TX-MCB BSMT UTIL

- Three-phase fault current: 8,018.8 A

Multiple short-circuit scenarios were only necessary when examining fault-current values at the 4th Avenue / Engineering Building, as it is the only building with multiple sources of power. The following short-circuit study cases were evaluated:

- Study Case No. 1 – System supplied from the Urban-Medical utility feed via Medium Voltage Switchgear B-EB-52-U1. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U2 are open.
- Study Case No. 2 – System supplied from the Urban-Gibbs utility feed via Medium Voltage Switchgear B-EB-52-U2. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U1 are open.
- Study Case No. 3 – System supplied from the Emergency Generator via Medium Voltage Switchgear B-EB-52-U3. Tie breakers BK-EB-52-T1 and

BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-U1 and BK-EB-52-U2 are open.

- Study Case No. 4 – System supplied from the Urban-Medical utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U1 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U2 is open.
- Study Case No. 5 – System supplied from the Urban-Gibbs utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U2 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U1 is open. **This is the worst case scenario and the scenario show on the one-line diagram in Appendix D.**

See Section 2, Appendix A and Appendix B for more information.

2. Equipment Evaluation

The Equipment Evaluation is based on the power system worst-case short-circuit current configuration.

The short-circuit ratings of protective devices and other distribution equipment are evaluated in Section 2, Table 2.1.

In summary of Table 2.1, multiple locations failed the equipment evaluation. See Section 2 for more details.

3. Coordination Study

The time-current coordination plots of the protective overcurrent devices are shown in Section 3. In developing the device settings, consideration was given to both isolation of faults, protection of cables, and protection of transformers.

Efforts were made to provide the best coordination possible with existing protective devices. It should be understood that selective coordination between two instantaneous trip units cannot be achieved for fault levels above the instantaneous pickup of the upstream device. There is some overlapping of curves that cannot be avoided.

For all locations except the 4th Avenue / Engineering Building, the system coordination began at first overcurrent protective device upstream of the utility transformer, and continued downstream through the service entrance to the largest overcurrent protective device which is not in series with the utility overcurrent device.

For the 4th Avenue / Engineering Building, the normal side system coordination began at the 12.47 kV utility fault interrupter and continued downstream the Switchboards B-EB-52-U1 and B-EB-52-U2 to the largest feeder breaker in each of the Unit Substations B-EB-USB-1 – B-EB-USB-7. The emergency system coordination began at the 12.47 kV main relay in B-

EB-52-E3 and continued downstream through Switchboards B-EB-52-U1 and B-EB-52-U2 to the largest feeder breaker in each of the Unit Substations B-EB-UB-1 – B-EB-USB-7.

See Section 3 for more information and Section 4 for device settings.

4. Suggested Protective Device Settings

Settings for the protective devices in the Portland State University – Non-West Campus Loop are shown in Section 4.

Each entry references a coordination plot number found in Section 3. The referenced plot illustrates the coordination of the listed device with the relevant “upstream” and “downstream” protective devices. The protective devices listed in Section 4 should be set per the suggested settings.

5. Arc Flash Analysis

Details of the arc flash analysis are shown in Section 5. This arc flash hazard analysis of the Portland State University Non-West Loop Service Entrances in Portland, Oregon required energy and boundary calculations for approximately seventy-seven (77) locations. In summary of Section 5, there are several locations that have incident energy levels that are above 40 cal/cm². According to NFPA 70E-2012, Article 130.7(A), Informational Note 3, greater emphasis must be placed on establishing an electrically safe work condition when working within the limited approach boundary at locations where the incident energy exceeds 40 cal/cm². The greater emphasis is due to additional hazards created from blast pressure associated with a possible arc. See NFPA 70E-2012, Article 120 for details on establishing an electrically safe work condition.

At the request of Portland State University, arc-flash incident energy calculations were performed at an 8’ working distance. This distance is greater than the standard working distances prescribed by IEEE 1584-2002 and are applicable for energized work, including non-contact voltage testing, being performed by a qualified person using a hot-stick. A distance of 8’ was chosen as it is the approximate distance the face and torso of a qualified person would be when using a 6’ hot-stick. To minimize confusion, these values will not be shown on the arc-flash labels.

Please note for this study, the arc flash hazard has been calculated but not the risk. The risk associated with performing energized electrical work will vary based on the work being performed as well as the condition of the equipment and other factors that can be best determined by a qualified person.

See Table 5.1, Table 5.2, and Table 5.3 for a complete arc flash summary. **Note that the incident energy values listed in Table 5.1, Table 5.2, and Table 5.3 are only valid after the recommended protective device settings shown in Section 4 have been implemented.**

1.3 Recommendations

1. Overdutied Equipment

It is recommended that the overdutied equipment listed in Table 2.1 be reviewed for replacement to comply with the short-circuit current ratings required. Before replacement of any equipment, the short-circuit rating of the equipment should be verified. Additionally, the impedance of the conductor between the utility transformer and the service entrance was not available at the time of this study and was therefore not included in this study. As many of these conductors are underground, it would not be possible to verify the length or size of these conductors with on-site data collection. Work should be done in cooperation with PGE to determine the length of the conductors between the utility transformer and the service entrance disconnect before any equipment is replaced. See Section 2 for detailed short-circuit analysis.

2. Low Voltage Equipment Recommendations

The majority of the low voltage equipment on the West Campus loop at Portland State University is very old and appears to have not been tested and maintained over the life of the equipment. It is critical that Portland State University create a plan to inspect and test the low voltage equipment in these buildings, similar to the testing that has occurred in Science Building II, to determine whether the electrical distribution equipment is still operable

- University Honors Program

The type of the largest feeder breaker in low voltage panelboard in the University Honors Program building could not be field verified. The feeder breakers in this panel were not marked with a type. Due to the age of this equipment it is recommended that it be tested to ensure proper operation and verify the breaker type.

- King Albert Building

While performing data collection it was found that the electrical room in the King Albert Building smelled strongly of natural gas. It is recommended that this room be inspected immediately for gas leaks. Due to the presence of natural gas, it was not possible to field verify the breaker type of the feeder breakers in this switchboard. It is recommended that this room be inspected immediately for gas leaks. Additionally, it is recommended that this equipment be tested for proper operation as well as to verify breaker type and settings.

- Stratford Building

The fused disconnect in the Stratford Building was not labeled with an interrupting rating and this rating was not able to be verified during data collection. The interrupting rating is assumed to be 200 kAIC based on the rating of the fuse present.

- Parkway Building

All equipment in the Parkway Building was verified during data collection. When modeling it was not possible to locate a time-current curve for the Thomas & Betts, Type TB main circuit breaker in the service entrance panelboard. It is assumed the trip characteristics of this circuit breaker are similar to those of a Siemens, Type QJH. This assumption only affects the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis. The difficulties in locating a time-current curve for this circuit breaker are due to the age of the device. Additionally, due to the age of this device, it is recommended that it be tested for proper operation and replaced if necessary.

- Simon Benson House

The fuses in fused disconnect F-SBH DISC B-USB were not able to be field verified. It was not possible to open the fused disconnect during data collection. It is assumed the fuses in this F-SBH DISC B-USB were the same as those in fused disconnect F-SBH DISC A-USB. Due to the age of this equipment, it should be inspected to ensure proper operation and during inspection, the fuse should be verified.

- Blackstone

The circuit breaker type of the main circuit breaker in Panelboards B-BLKS L1-USB, B-BLKS L2-USB, B-BLKS L3-USB, B-BLKS L4-USB, and B-BLKS L5-USB could not be field verified. The circuit breaker label did not contain information on the circuit breaker type. It is assumed this circuit breaker is type HQJ2H. This assumption only affects the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis. It is recommended that this equipment be removed from service and inspected for proper operation and to see if the circuit breaker type can be determined.

- Shattuck Hall

The settings of the circuit breakers at Shattuck Hall could not be field verified. The electronic trip units were unresponsive during data collection. It is recommended these circuit breakers be tested to ensure they are properly programmed and a coordination study has been completed. If this study has not been completed, it is further recommended that a study be completed to determine proper settings for these circuit breakers. For the purposes of this study, it was assumed the circuit breakers are programmed at their maximum settings. This assumption only affects the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis.

- East Hall

The size of cables C-EH JUNC-EHA, C-EH JUNC-EH b, and C-EH JUNC-EH C could not be field verified. It is assumed each of these cables is sized at 1

– 3/0 per phase. If any equipment in East Hall is tested in the future, this assumption should be verified.

The fuse in Fused Disconnect B-EH E DISC-USB could not be field verified. It was not possible to open the fused disconnect without de-energizing. It is assumed the interrupting rating of this fused disconnect is 100 kAIC. This is the lowest standard rating for a Cutler-Hammer fused disconnect of this type. During a maintenance outage, the fuse types and interrupting rating of this switch should be verified.

- University Center Building

The breaker type of the largest breaker in the switchboard in the University Center Building could not be field verified. The circuit breaker is very old and does not have a type listed on the nameplate. It is assumed this circuit breaker is a type THJK. Additionally, it is assumed the adjustable thermal magnetic trip in this circuit breaker is at its maximal setting. These assumptions only affect the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis. Due to the age of this circuit breaker, it is recommended that it is tested to ensure proper operation. If found to not properly operate, it should be replaced.

- Ondine (Main Electrical Room)

The circuit breaker type of the main disconnect could not be field verified. The electrician was uncomfortable with opening equipment for data collection purposes due to the age of the equipment and the confusing layout / lack of labeling. The layout and lack of labeling made it difficult to determine the flow of power and which devices were being used as service disconnects. Additionally, there was no evidence that any of the equipment had been tested or maintained recently. It is assumed that the main disconnect circuit breaker type is PA. Additionally, it is assumed that the adjustable thermal magnetic trip in this circuit breaker was at its maximal setting. Based on this assumption, it is further assumed the interrupting rating of low voltage Switchboard B-OND MAIN SWBD-USB is 65 kAIC. It is recommended this equipment is inspected for proper operation and verification of study assumptions. Additionally, it is recommended that the equipment be clearly labeled to help a qualified person understand the flow of power for this equipment.

- Ondine (15th Floor Electrical Room)

The circuit breaker type of the main disconnect could not be field verified. The circuit breaker was very old and the label did not state the circuit breaker type. It is assumed the circuit breaker was a type NN. Additionally, it is assumed that the adjustable thermal magnetic trip unit in this circuit breaker is at its maximum setting.

It was not possible to locate a time-current curve for the Zinsco, Type QFB circuit breaker in this switchboard. It is assumed the trip characteristics of this circuit breaker are similar to those of an Eaton, Type HJD.

These assumptions only affect the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis.

Based on the age of the equipment, it is recommended that all circuit breakers in the Ondine, 15th Floor Electrical Room be tested for proper function. Additionally, it is known that many Zinsco breakers are prone to failure and all Zinsco breakers should be considered for replacement.

- Art Building

Fused Disconnect B-AB DISC-USB in the Art Building was not labeled with an interrupting rating and this rating was not able to be verified during data collection. The interrupting rating is assumed to be 200 kAIC based on the rating of the fuse present.

- Art Building Annex

While performing data collection it was found that disconnect in the electrical room of the Art Building Annex contained multiple fuse types and manufacturers. All fuses in a disconnect should be the same type with the same trip characteristics and all must be the proper type, specified by the manufacturer. This ensures safe operation of the fused disconnect in the event of a fault. It is recommended that a single fuse type and manufacturer be chosen and all fuses replaced to this standard.

Additionally, Fused Disconnect B-AB DISC ANNEX-USB in the Art Building Annex was not labeled with an interrupting rating and this rating was not able to be verified during data collection. The interrupting rating is assumed to be 10 kAIC based on the rating of the fuse present.

- 4th Avenue / Engineering Building

It was found that many feeder breakers in the unit substations at the 4th Avenue / Engineering building had the instantaneous portion of their trip curves set to 'OFF'. Specifically, this was found in Unit Substations:

- i. USB-1
- ii. USB-2
- iii. USB-3
- iv. USB-5
- v. USB-6

All loads supplied by feeder breakers with the instantaneous trip function removed should be inspected to ensure they are properly protected by a local overcurrent device with instantaneous protection. If the equipment is not, the settings for these breakers must be revised to include an instantaneous trip function.

The current rating of bus busway BWY-EB-52-U3-52-U1 and BWY-EB-52-E3-52-U2 could not be verified. It was assumed each bus duct was rated at 1200 A. During a maintenance outage, this assumption should be verified.

- Science & Education Center

The fuse type in Fused Disconnect F-SEC SOUTH DISC 1A could not be verified. Based on fuses found in similar fused disconnects in this building, it is assumed this fuse is a type FLNR. During a maintenance outage, this assumption should be verified. This assumption only affects the time-current curve presented for this location and does not affect the equipment evaluation or arc-flash hazard analysis.

Fused Disconnects B-SEC SOUTH DISC 1S-USB, B-SEC SOUTH DISC 2A-USB, and B-SEC SOUTH DISC 2B-USB were not labeled with an interrupting rating and this rating was not able to be verified during data collection. The interrupting rating is assumed to be 200 kAIC based on the rating of the fuse present. During a maintenance outage, these assumptions should be verified.

- University Place

480 V Electrical Service: Upon inspection, it appears that Low Voltage Switchboard B-UP-A-USB, or the 480 V service in at University Place, has more than six disconnects without a main circuit breaker. This appears to be in violation of NEC Article 230.71, commonly known as the 'six disconnect rule.' It is recommended that this Switchboard be inspected for possible compliance to or exception from Article 230.71 before replacement.

208 V Electrical Service: While performing data collection, it was found that the electrical room housing the 208 V service at University Place is in disrepair. There were multiple holes in the ceiling resulting in leaks and standing water in the electrical room. There was also evidence of rodents. Rodents are known to get into equipment and cause damage by chewing through insulation. This can lead to an arc-flash and major equipment damage, injury to any personnel in the room at the time and a loss of service. The equipment in this room may not have been properly maintained as the last inspection sticker dates from 1992. Additionally, there was a large amount of rust and corrosion present on the equipment. Many of the exits from the section of University Place that houses the electrical equipment were blocked. It is recommended that this equipment be taken out of service for maintenance as well as being inspected for replacement. It is also recommended that the electrical room be repaired and all water issues corrected immediately.

- Academic & Student Rec Center

Based on the as-found settings for circuit breakers in the Academic & Student Rec Center, it appears there may not have been a coordination study performed when this equipment was commissioned. If a study were performed, the settings recommended in that study may not have been

implemented. As currently set, a fault downstream of a feeder breaker may result in a loss of the entire service due to a lack of selectivity between the main circuit breaker and the largest feeder breaker. It is recommended to verify if a study were performed for this equipment and that the settings were properly implemented. If a study has not been performed, it is recommended that the coordination of this system be fully examined and breaker settings be adjusted based on that examination.

- **Market Center Building**

The fuse type on the primary side of PacifiCorp Transformer TX-MCB UTIL-B could not be verified. It is assumed to be the same fuse as on the primary side of PacifiCorp Transformer TX-MCB UTIL-A. If it is possible to obtain information from PacifiCorp, this assumption should be verified.

3. Arc Flash Hazard Analysis

It is recommended the scope of this study be expanded to include a system wide arc flash hazard analysis of all equipment at Portland State University not supplied by the West Campus Loop. The results of the arc flash hazard analysis are used to determine the incident energy, arc flash boundary, and personal protective equipment requirements for each location. The arc flash hazard analysis, for all equipment, is a requirement of NFPA 70E, and is required by OSHA through the general duty clause. Completion of this study will ensure all equipment in the Portland State University Non-West Loop distribution system complies with NFPA 70E guidelines regarding arc flash analysis and labeling. The analysis is performed in conjunction with a short-circuit analysis, and will utilize the existing settings and ratings of the protective devices. If a lack of selectivity is discovered among existing devices during the study, new settings will be recommended and will be used as the basis for the arc flash hazard analysis.

It is recommended these studies be conducted on a per building basis. Buildings with newer electrical equipment and buildings which may not need replacement of electrical equipment should have the studies conducted first. Studies in buildings with older equipment which may require replacement may be conducted later in order to replace the equipment first and not require a follow-up study.

4. Recommended Settings

Adjustable protective device settings should be set according to the settings tables provided in Section 4.

5. Reducing Incident Energy Levels

The calculated incident energy at a particular location is dependent on three main factors: short-circuit current, distance, and time. These three factors directly affect the incident energy in the following manner:

Short-circuit current: The short-circuit current for a given power system is dependent on the system impedance and source fault current, and cannot be easily reduced.

Distance: IEEE Std 1584™-2002 provides a table with typical working distances. Increasing the working distance reduces the amount of incident energy that reaches the worker; however it becomes difficult to perform many work tasks with an increased working distance, therefore, this is not an optimal solution for most cases.

Time: The incident energy decreases when reducing the exposure time of the arc. This exposure time is directly related to the clearing time of the protective device(s) which feed the fault location.

Based on the preceding summary, arc flash mitigation techniques are most effective and feasible when they involve reducing the arc exposure time. In many locations, the setting of the protective device can be adjusted in order to decrease the interrupting time, resulting in a decreased incident energy. However, in this study, settings for protective devices have not been adjusted to reduce incident energy if the chance of nuisance trips within critical circuits is introduced.

The other option involving reducing the arc exposure time is to consider equipment modifications and upgrades. Several solutions include upgrading trip units, installing “maintenance switches”, and using relays with multiple settings groups. Each specific location needs to be analyzed to determine which reduction method is best employed.

6. Testing and Preventative Maintenance

It is recommended that regularly scheduled testing and preventative maintenance be performed to ensure that the electrical distribution equipment continues to perform at an optimum level. Testing should entail primary injection testing of all circuit breakers to verify proper tripping ranges, contact resistance testing, insulation resistance testing and complete switchgear and transformer cleaning and inspection.

7. Periodic Arc Flash Analysis Review

The 2012 edition of NFPA 70E includes several new requirements regarding arc flash hazard analysis. One new requirement found in Article 130 is that an arc flash hazard analysis must be updated:

- Every five years (at minimum)
- When the electrical system is modified or renovated in any way, including renovations, additions, or subtractions to the system

It is recommended that a plan is implemented to schedule a review of the arc flash hazard analysis for the Portland State University Non-West Campus Loop in a period not to exceed five years, and that a review is performed whenever substantial modifications or renovations take place.

2.0 SHORT-CIRCUIT ANALYSIS

The short-circuit study determines the fault currents that flow in the system during various fault conditions. The calculated fault currents are used in the device evaluation and coordination studies. See Appendix A and Appendix B for the computer generated input data and output data. NEC-2011, Article 110.24(A) requires that service entrance equipment is labeled with the following pieces of information:

- Maximum available fault current
- Date on which the fault current was calculated

Article 110.24(B) adds that if there is a modification that may change this fault current value, it must be recalculated. The field marking must be updated to reflect the new value of maximum fault current.

The short-circuit calculations were done using A_FAULT, a computer software package by SKM Systems Analysis. The short-circuit analysis performed by A_FAULT is based on IEEE Std C37.010™-1999, IEEE Std C37.5™-1979, and IEEE Std C37.13™-2008.

Separate “Z” (complex), “X” (reactive), and “R” (resistive) networks are used by A_FAULT for the short-circuit analysis. A_FAULT uses complex network reduction and the relationship E/Z to calculate the fault current magnitude and angle at each faulted bus. The complex equivalent circuit impedance, Z , is calculated by the reduction of the “Z” (complex) network, and is reported as the “EQUIV. IMPEDANCE” in the A_FAULT reports. The X/R ratios calculated for each fault condition are based on the separate reduction of the X and R networks. These X/R ratios are used for the calculation of fault duty multipliers, to evaluate the short-circuit ratings of system components.

A_FAULT is capable of generating three types of short-circuit reports for both balanced (three-phase bolted) and unbalanced (line-to-ground) faults. The reports that are generated depend on the system that is being evaluated.

The three types of short-circuit reports are:

- Fault Report (for low voltage)
- Momentary Duty Report (for medium voltage)
- Interrupting Duty Report (for medium voltage)

1. Fault Report

The fault currents reported in the “Fault Report” are applicable to low voltage devices and components. The fault currents calculated in this report are based on the contribution data derived from IEEE Std C37.13-2008. The fault currents are calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the first cycle duty multipliers described in IEEE Std 141™-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The momentary symmetrical current = E/Z .
- The X/R ratio is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.

Multiplying factors are determined, and used to adjust the calculated symmetrical fault current. The adjusted current is used to evaluate low voltage protective devices. Low voltage output algorithms and output reports reflect NEMA AB-1 molded case breaker de-rating multipliers. Breakers are de-rated for circuits where the power factor is lower than the NEMA test circuit (higher X/R ratio). The multipliers adjust the symmetrical fault current to the value associated with the systems fault point X/R ratio. The adjusted value listed on the report may then be compared directly with the manufacturer's published interrupting rating.

2. Momentary Duty Report

The “Momentary Duty Report” contains the calculated fault currents that occur during the first half-cycle of the fault. The momentary fault currents are used to evaluate medium and high voltage fuses, and the “closing and latching” capability (momentary rating) of medium and high voltage breakers. The fault currents reported in the “Momentary Duty Report” are calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the first cycle duty multipliers described in IEEE Std 141-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The momentary symmetrical current = E/Z .
- The X/R ratio reported is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.
- A_FAULT calculates and reports the momentary asymmetrical current in two different ways, once as “sym*1.6” and again as “momentary based on X/R ”. The “sym*1.6” value is the momentary symmetrical current multiplied by 1.6. The “momentary based on X/R ” value is the momentary symmetrical current multiplied by

$$\sqrt{1+2e^{(-2\pi/(X/R))}}$$

3. Interrupting Duty Report

The fault currents reported in the “Interrupting Duty Report” are used to evaluate the interrupting rating of medium- and high-voltage breakers. The interrupting symmetrical current is calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the interrupting duty multipliers described in IEEE Std 141-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The interrupting symmetrical current = E/Z .
- The X/R ratio reported is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.
- A_FAULT uses the calculated X/R ratio to determine the minimum contact parting time multiplying factors for 2, 3, 5, and 8 cycle breakers. The multiplying factors are based on IEEE Std C37.5-1979 and IEEE Std C37.010-1999 standards. The multiplying factors are applied to the interrupting symmetrical current in order to calculate the RMS short-circuit current interrupting duty for 2, 3, 5, and 8 cycle breakers. This duty is compared to the symmetrical current interrupting rating of the circuit breaker. NACD (No AC Decrement) ratios are calculated with consideration of generator “Local” and “Remote” contributions as outlined in IEEE Std C37.010-1999.
- Motor and generator impedance multipliers for the short-circuit calculations are summarized in the following table. This is based on the recommended combination network for comprehensive multi-voltage system calculations (from IEEE Std 141-1993; Red Book):

<u>Machine Type</u>	<u>Impedance (First Cycle Duty)</u>	<u>Impedance (Interrupting Duty)</u>
Turbine generators, Condensers, Hydrogenerators with amortisseur windings	1.0 Xd"	1.0 Xd"
Synchronous motors	1.0 Xd"	1.5 Xd"
Induction motors > 1000 hp at speed ≤ 1800 RPM, or > 250 hp at 3600 RPM.	1.0 Xd"	1.5 Xd"
Induction motors ≥ 50 hp not covered above.	1.2 Xd"	3.0 Xd"
Induction motors < 50 hp	1.67 Xd"	Neglect

Note: Xd" is the subtransient reactance of the rotating machine.

2.1 Short-Circuit Objectives

The objective of the short-circuit analysis is to calculate the maximum short-circuit currents produced by balanced three-phase and unbalanced faults at each bus shown on the one-line diagrams in Appendix D.

2.2 System Modeling

For all systems with either a 480/277 V or 208/120 V, wye configured service, short-circuit currents were calculated for a three-phase bolted fault and single-line-to-ground fault at each bus shown on the one-line diagrams found in Appendix D. The system was modeled for worst-case fault currents.

For all systems with a 240/120 V, open delta configured service, short-circuit currents were calculated for a line-to-line bolted fault at each bus shown on the one-line diagrams found in Appendix D. It is not possible to model single winding transformers in SKM, therefore an equivalent three-phase transformer was modeled to provide the most accurate results possible while still remaining conservative. For all 240/120 V services with unequally sized transformers, or transformers with unequal impedances, a three-phase, delta winding, the kVA of the equivalent transformer is modeled as three times the kVA of the largest single transformer installed by PGE. The impedance of the equivalent transformer is modeled as equal to the %Z of the largest single transformer installed by PGE. For all 240/120 V services with equally sized transformers, the equivalent transformer is modeled as three times the kVA of a single transformer winding. The impedance of the equivalent transformer is modeled as equal to the winding with the lowest %Z. In the equipment

evaluation, the calculated line-to-line fault was reported to represent the worst-case scenario.

1. Cases:

Multiple scenarios were only necessary when examining fault-current values at the 4th Avenue / Engineering Building, as this is the only building with multiple sources of power. The following short-circuit study cases were evaluated:

- Study Case No. 1 – System supplied from the Urban-Medical utility feed via Medium Voltage Switchgear B-EB-52-U1. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U2 are open.
- Study Case No. 2 – System supplied from the Urban-Gibbs utility feed via Medium Voltage Switchgear B-EB-52-U2. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U1 are open.
- Study Case No. 3 – System supplied from the Emergency Generator via Medium Voltage Switchgear B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-U1 and BK-EB-52-U2 are open.
- Study Case No. 4 – System supplied from the Urban-Medical utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U1 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U2 is open.
- Study Case No. 5 – System supplied from the Urban-Gibbs utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U2 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U1 is open. **This is the worst case scenario and the scenario illustrated in the one-line diagram found in Appendix D.**

2. Utility Information:

Utility transformer and source impedance information was provided by Tom Riddle with PGE on 1/10/2013 via email. Information for all PGE utility sources is summarized in Appendix C.

The Market Center Building is not supplied by PGE, but is supplied by PacifiCorp. It was not possible to obtain fault current information from PacifiCorp at the time of this study. To ensure conservative results, an infinite bus was assumed on the primary side (12.47 kV) of utility transformers TX-MCB UTIL-A, TX-MCB UTIL-B and TX-MCB BSMT UTIL. The following values were calculated on the secondary side (480 V) of each transformer based on transformer nameplate information gathered during data collection:

TX-MCB UTIL-A

- Three-phase fault current: 15,826.5 A

TX-MCB UTIL-B

- Three-phase fault current: 16,705.7 A

TX-MCB BSMT UTIL

- Three-phase fault current: 8,018.8 A

3. System Information:

Input data used in this study was obtained from the following sources:

- Building one-line diagrams provided by Portland State University
- Eaton on-site data collection performed October 2012 to February 2013.

4. Assumptions:

The following assumptions were used in modeling the power system, and ensure conservative, worst-case results:

- For fault currents in the Market Center Building (MCB), it was assumed that three-phase and single-line to ground fault currents were identical.
- An X/R ratio of 5.2402 was used to model utility fault contributions MCB INF UTIL-A and MCB INF UTIL-B. An X/R ratio of 4.1498 was used to model utility fault contribution MCB BSMT INF UTIL.
- It is assumed that fault current contributions from motors would be negligible.
- It is assumed that the impedance of cables from the utility transformer to each service entrance would be negligible; therefore these cables were excluded from the study.
- System voltage is modeled at 100% nominal.
- All low voltage cable is modeled in non-magnetic conduit.
- All medium voltage cable is modeled in non-magnetic conduit.
- Generator subtransient reactances for generator G-EB GEN (X''_d , X_2 , and X_0) are assumed to be 10%.
- Unless otherwise provided, transformer X/R ratios are obtained from IEEE Std C37.010-1999.
- It was assumed the Urban-Gibbs and Urban-Medical utility feeds in the Engineering Building had the same fault current characteristics.

Complete information regarding the system model used for the computer simulation is included in Appendix A.

2.3 Short-Circuit Results

The results of the short-circuit analysis, including calculated branch contributions, are provided in Appendix B. The one-line diagrams with referenced bus identification are included in Appendix D.

2.4 Equipment Evaluation

The purpose of the equipment evaluation is to compare the *maximum* calculated short-circuit currents to the short-circuit ratings of protective devices. The comparison is made in order to determine if the device can interrupt or withstand the available fault currents of the electrical system to which the device is applied, as required by NEC-2011, Article 110.9 and NEC-2011, Article 110.10. The device evaluation follows the evaluation procedures outlined in IEEE Std C37.13-2008, IEEE Std C37.010-1999, IEEE Std C37.5-1979, IEEE Std C37.41™-2008, IEEE Std 1015™-2006 (Blue Book), and applicable ANSI, NEMA, and UL standards.

The results of the short-circuit equipment evaluation are summarized in Table 2.1. The table indicates “Bus I.D.” (corresponds to bus designations used in the one-line diagrams of Appendix D), “Manufacturer”, “Status” (Pass, fail, unknown, or marginal), “Type” (equipment category), “Equip Volts”, calculated short-circuit duty, the equipment short-circuit rating, the series rating (if applicable), and the maximum duty rating.

The maximum duty rating is calculated by:

$$\frac{S.C.duty}{DeviceS.C.Rating} \times 100$$

For equipment with series ratings, the maximum duty rating is calculated using the series rating instead of the individual device short-circuit rating. All short-circuit current values are reported in units of kA.

1. For low voltage devices:

The calculated short-circuit duty is reported under “Calc Isc (kA)” and the device short-circuit rating is reported under “Equip Isc (kA)”. The calculated duty has been adjusted accordingly per the system X/R and device test X/R. For all 240/120 V systems, the line-to-line fault current is presented under the column “Calc Isc (kA)”. 240/120 V entries do not include an X/R adjustment. By examination it was determined that this adjustment will not change the pass/fail status of any 240/120 equipment and was therefore excluded.

2. For medium/high voltage breakers:

The calculated *interrupting* short-circuit duty is reported under “Calc Isc (kA)” and the breaker short-circuit interrupting rating is reported under “Equip Isc (kA)”. The interrupting duty has been adjusted per multiplying factors based on the breaker clearing time and system X/R. The calculated momentary

duty (i.e. close-and-latch duty) is reported under "Calc Mom (kA)". The breaker momentary (i.e. close-and-latch) rating is reported under "Equip Msc (kA)".

3. For medium/high voltage fuses, switches, and motor starters:

The calculated *momentary symmetrical* short-circuit duty is reported under "Calc Isc (kA)" and the device's momentary symmetrical short-circuit rating is reported under "Equip Isc (kA)". The calculated *momentary asymmetrical* duty is reported under "Calc Mom (kA)". The device's momentary asymmetrical short-circuit rating is reported under "Equip Mom (kA)".

Table 2.1 - Equipment Evaluation

Bus I.D.	Manufacturer	Status	Type	Bus Voltage (V)	Calc Isc (kA)	Equip Isc (kA)	Rating %	Calc Mom (kA)	Equip Mom (kA)	Rating %
B-SEC NORTH ECB-USB	ITE	Pass	LV Enclosed Circuit Breaker	240	35.167	42.00	83.73			
B-EB-FP DISC-USB	Eaton	Pass	LV Enclosed Circuit Breaker	480	1.90	35.00	5.43			
B-AB ANNEX DISC-USB	GE	Fail	LV Fused Disconnect	208	*33.77 (*N1)	10.00	337.70			
B-AB DISC-USB	Pierce	Pass	LV Fused Disconnect	208	42.53	200.00	21.27			
B-BLKS K-USB	Siemens	Pass	LV Fused Disconnect	240	27.127	200.00	13.56			
B-EH E DISC-USB	Cutler-Hammer	Pass	LV Fused Disconnect	240	19.674	100.00	19.67			
B-PS3-USB	Circle W Products	Pass	LV Fused Disconnect	208	16.29	200.00	8.15			
B-SBH DISC A-USB	Siemens	Pass	LV Fused Disconnect	240	8.109	100.00	8.11			
B-SBH DISC B-USB	Siemens	Pass	LV Fused Disconnect	240	8.109	100.00	8.11			
B-SEC SOUTH DISC 1A-USB	Major	Pass	LV Fused Disconnect	240	31.585	200.00	15.79			
B-SEC SOUTH DISC 2A-USB	Major	Pass	LV Fused Disconnect	240	31.232	200.00	15.62			
B-SEC SOUTH DISC 2B-USB	Major	Pass	LV Fused Disconnect	240	31.232	200.00	15.62			
B-STFR-USB	Bulldog	Pass	LV Fused Disconnect	240	45.17	200.00	22.59			
B-URBN FP DISC-USB	GE	Pass	LV Fused Disconnect	480	40.74	100.00	40.74			
B-KHSE-USB	Square D	Pass	LV Fused Panelboard	208	30.43	200.00	15.22			
B-MONT-USB	Gould	Pass	LV Fused Switchboard	240	35.777	200.00	17.89			
B-AB PNLBRD-USB	FPE	Fail	LV Panelboard	208	*45.45 (*N1)	18.00	302.50			
B-BLKS L1-USB	Gould	Fail	LV Panelboard	240	32.633	10.00	326.33			
B-BLKS L2-USB	Gould	Fail	LV Panelboard	240	32.633	10.00	326.33			
B-BLKS L3-USB	Gould	Fail	LV Panelboard	240	32.633	10.00	326.33			
B-BLKS L4-USB	Gould	Fail	LV Panelboard	240	32.633	10.00	326.33			
B-BLKS L5-USB	Gould	Fail	LV Panelboard	240	32.633	10.00	326.33			
B-BLKS X-USB	Gould	Fail	LV Panelboard	240	24.199	10.00	241.99			
B-EH A-USB	Cutler-Hammer	Fail	LV Panelboard	240	19.674	10.00	196.74			
B-EH B-USB	Cutler-Hammer	Fail	LV Panelboard	240	19.674	10.00	196.74			
B-EH C-USB	Cutler-Hammer	Fail	LV Panelboard	240	19.674	10.00	196.74			
B-HGDC-USB	Square D	Pass	LV Panelboard	240	38.765	65.00	59.64			

Bus I.D.	Manufacturer	Status	Type	Bus Voltage (V)	Calc Isc (kA)	Equip Isc (kA)	Rating %	Calc Mom (kA)	Equip Mom (kA)	Rating %
B-HH 1-USB	GE	Fail	LV Panelboard	240	44.004	10.00	440.04			
B-HH 2-USB	GE	Fail	LV Panelboard	240	39.714	10.00	397.14			
B-HSB-USB	Cutler-Hammer	Fail	LV Panelboard	240	42.323	10.00	423.23			
B-PRKW L1-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-PRKW L2-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-PRKW L3-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-PRKW L4-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-PRKW L5-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-PRKW X-USB	ITE	Fail	LV Panelboard	240	35.121	10.00	351.21			
B-SEC NORTH PNL-USB	ITE	Fail	LV Panelboard	240	35.167	10.00	351.67			
B-SEC SOUTH PNL 1B-USB	Square D	Fail	LV Panelboard	240	31.232	10.00	312.32			
B-SEC SOUTH PNL 1C-USB	Square D	Fail	LV Panelboard	240	31.232	10.00	312.32			
B-SEC SOUTH PNL 1D-USB	Square D	Fail	LV Panelboard	240	31.232	10.00	312.32			
B-STHL L1-USB	ITE	Fail	LV Panelboard	240	16.123	10.00	161.23			
B-STHL L2-USB	ITE	Fail	LV Panelboard	240	15.98	10.00	159.80			
B-STHL L3-USB	ITE	Fail	LV Panelboard	240	15.838	10.00	158.38			
B-STHL L4-USB	ITE	Fail	LV Panelboard	240	15.698	10.00	156.98			
B-STHL L5-USB	ITE	Fail	LV Panelboard	240	15.559	10.00	155.59			
B-STHL X-USB	ITE	Fail	LV Panelboard	240	15.423	10.00	154.23			
B-UHP-USB	GE	Fail	LV Panelboard	240	13.47	10.00	134.70			
B-ARC-A-USB	ITE	Pass	LV Switchboard	480	16.34 (*N1)	18.00	90.78			
B-ARC-B-USB	ITE	Fail	LV Switchboard	208	*23.42 (*N1)	18.00	130.11			
B-BHB MSB-A-USB	Square D	Pass	LV Switchboard	480	18.55 (*N1)	65.00	28.54			
B-BHB MSB-B-USB	Square D	Pass	LV Switchboard	208	27.65	65.00	42.54			
B-BHB MSB-C-USB	Square D	Pass	LV Switchboard	208	27.65	65.00	42.54			
B-HOFF-USB	GE	Pass	LV Switchboard	208	33.25	65.00	51.15			
B-JCB-USB	GE	Pass	LV Switchboard	208	33.47	65.00	51.49			
B-KNGA-USB	GE	Fail	LV Switchboard	240	42.323	10.00	423.23			
B-MCB BSMT-USB	ITE	Pass	LV Switchboard	480	8.54 (*N1)	18.00	47.44			

Bus I.D.	Manufacturer	Status	Type	Bus Voltage (V)	Calc Isc (kA)	Equip Isc (kA)	Rating %	Calc Mom (kA)	Equip Mom (kA)	Rating %
B-MCB PNTHS-USB	ITE	Fail	LV Switchboard	480	*35.37 (*N1)	18.00	196.50			
B-MSB-A SUB SWBD-USB	Square D	Pass	LV Switchboard	480	18.50 (*N1)	65.00	28.46			
B-NASC-USB	Square D	Pass	LV Switchboard	208	15.56	65.00	23.94			
B-OND 15 FLR-USB	FPE	Fail	LV Switchboard	240	18.488	10.00	184.88			
B-OND ANNEX SWBD-USB	Cutler-Hammer	Pass	LV Switchboard	208	39.76	65.00	61.17			
B-OND MAIN SWBD-USB	Cutler-Hammer	Pass	LV Switchboard	480	16.60	65.00	25.54			
B-SBA-USB	ITE	Fail	LV Switchboard	208	*33.13 (*N1)	18.00	184.06			
B-SEH-USB	GE	Pass	LV Switchboard	208	33.25	65.00	51.15			
B-SH-USB	GE	Pass	LV Switchboard	208	52.21	85.00	61.42			
B-UCB-USB	GE	Pass	LV Switchboard	208	31.92	42.00	76.00			
B-UP-A-USB	ITE	Fail	LV Switchboard	480	*40.92 (*N1)	18.00	227.33			
B-UP-B-USB	ITE	Fail	LV Switchboard	208	*72.32 (*N1)	10.00	723.20			
B-URBN SWBD-USB	Cutler-Hammer	Pass	LV Switchboard	480	40.74	65.00	62.68			
B-EB-USB-1	Eaton	Pass	LV Switchgear	480	26.42	65.00	40.65			
B-EB-USB-2	Eaton	Pass	LV Switchgear	480	26.44	65.00	40.68			
B-EB-USB-3	Eaton	Pass	LV Switchgear	208	36.47	65.00	56.11			
B-EB-USB-5	Eaton	Pass	LV Switchgear	480	25.79	65.00	39.68			
B-EB-USB-6	Eaton	Pass	LV Switchgear	480	26.41	65.00	40.63			
B-EB-USB-7	Eaton	Pass	LV Switchgear	480	26.43	65.00	40.66			
B-EB-52-U1	Eaton	Pass	MV Switchgear	12470	5.91	23.00	25.70	7.44	37.00	20.12
B-EB-52-U2	Eaton	Pass	MV Switchgear	12470	5.92	23.00	25.74	7.46	37.00	20.16
B-EB-52-U3	Eaton	Pass	MV Switchgear	12470	5.91	23.00	25.70	7.45	37.00	20.15

(*N1) System X/R higher than Test X/R, Calc Isc kA modified based on low voltage factor.

3.0 PROTECTIVE DEVICE COORDINATION STUDY

The protective device coordination study determines overcurrent protective relay and circuit breaker settings in order to provide an optimal compromise between protection and selectivity.

The coordination plots were developed using SKM System Analysis' CAPTOR software. Protective device coordination was performed in accordance with IEEE Std 242™-2001 (Buff Book). Minimum guidelines for equipment protection, as outlined in the National Electrical Code (NEC) and applicable standards of the American National Standards Institute (ANSI), were followed.

3.1 General Description and Protection Philosophy

Using the appropriate maximum fault currents, the time-current coordination curves were plotted as operating time versus current magnitudes to show protective device tripping and/or clearing characteristics and coordination among these devices.

Consideration was given to provide both selective isolation of faults and maximum protection of equipment such as cables, transformers, motors, etc.

To achieve the optimum protection and selectivity, the following guidelines were followed throughout the study:

1. Ideally, the settings of any overcurrent device should be high enough to permit the continuous full-load operating capacity of the cables and the equipment they supply, and to ride through system temporary disturbances such as in-rush current. On the other hand, the settings should be low enough to provide overload and short-circuit protection under minimum fault conditions.
2. Considering any two protective devices in series:
 - The maximum available fault current at the downstream device determines the upper limit of the coordination range between these two devices.
 - The minimum available fault current at the downstream device or the pick-up setting of the upstream device determines the lower limit of the coordination range.
 - Series instantaneous devices do not coordinate unless there is sufficient impedance between the two devices.
 - When plotting coordination curves, certain time intervals must be maintained between the curves in order to ensure correct selectivity. These time intervals vary, depending on the device types. In general, however, the following must be taken into consideration when determining the appropriate time separation interval: Breaker clearing

time, relay tolerances, induction disk over-travel, and a reasonable safety margin for error.

3.2 Codes and Standards

The minimum protection requirements as outlined in the National Electric Code (NEC), ANSI, and IEEE Standards were used as guidelines for protective device settings.

Applicable requirements are summarized below.

1. Cables

Power cables require overload and short-circuit protection in order to meet the requirements stated in NEC-2011, Article 240, and IEEE Std 242-2001 (Buff Book). NEC further requires that the ampacity of low voltage cable (0-2000 Volts) be determined by NEC-2011, Article 310.15. Cable de-rating based upon ambient temperature and the number of current carrying conductors in a raceway must also be applied. Medium voltage cable (2001-35,000 Volts) ampacity is defined by NEC-2011, Article 240.100(A) and NEC-2011, Article 310.60.

2. Transformers

A transformer is recommended to have protective devices on both primary and secondary side in order to meet the basic protection requirements for overloads and short-circuit withstand values. However, a transformer is permitted to be protected by only a primary side device if it meets the exceptions listed in NEC-2011, Article 240.4(F). In addition, the transformer protective devices must be able to withstand magnetizing inrush currents without tripping.

NEC protection requirements for transformers: Overcurrent devices are selected, and settings are recommended to provide overcurrent protection in accordance with NEC-2011, Article 450.3. Paragraph (A) specifies that transformers over 600 V comply with Table 450.3(A). Paragraph (B) specifies that transformers less than 600 V comply with Table 450.3(B). These tables provide guidance for sizing of primary and secondary overcurrent protective devices based on transformer full load ampere ratings, transformer impedance, and transformer location.

Short-circuit thermal limits for transformers: The primary devices should be set on the basis that the transformers have short-circuit withstand capabilities as defined by IEEE Std C57.109™-1993.

3. Motors

The motors should have appropriate protective devices to meet the basic protection requirements for overloads and fault current withstand values. In addition, the motor short-circuit and ground fault protective devices should be set to ride through motor starting current.

3.3 Coordination Objectives

Review the existing system overcurrent protection and coordination. Provide suggestions for improvement.

3.4 Coordination Results

For all locations except the 4th Avenue / Engineering Building, the system coordination began at first overcurrent protective device upstream of the utility transformer, and continued downstream through the service entrance to the largest overcurrent protective device which is not in series with the utility overcurrent device.

For the 4th Avenue / Engineering Building, the normal side system coordination began at the 12.47 kV utility fault interrupter and continued downstream the Switchboards B-EB-52-U1 and B-EB-52-U2 to the largest feeder breaker in each of the Unit Substations B-EB-USB-1 – B-EB-USB-7. The emergency system coordination began at the 12.47 kV main relay in B-EB-52-E3 and continued downstream through Switchboards B-EB-52-U1 and B-EB-52-U2 to the largest feeder breaker in each of the Unit Substations B-EB-UB-1 – B-EB-USB-7.

As shown on the time-current plots, each device curve is tagged with an arrow and label referencing its location on the plot's individual representative one-line diagram. This label also references the device to its' specific manufacturer information, including ratings and settings, as indicated in the text box on each plot. The device time-current characteristics are truncated at maximum through-fault current for a downstream fault.

Efforts were made to provide the best coordination possible with the existing protective devices. Areas where breaker trip curves overlap indicate areas of possible non-selective breaker operation. Where possible, efforts were made to reduce non-selective breaker operation while maintaining adequate system protection. In some cases, because of device limitations, little can be done to improve device selectivity. Such device limitations include the fixed operating characteristic of a fuse, the built-in instantaneous or instantaneous "over-ride" elements of molded case circuit breakers, and the limited instantaneous trip range of trip units with an instantaneous trip function.

In cases involving redundant protective devices, non-selective breaker operation is of little or no concern. Protective devices are redundant if, regardless of which device opens, the same system outage occurs. Often, in order to improve overall system protection and coordination, redundant devices are intentionally set to overlap (i.e. non-selectively coordinate with) one another.

Adequate coordination is achieved using the recommended protective devices, with settings and ratings as listed in Section 4. The recommended adjustments would maximize coordination in an attempt to allow the various downstream devices to isolate faults without operation of the upstream devices. Although instantaneous trip devices provide the highest degree of

protection, when applied in series they compromise selectivity at high-magnitude fault currents.

3.5 Coordination Recommendations

All of the adjustable low voltage electronic trip and thermal magnetic circuit breakers and medium voltage equipment should be tested and adjusted according to the recommended settings given in Section 4.

If the largest feeder breaker in a service entrance disconnect was adjustable, the as-found settings were used to plot the coordination curve. It is not possible to ensure these breakers are properly set without expanding the scope of this study to downstream locations. Therefore, no settings are recommended for these locations.

Additionally, medium voltage coordination in the Engineering Building should be examined to ensure proper settings in all relays. Many of the relays have an instantaneous overcurrent function (ANSI function 50) programmed for both the phase and neutral trip settings. In many cases this is not desirable as it can lead to a lack of selectivity or a ‘race’ between two relays when a fault with a high current is detected. This ‘race’ may result in an operation of both the main and feeder breaker and may result in unnecessary loss of load to the system. It is recommended that these settings be examined to determine if there are any possible changes that would improve coordination. When reviewing the settings, it may be important to include PGE in the conversation to ensure new settings do not disrupt the use of the 3 MW turbine as a co-generation facility.

3.6 Time-Current Characteristic Plots

Refer to the following pages for the plotted coordination curves, which graphically indicate the degree of selectivity and protection obtained.

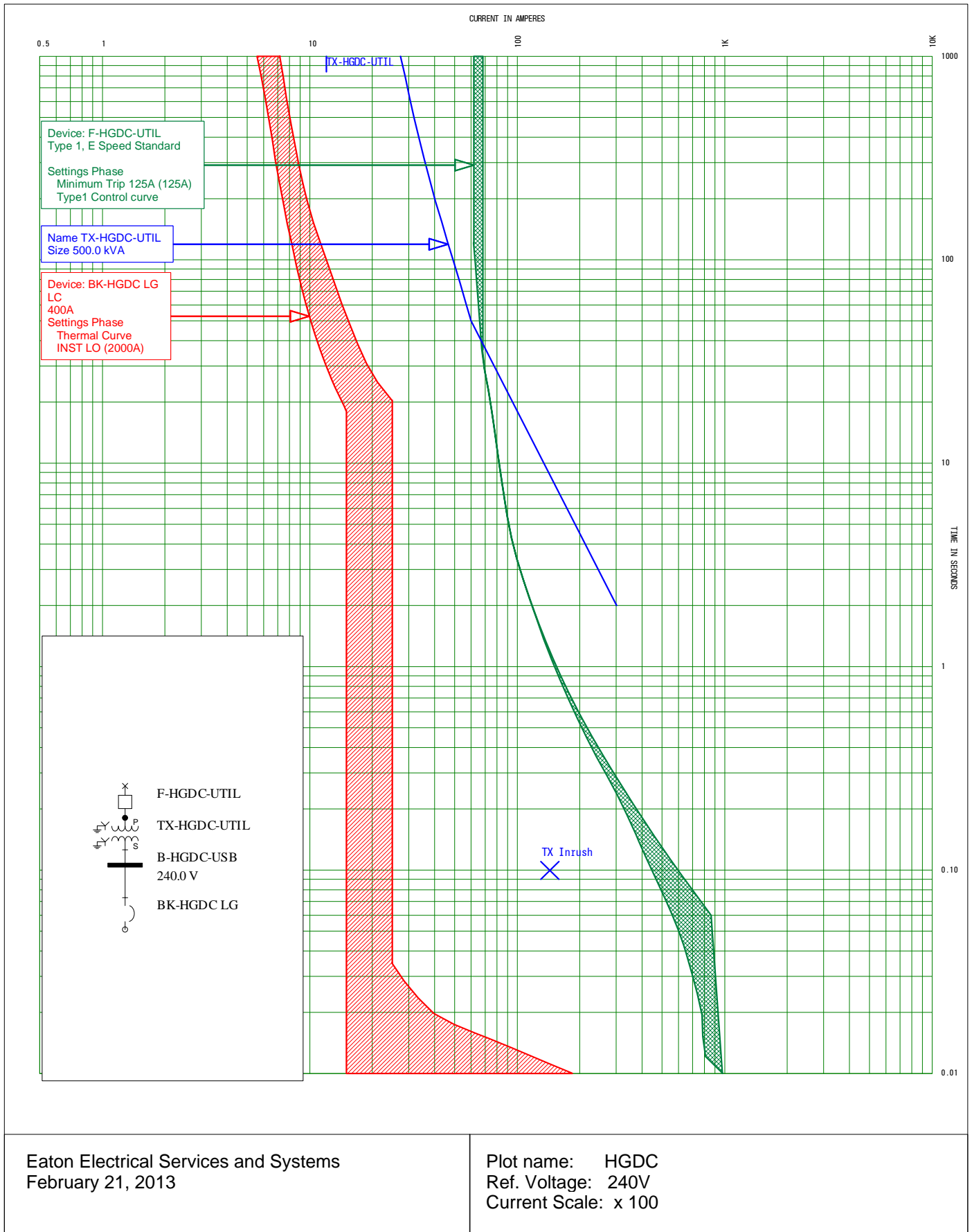
In some cases, a single time-current curve may be applicable to several locations in the system, where each location utilizes substantially similar devices, and serves similar loads.

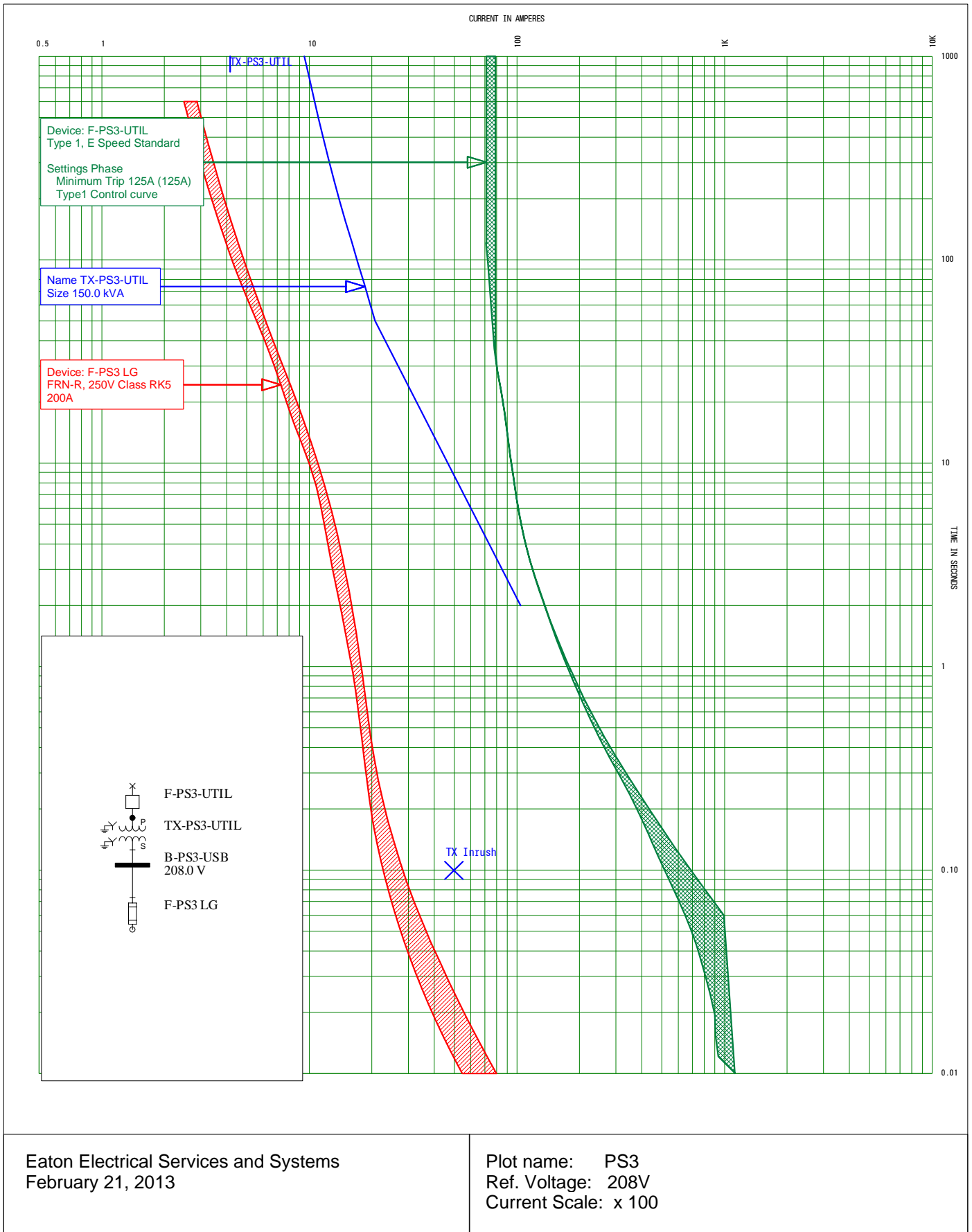
The following list references the attached time-current curves for this report.

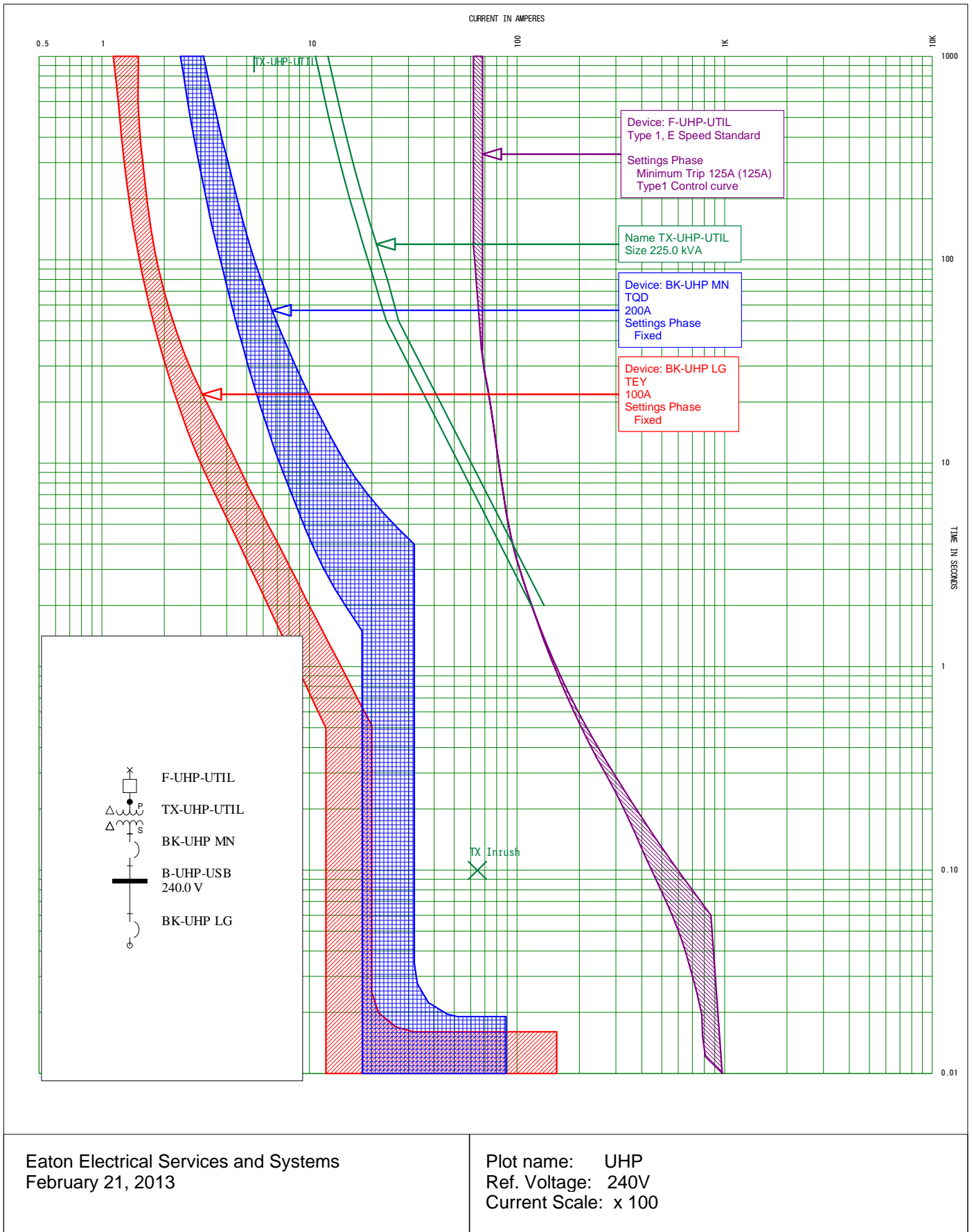
Table 3.1 – TCC Plots Index

HGDC	Page 3-6
PS3	Page 3-7
UHP	Page 3-8
JCB	Page 3-9
STHL L1	Page 3-10
STHL X	Page 3-11
SEH	Page 3-12
HOFF	Page 3-13
KNGA	Page 3-14
STFR	Page 3-15

HH 1	Page 3-16
HH 2	Page 3-17
PRKW L3	Page 3-18
PRKW X	Page 3-19
HSB	Page 3-20
MONT	Page 3-21
SBH	Page 3-22
BLKS L1	Page 3-23
BLKS K	Page 3-24
SH	Page 3-25
EH	Page 3-26
UCB	Page 3-27
OND MAIN	Page 3-28
OND 15TH FLR	Page 3-29
OND ANNEX	Page 3-30
BHB MSB-A	Page 3-31
BHB MSB-B	Page 3-32
NASC	Page 3-33
AB DISC	Page 3-34
AB PNLBD	Page 3-35
AB ANNEX	Page 3-36
EB USB-1 MV	Page 3-37
EB USB-7 MV	Page 3-38
EB USB-3	Page 3-39
EB USB-5	Page 3-40
EB 52-U1 GEN	Page 3-41
EB FP	Page 3-42
EB USB-1-2 LV	Page 3-43
EB USB-6-7 LV	Page 3-44
EB USB-1-2 GF	Page 3-45
EB-USB-3 GF	Page 3-46
EB-USB-5 GF	Page 3-47
EB USB 6-7 GF	Page 3-48
EB 52-U1 GF	Page 3-49
EB 52-U3 GF	Page 3-50
SEC SOUTH DISC 1A	Page 3-51
SEC SOUTH PNL 1B	Page 3-52
SEC SOUTH PNL 1C	Page 3-53
SEC NORTH	Page 3-54
UP A	Page 3-55
UP B	Page 3-56
KHSE	Page 3-57
SBA	Page 3-58
ARC A	Page 3-59
ARC B	Page 3-60
URBN SWBD	Page 3-61
URBN FP	Page 3-62
MCB	Page 3-63

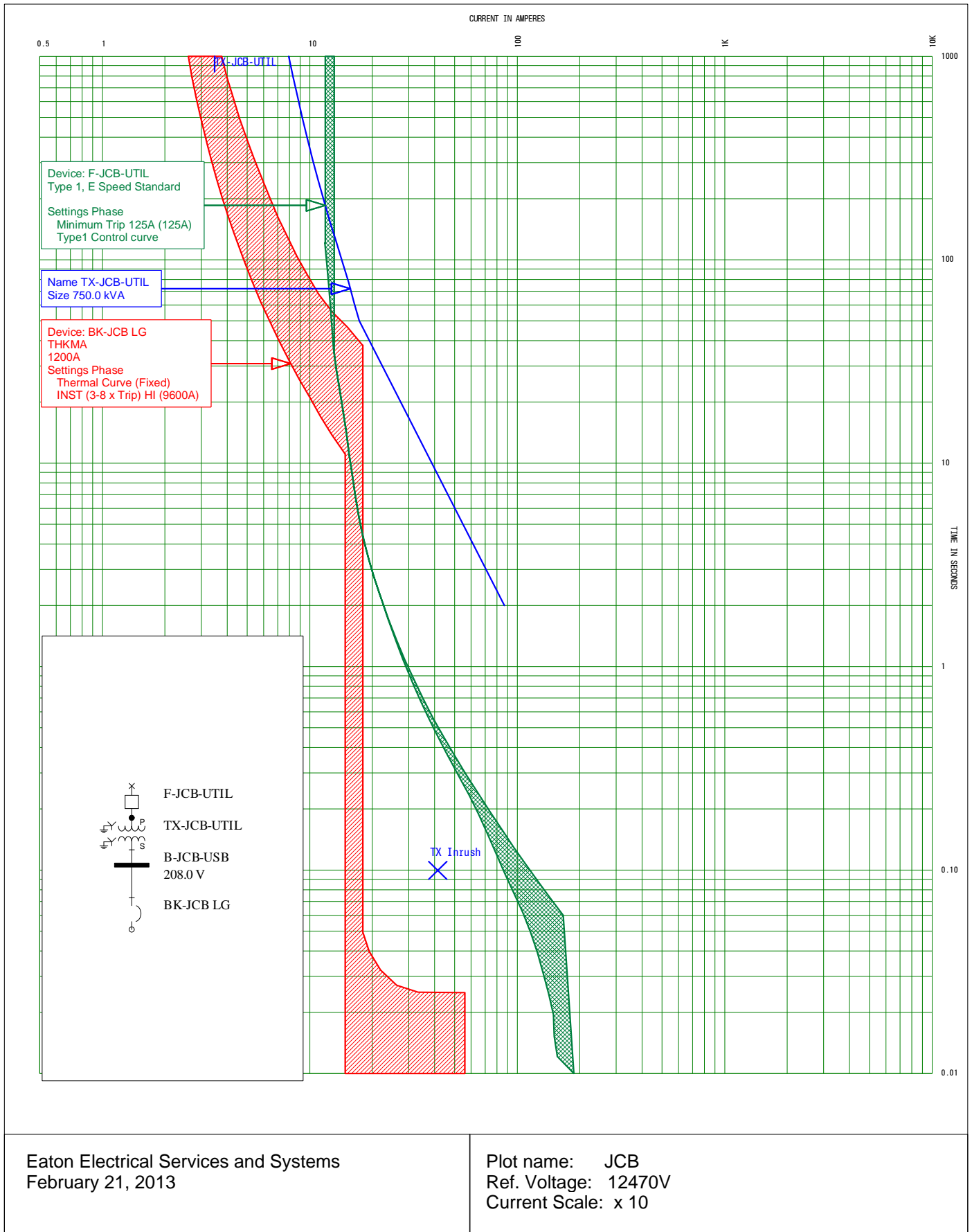






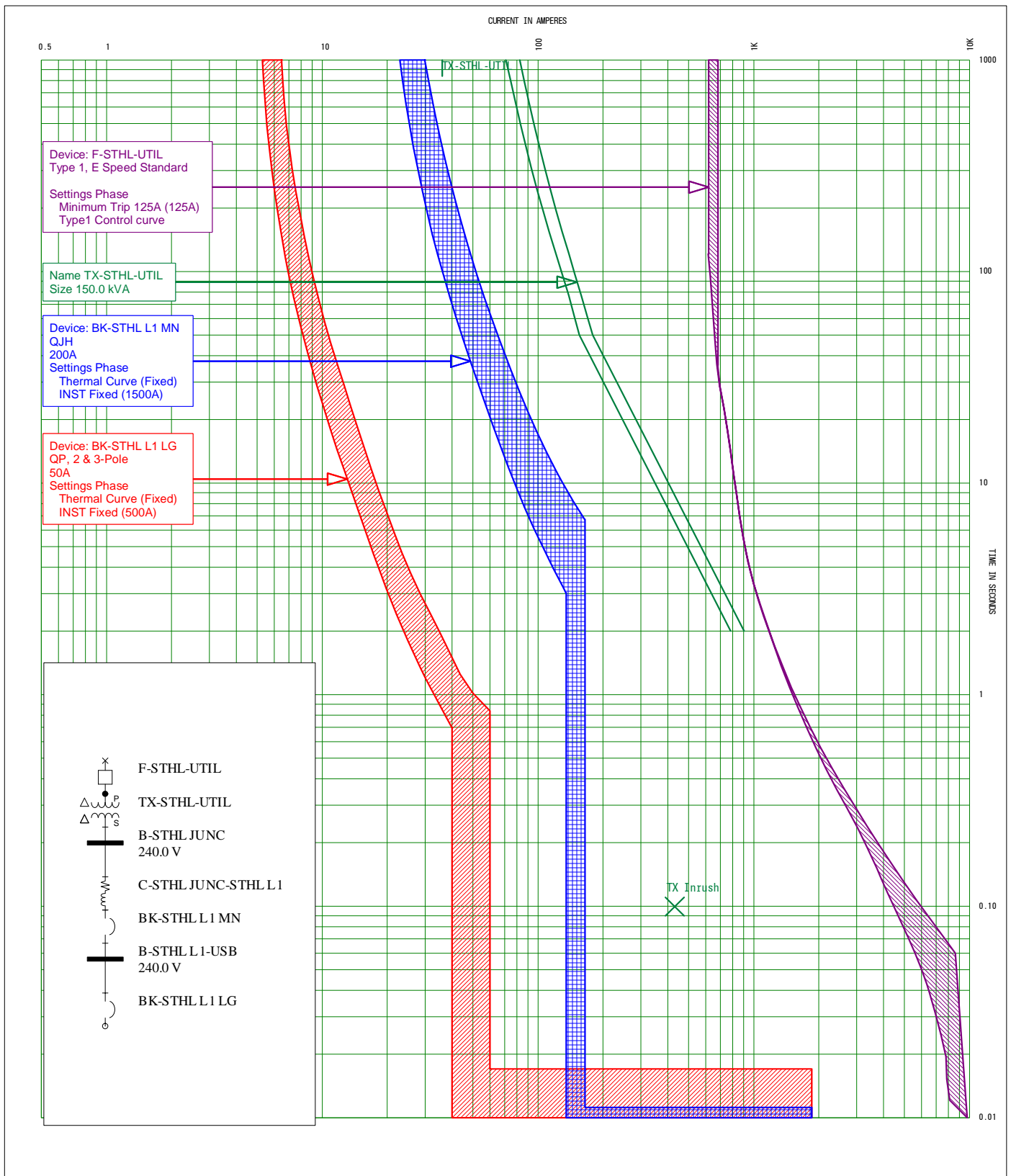
Eaton Electrical Services and Systems
February 21, 2013

Plot name: UHP
Ref. Voltage: 240V
Current Scale: x 100



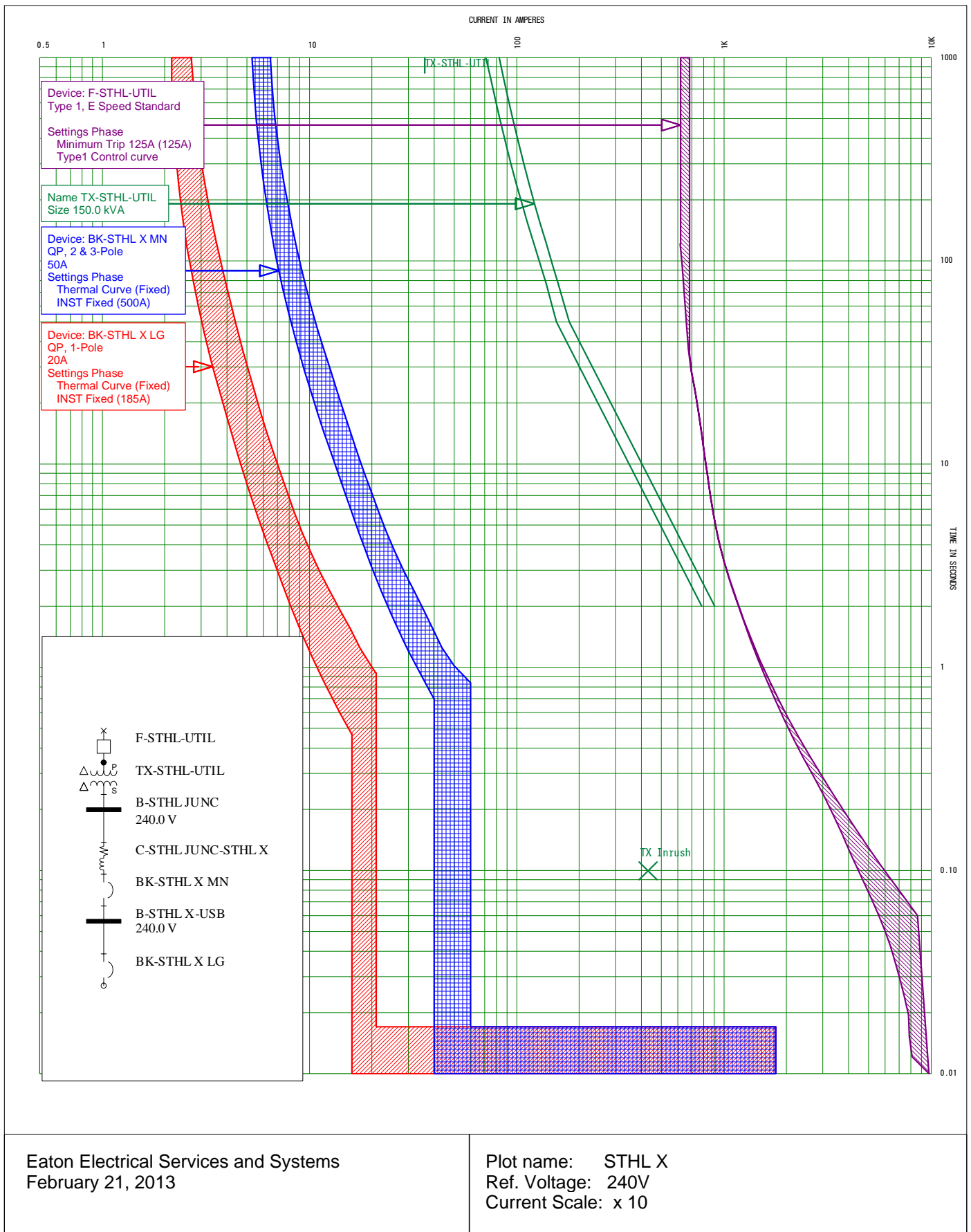
Eaton Electrical Services and Systems
February 21, 2013

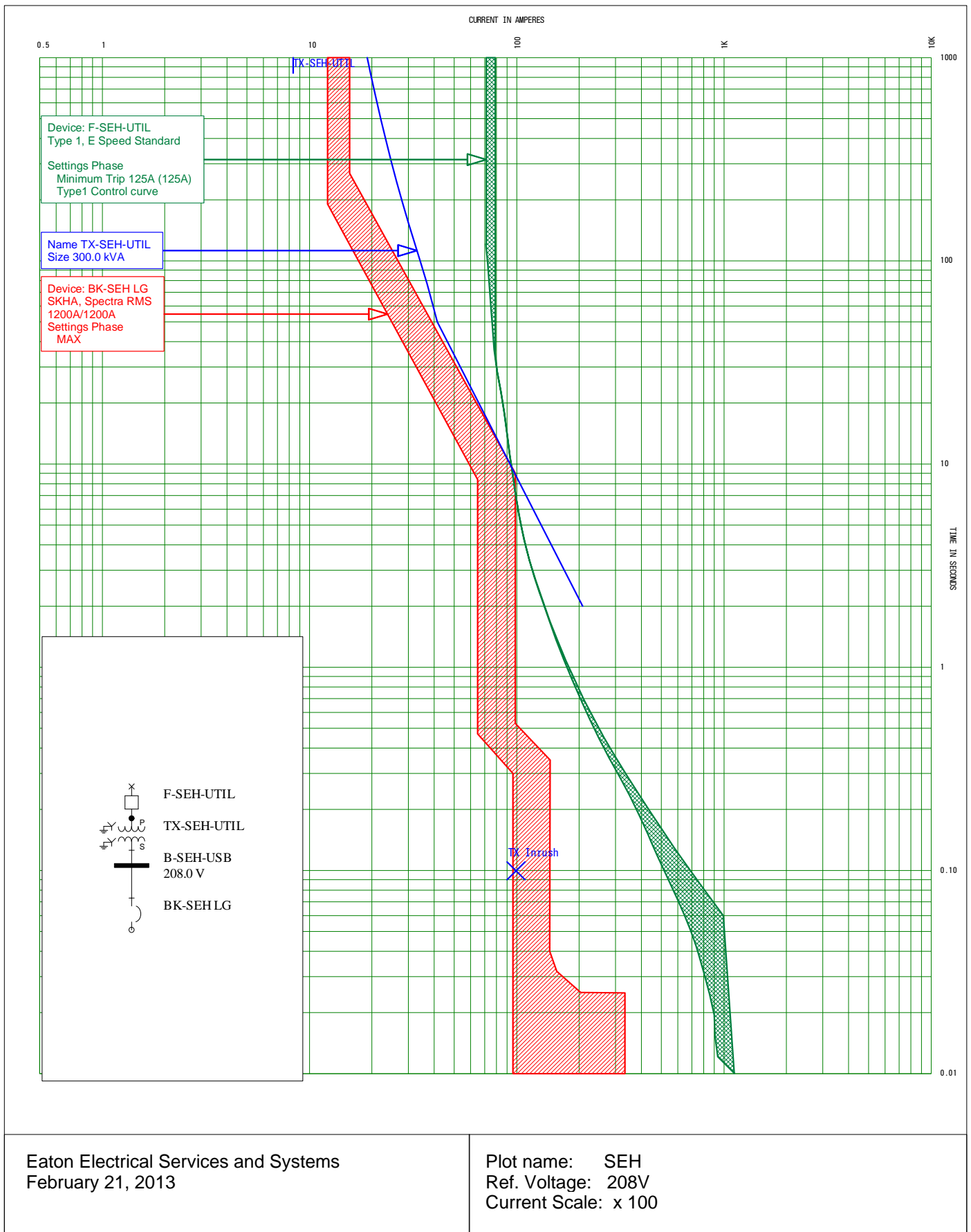
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Ref. Voltage: 12470V
Current Scale: x 10

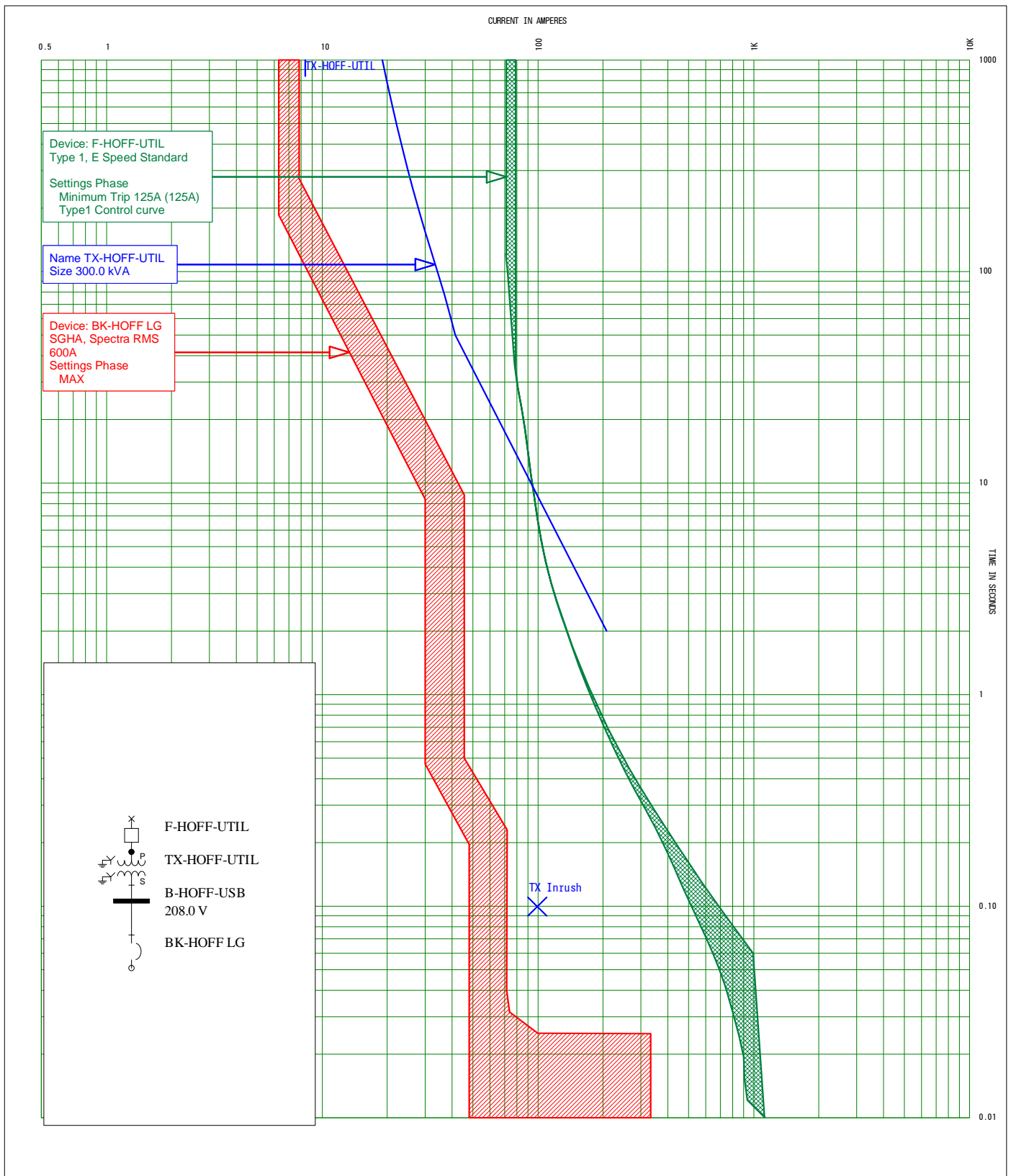


Eaton Electrical Services and Systems
February 21, 2013

Plot name: STHL L1
Ref. Voltage: 240V
Current Scale: x 10

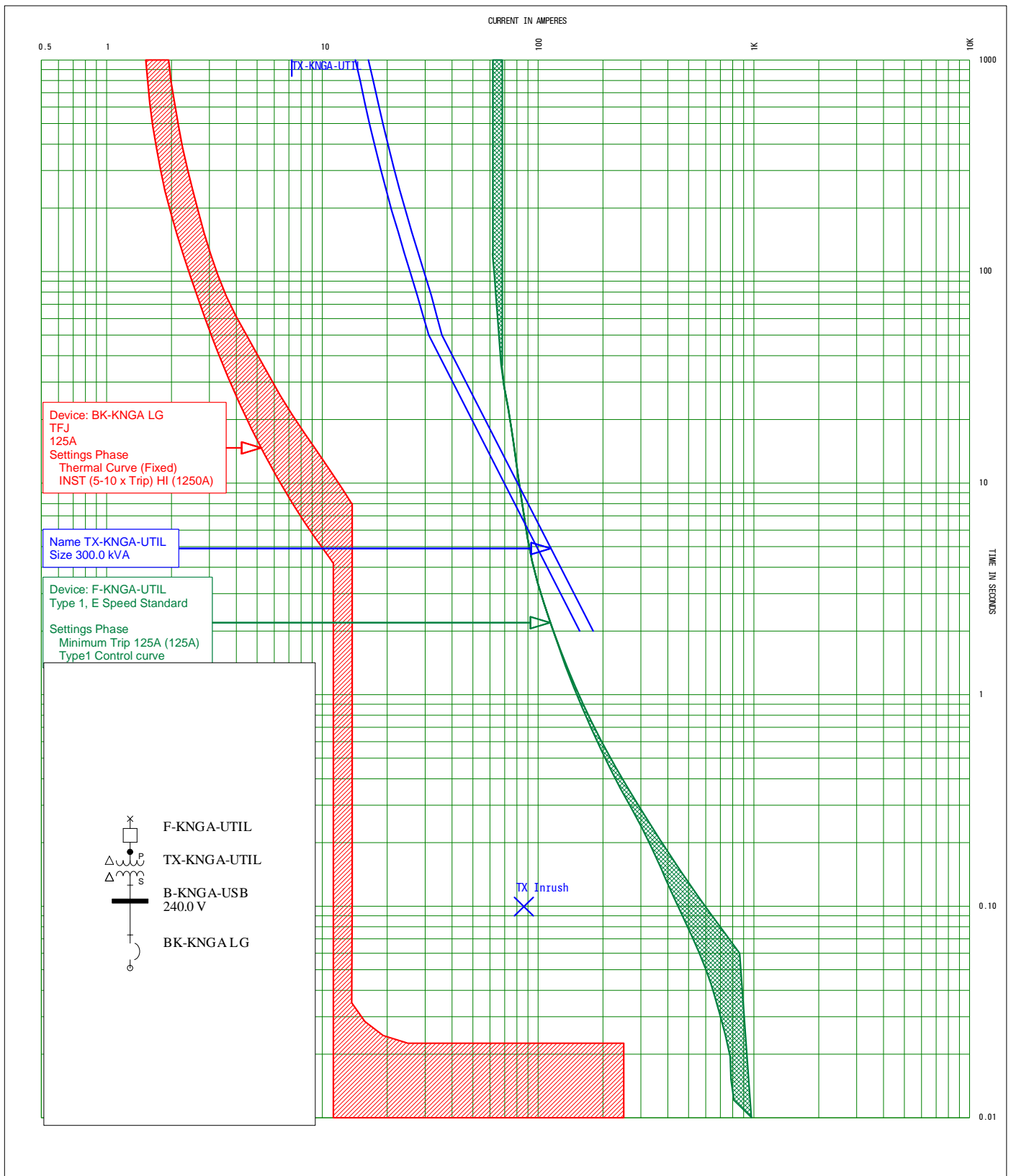






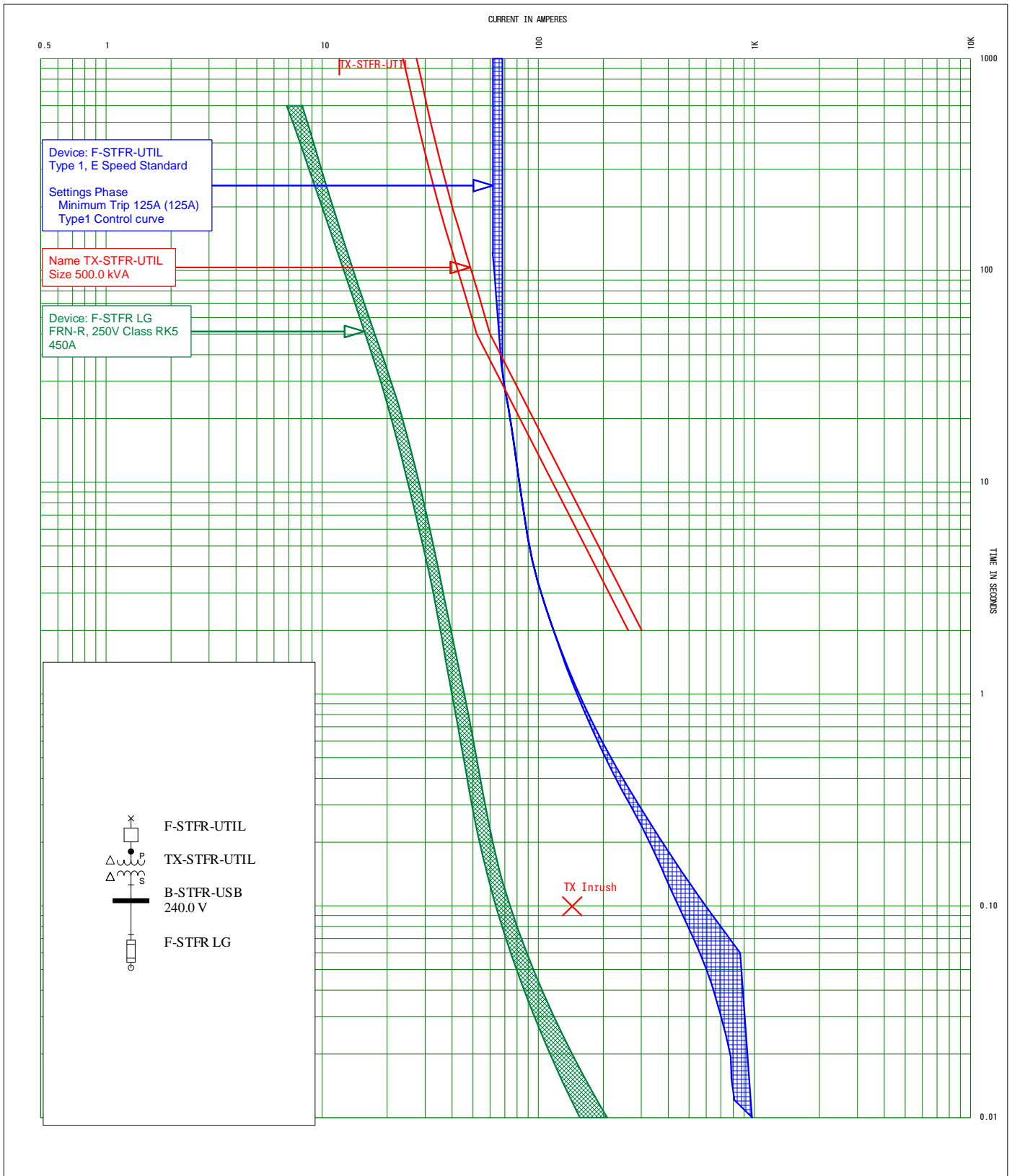
Eaton Electrical Services and Systems
February 21, 2013

Plot name: HOFF
Ref. Voltage: 208V
Current Scale: x 100



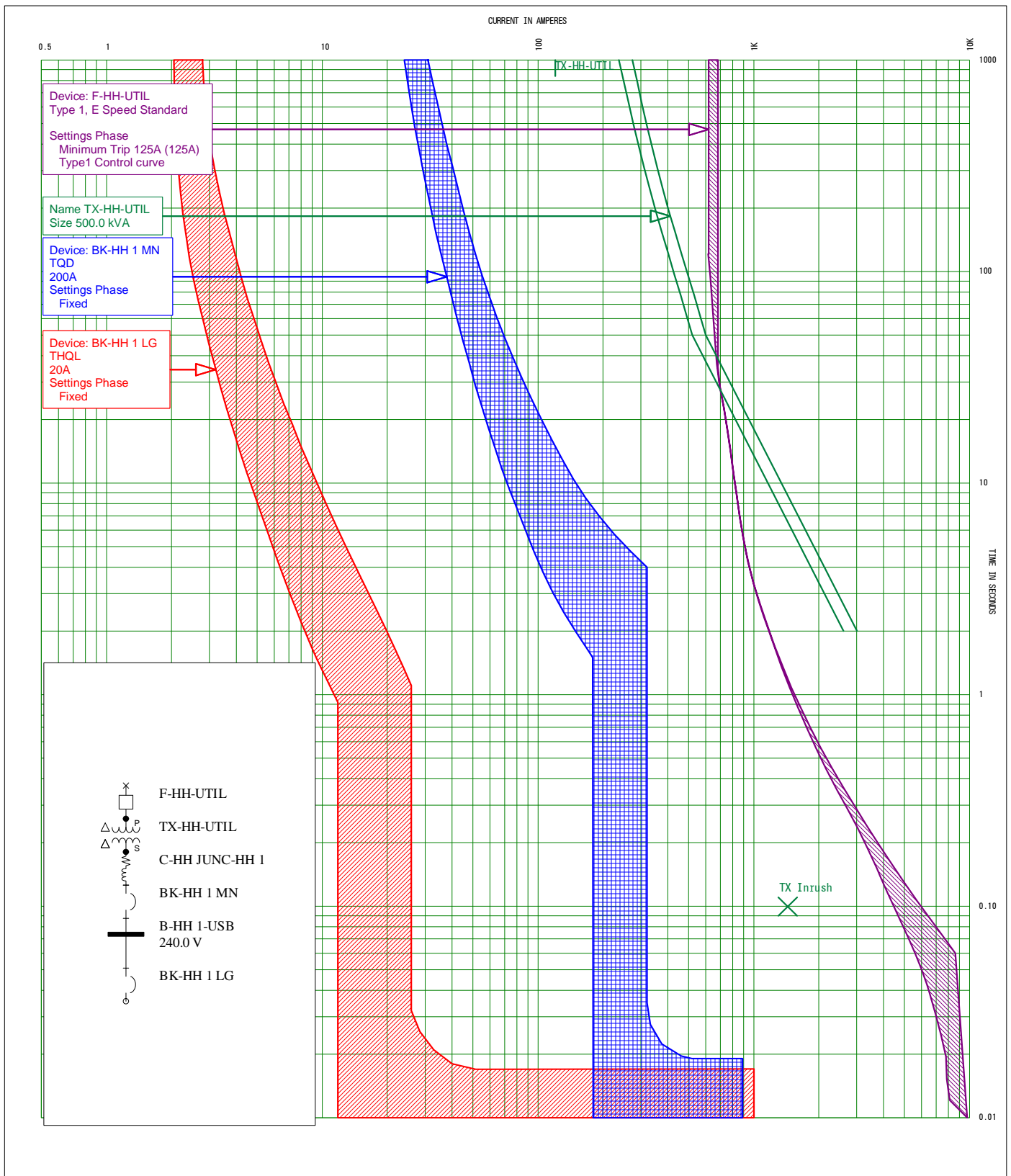
Eaton Electrical Services and Systems
February 21, 2013

Plot name: KNGA
Ref. Voltage: 240V
Current Scale: x 100



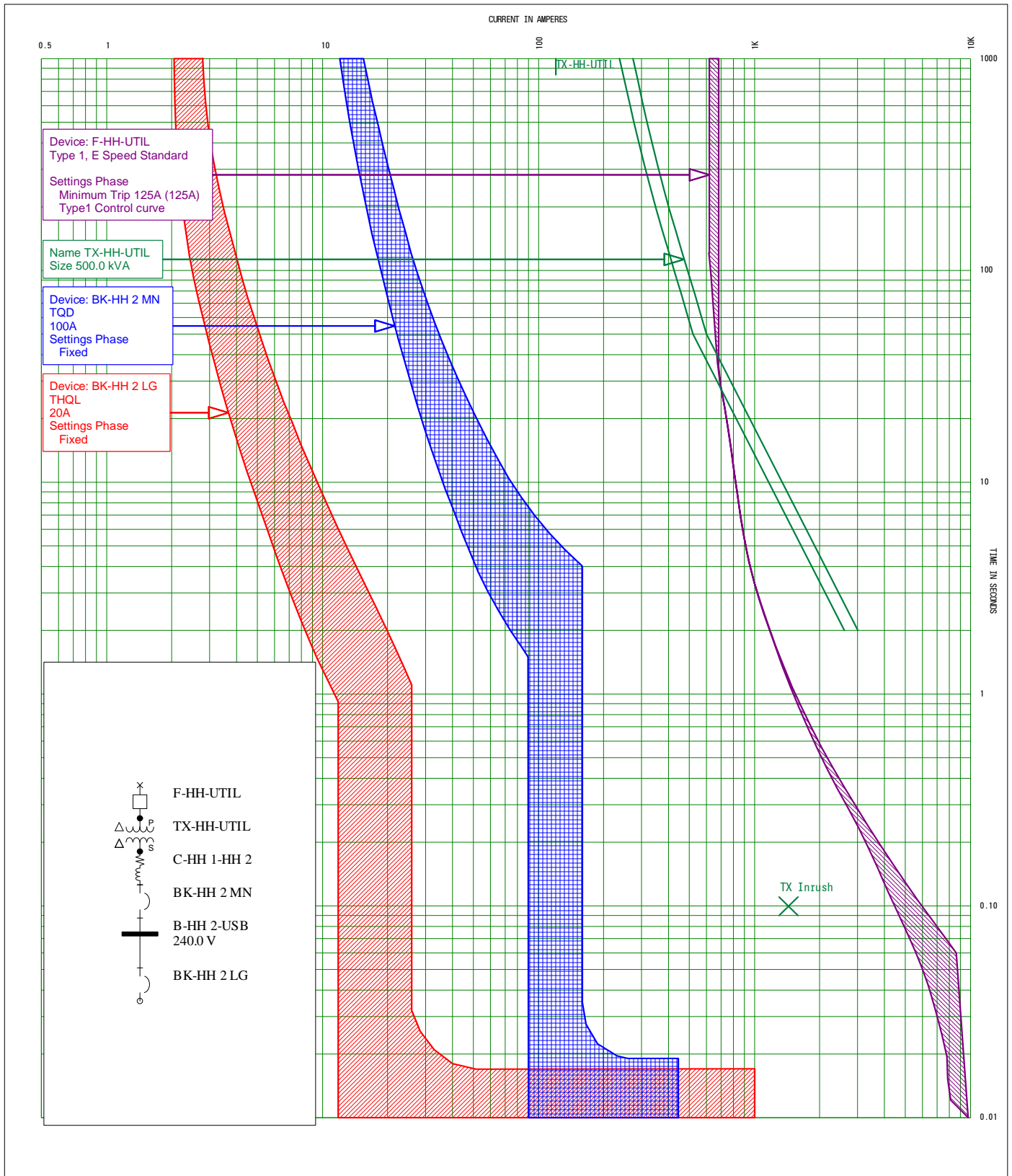
Eaton Electrical Services and Systems
February 21, 2013

Plot name: STFR
Ref. Voltage: 240V
Current Scale: x 100



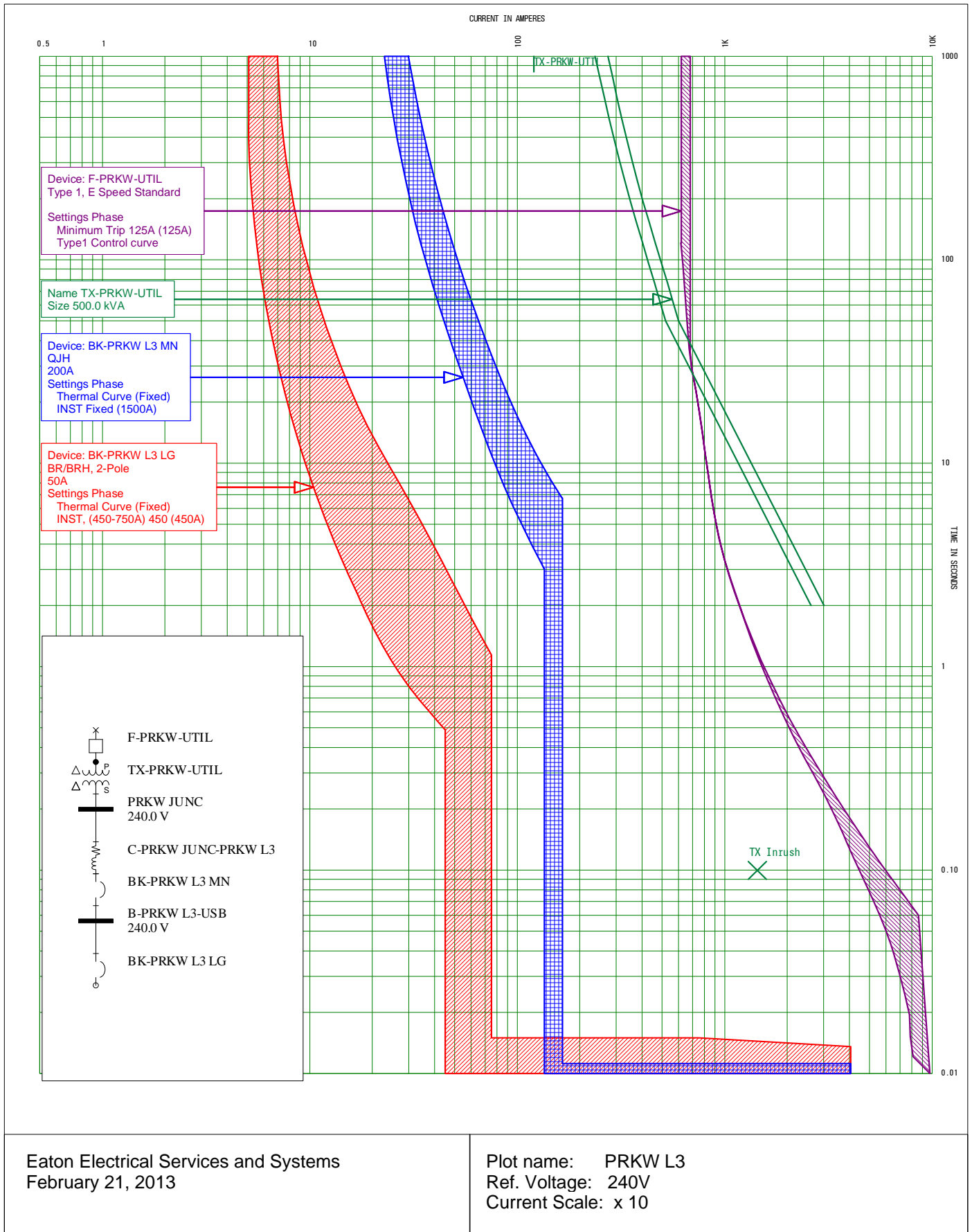
Eaton Electrical Services and Systems
February 21, 2013

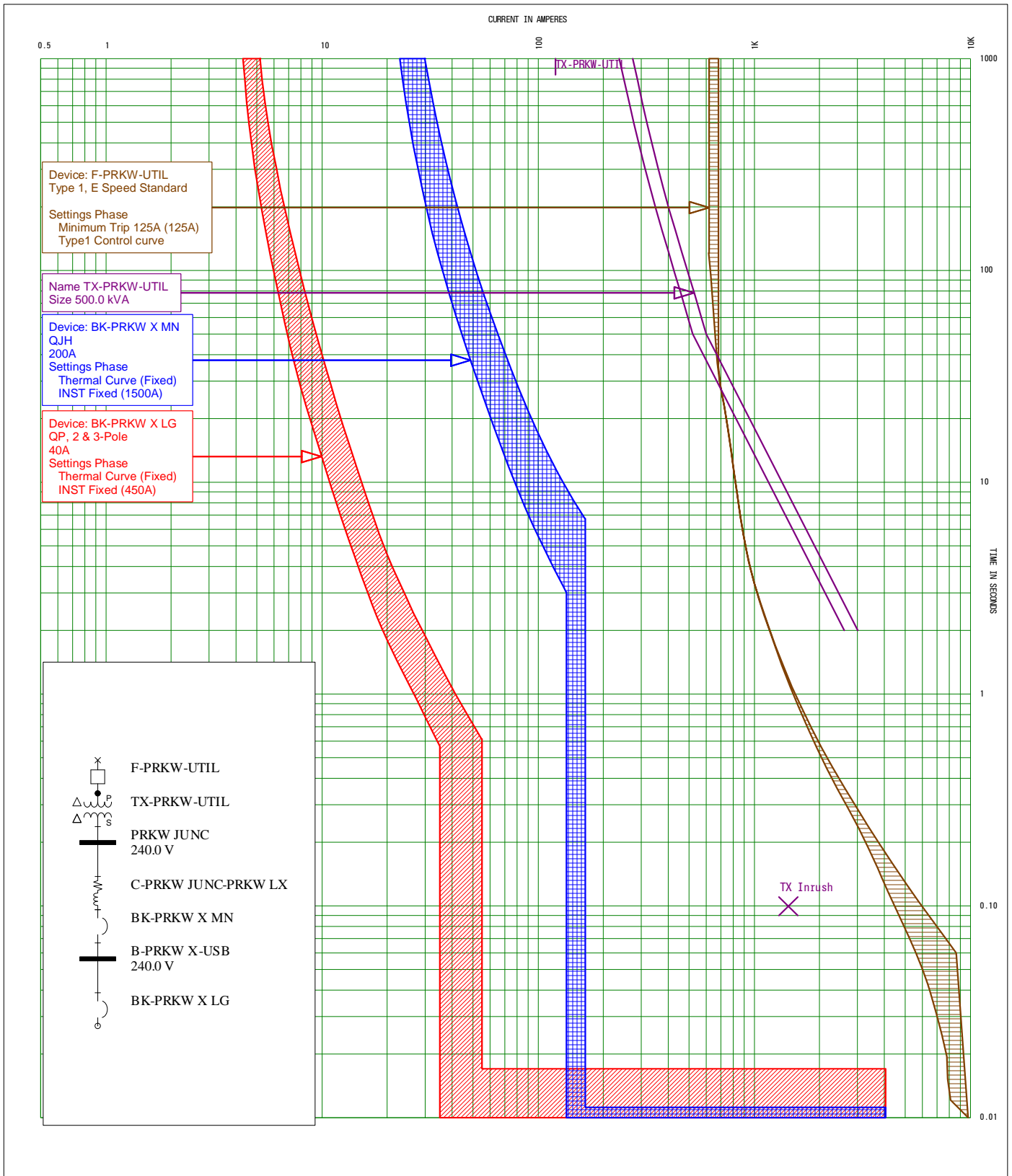
Plot name: HH1
Ref. Voltage: 240V
Current Scale: x 10



Eaton Electrical Services and Systems
February 21, 2013

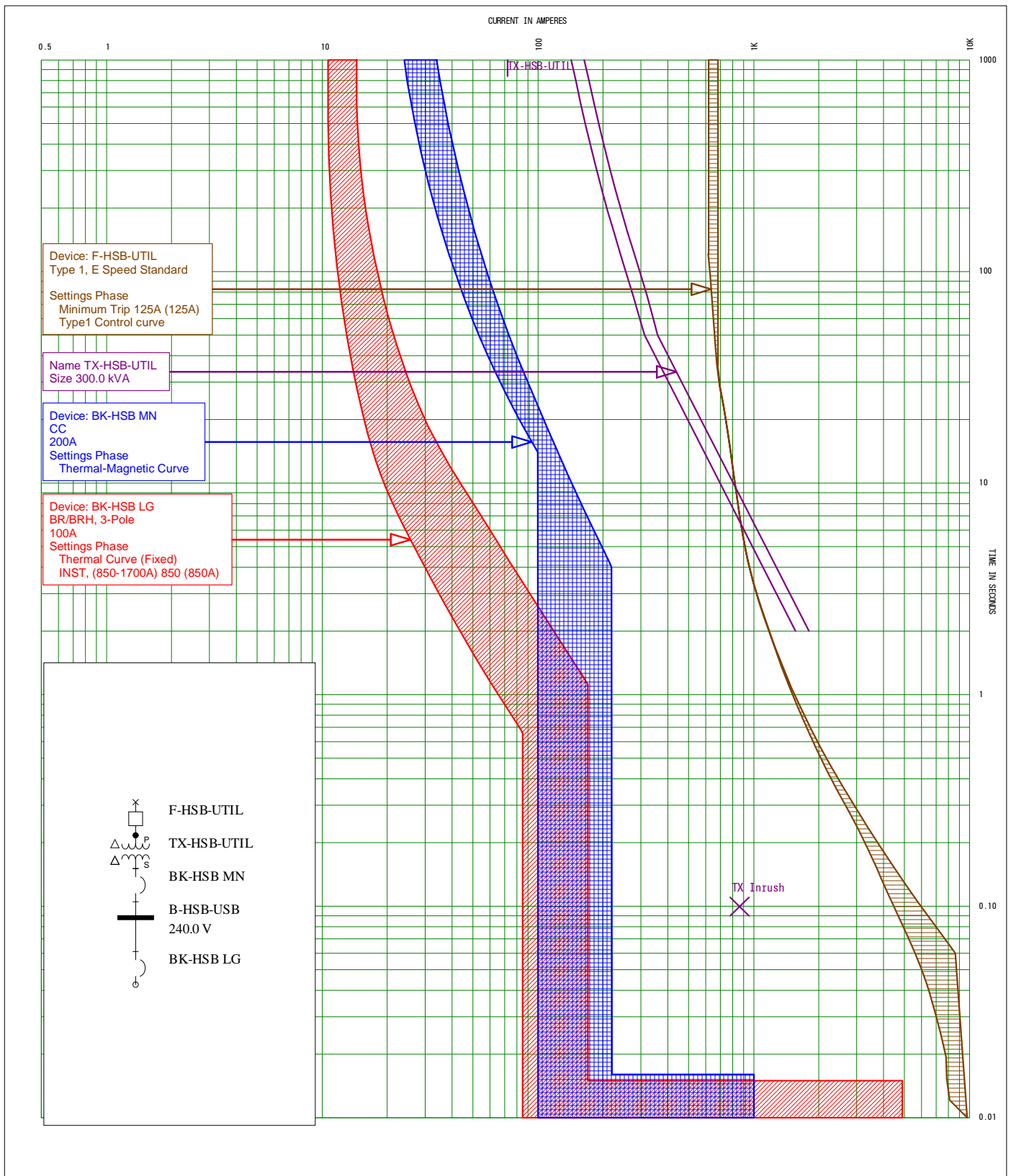
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Ref. Voltage: 240V
Current Scale: x 10





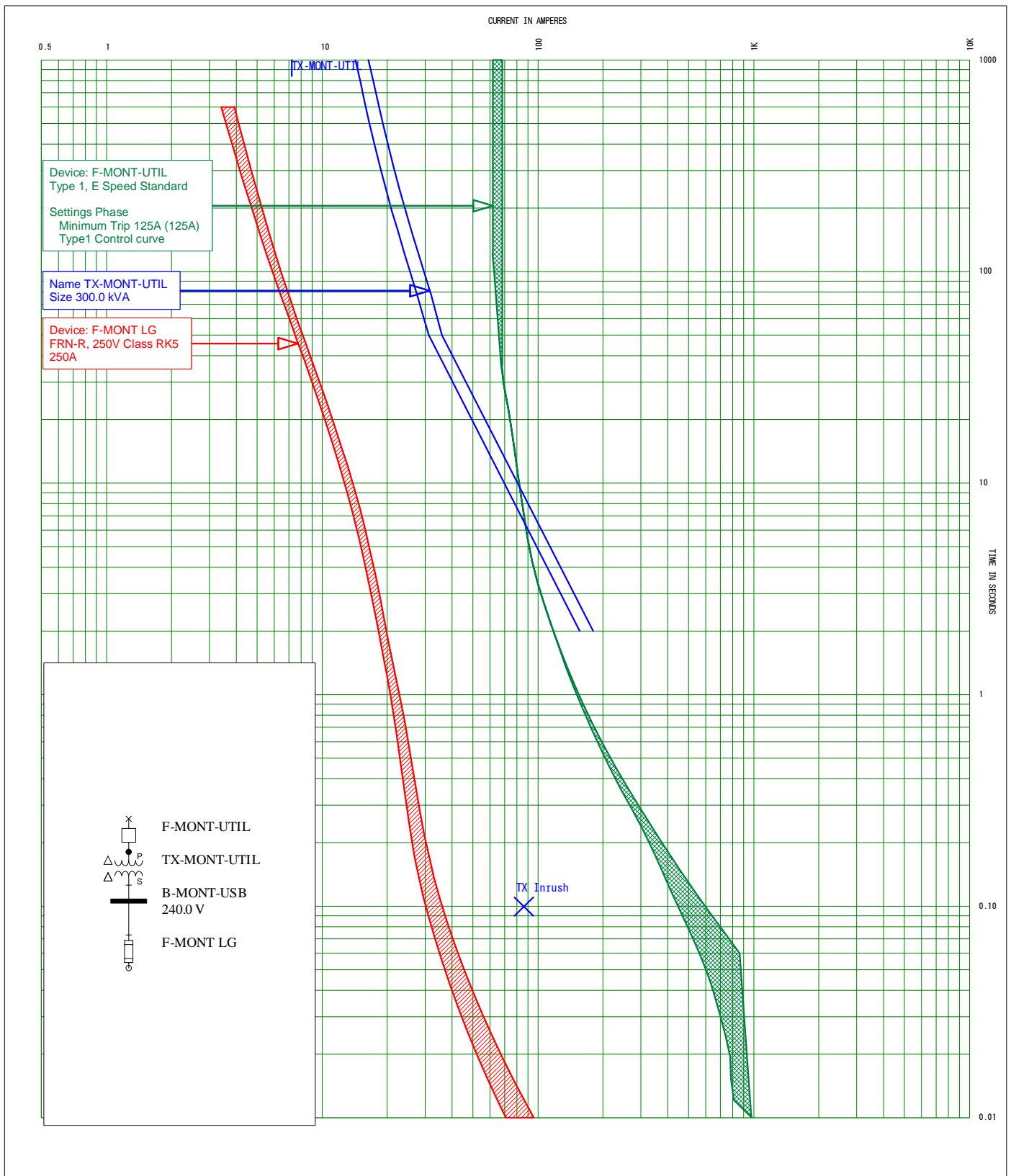
Eaton Electrical Services and Systems
February 21, 2013

Plot name: PRKW X
Ref. Voltage: 240V
Current Scale: x 10



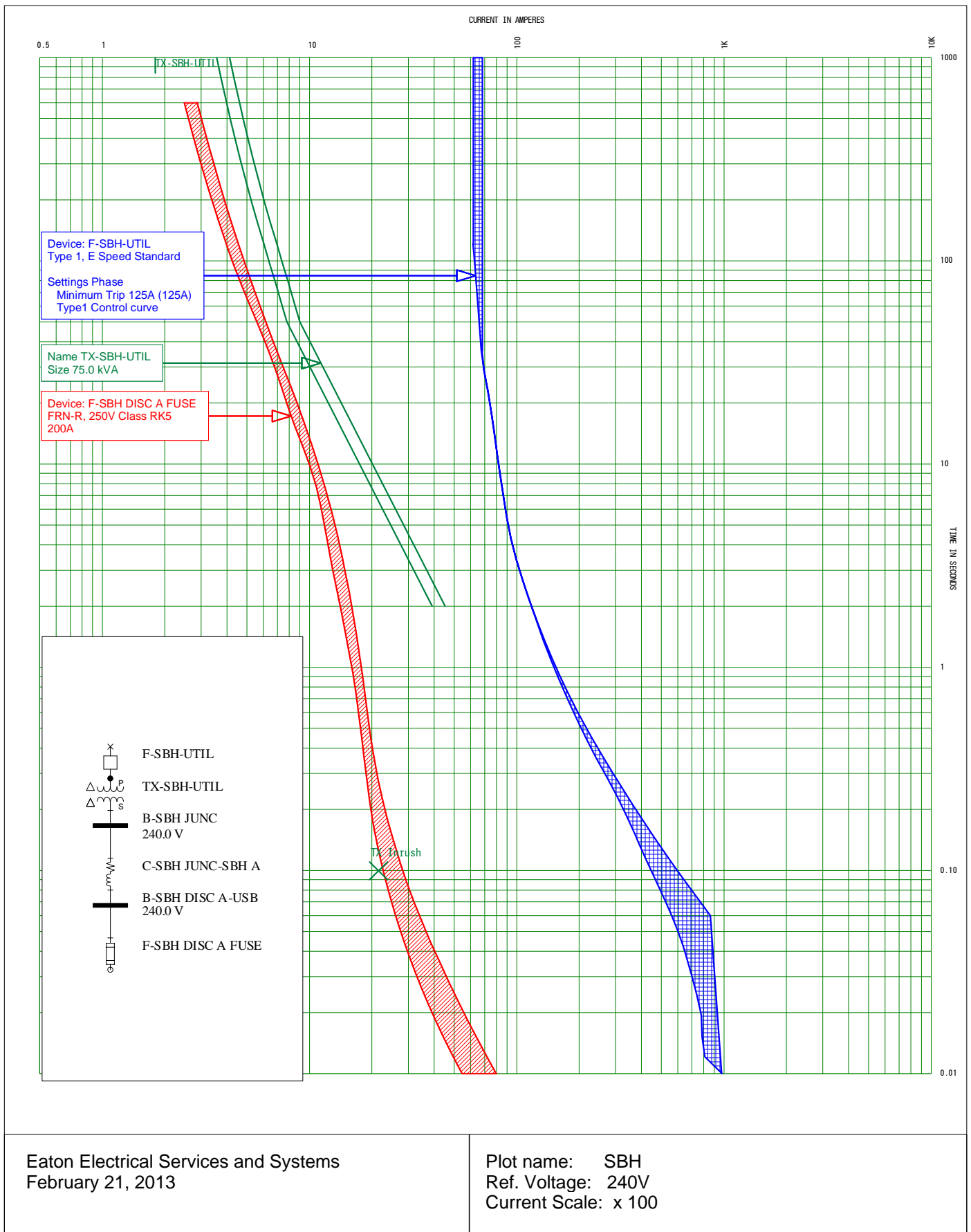
Eaton Electrical Services and Systems
February 21, 2013

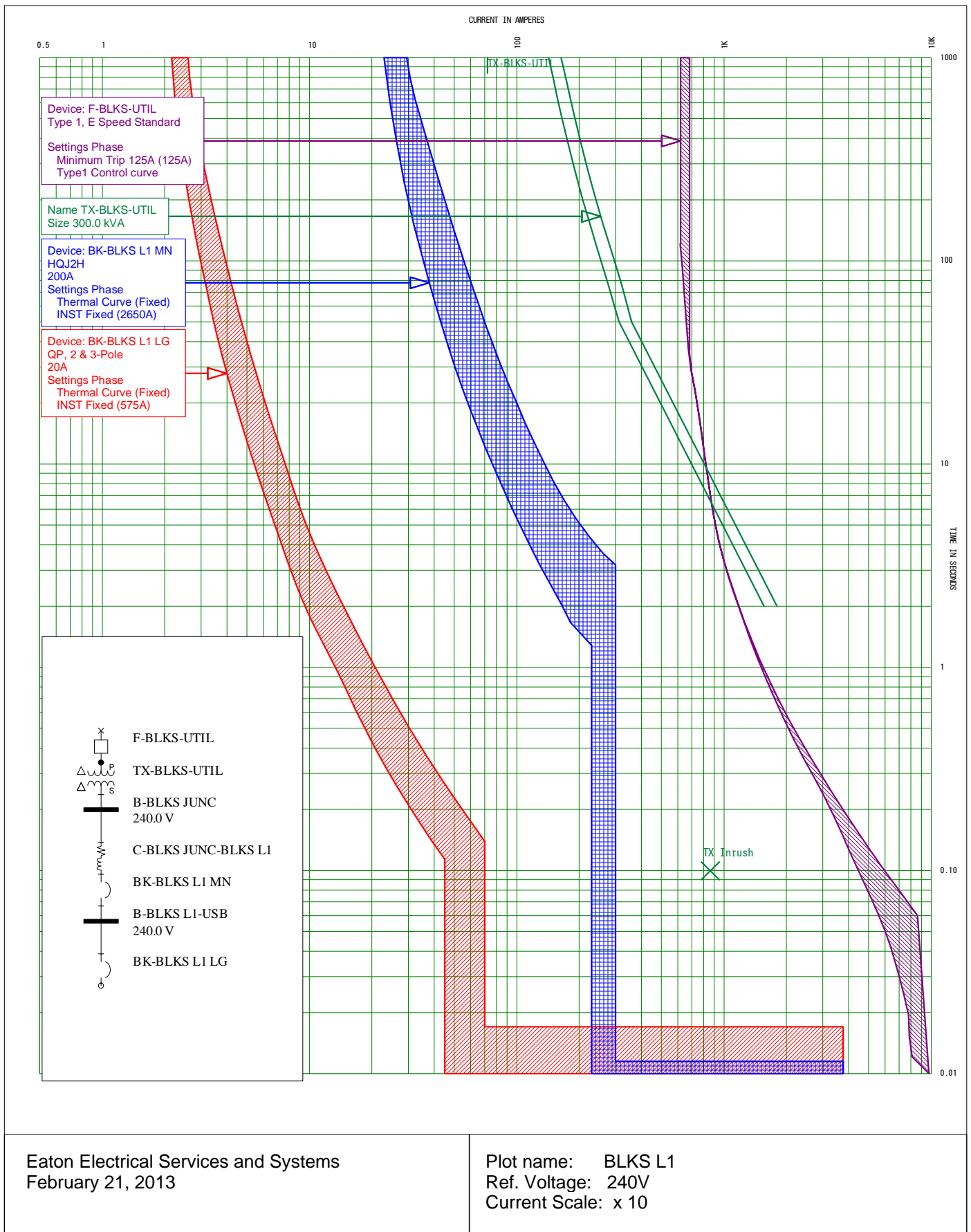
Plot name: HSB
Ref. Voltage: 240V
Current Scale: x 10

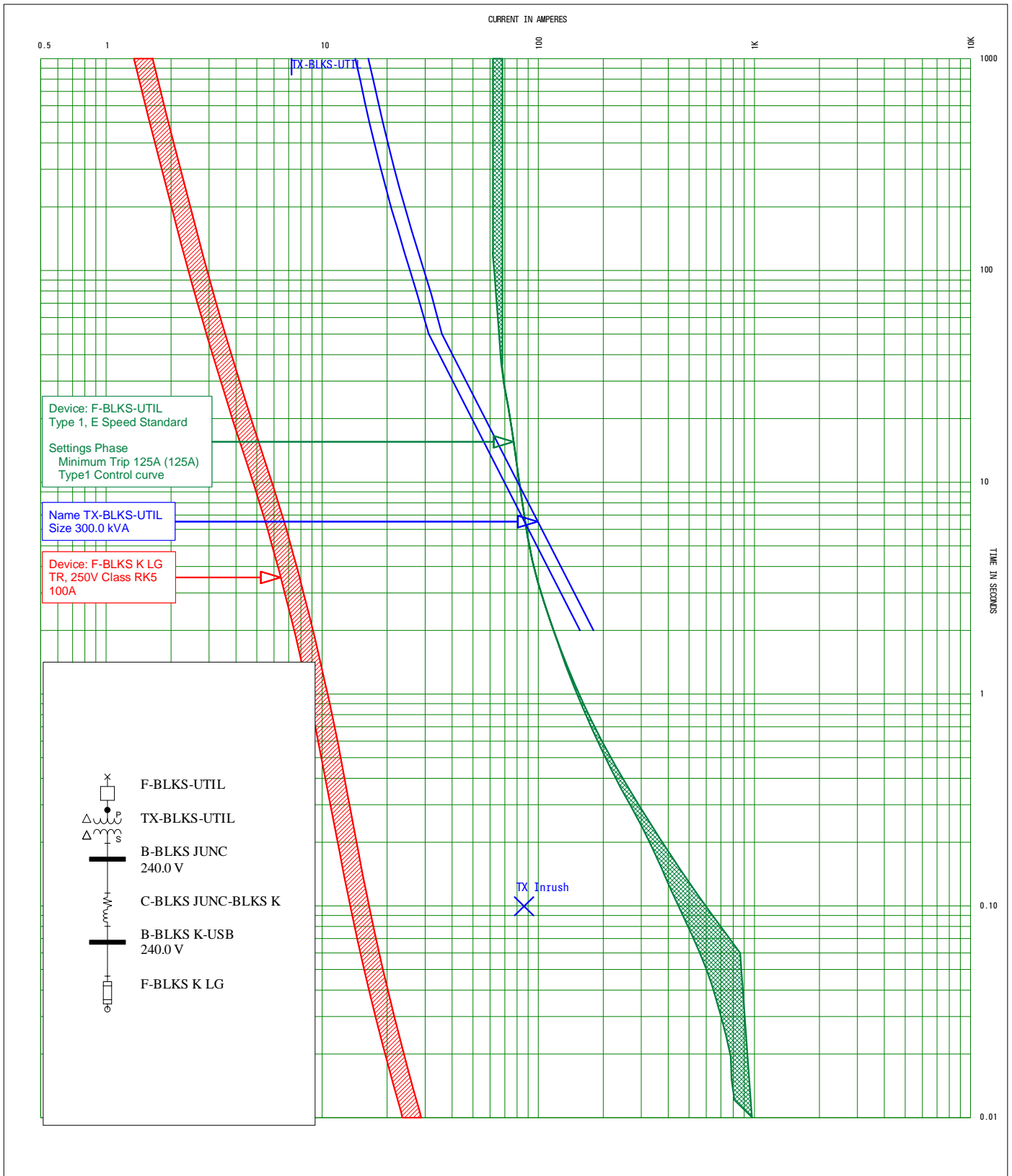


Eaton Electrical Services and Systems
February 21, 2013

Plot name: MONT
Ref. Voltage: 240V
Current Scale: x 100

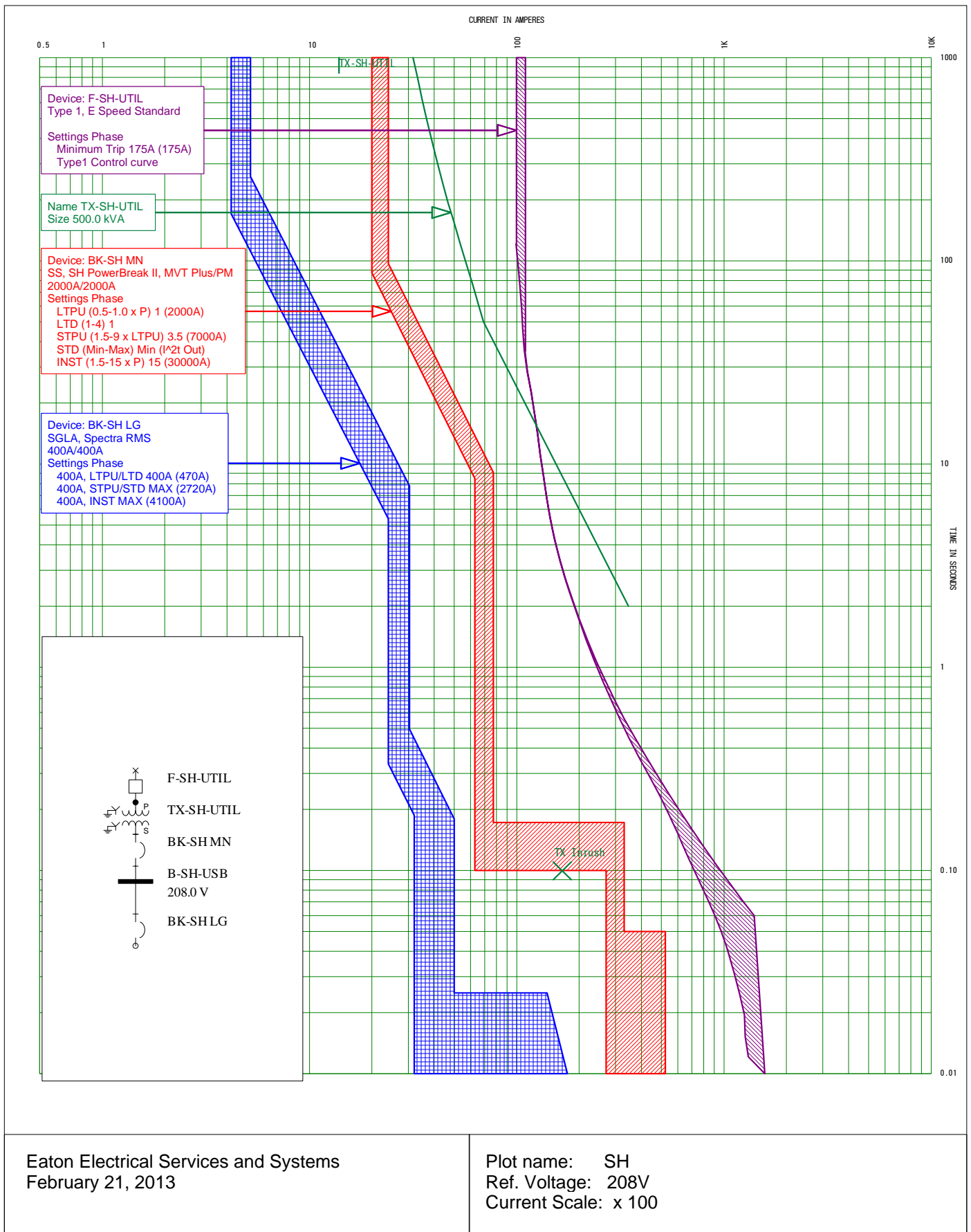


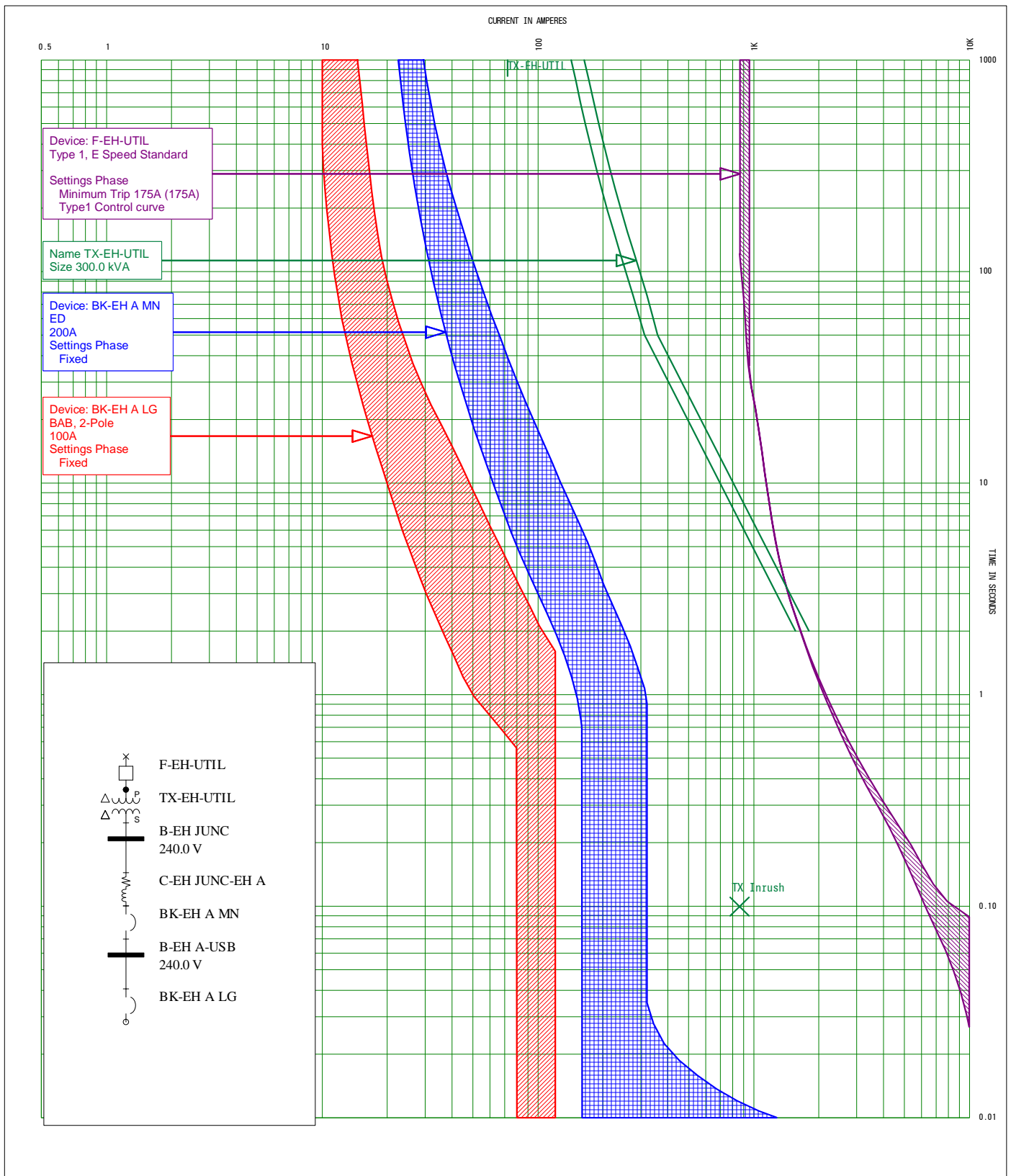




Eaton Electrical Services and Systems
February 21, 2013

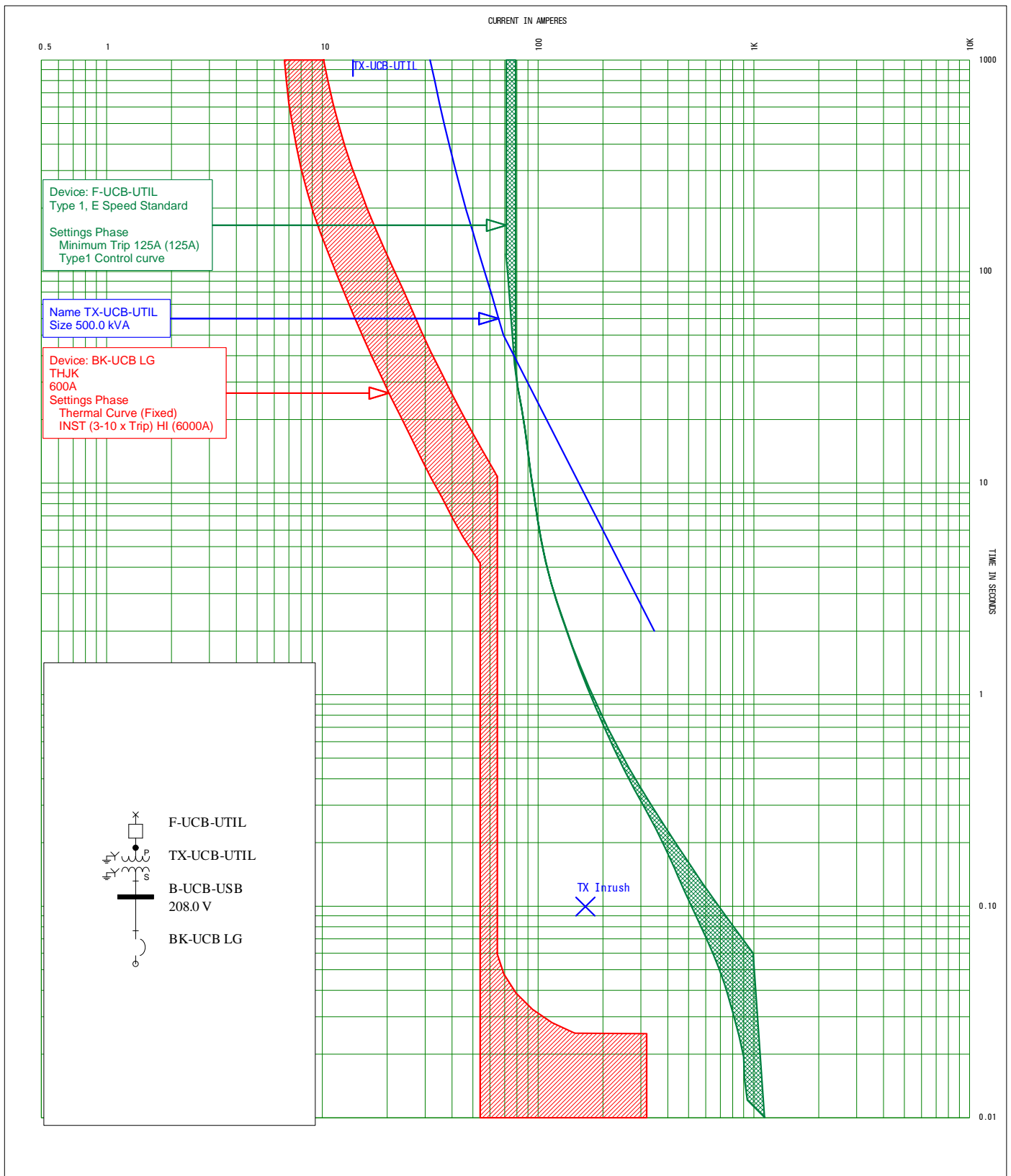
Plot name: BLKS K
Ref. Voltage: 240V
Current Scale: x 100





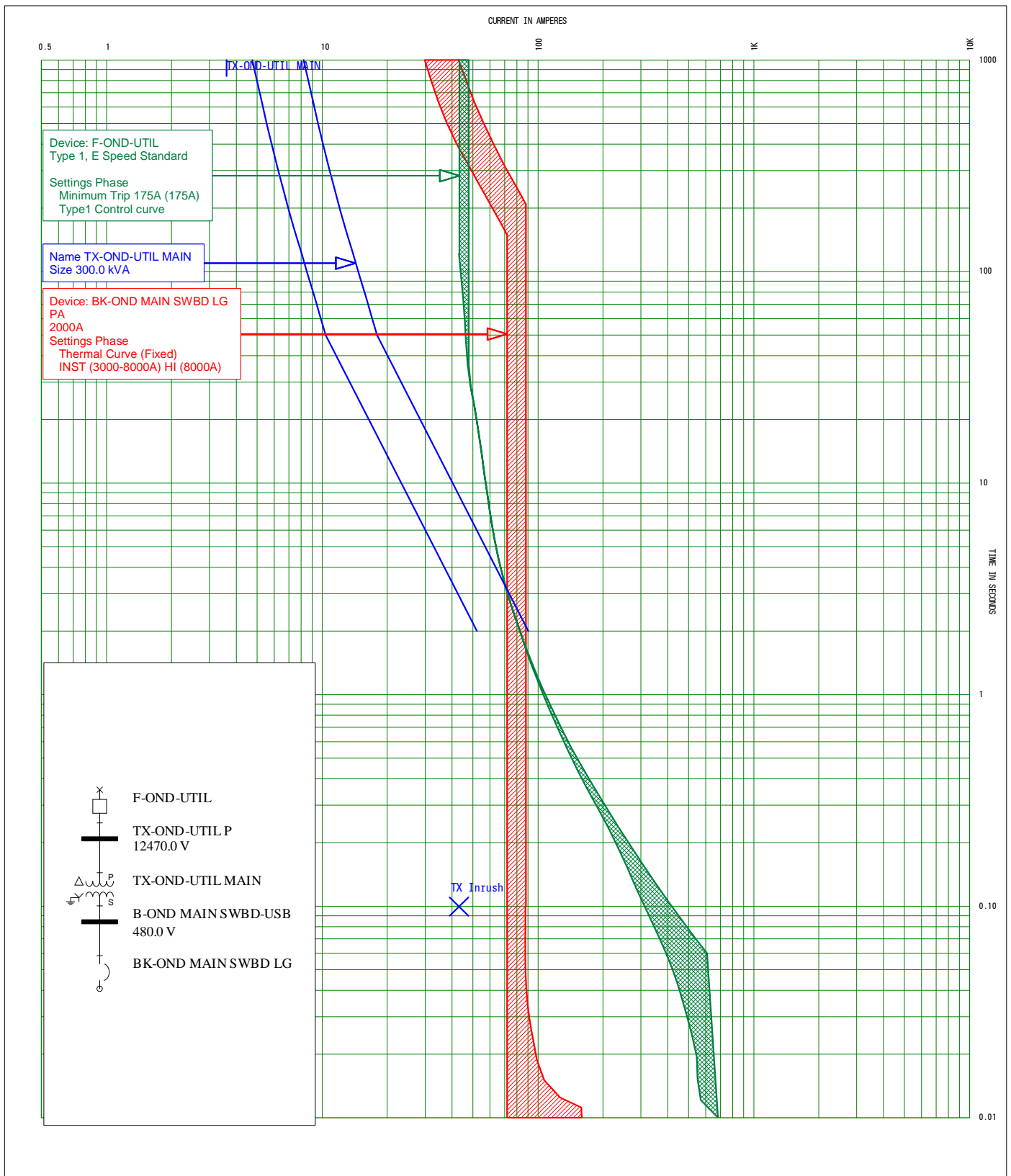
Eaton Electrical Services and Systems
 February 21, 2013

Plot name: EH
 Ref. Voltage: 240V
 Current Scale: x 10



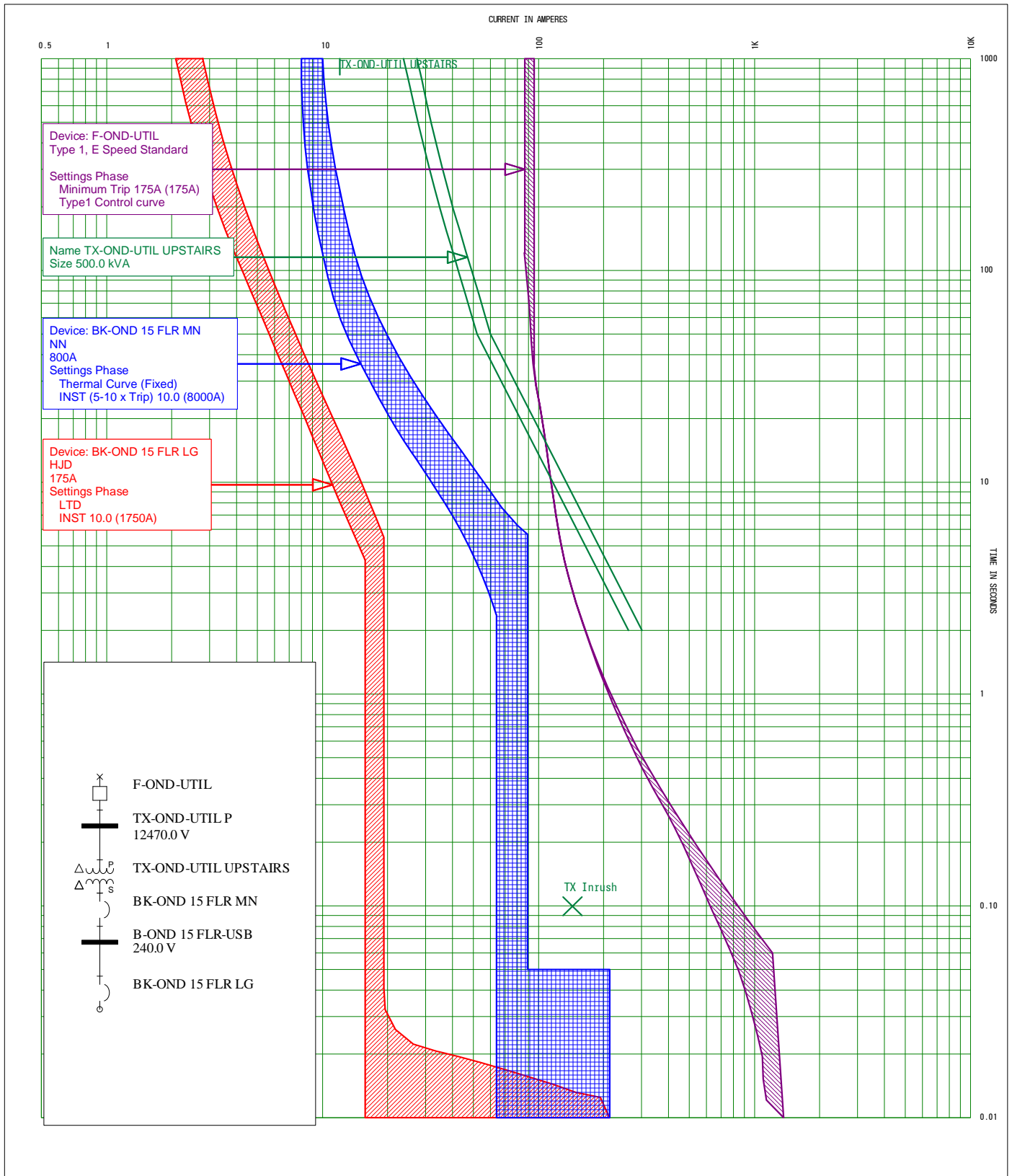
Eaton Electrical Services and Systems
February 21, 2013

Plot name: UCB
Ref. Voltage: 208V
Current Scale: x 100



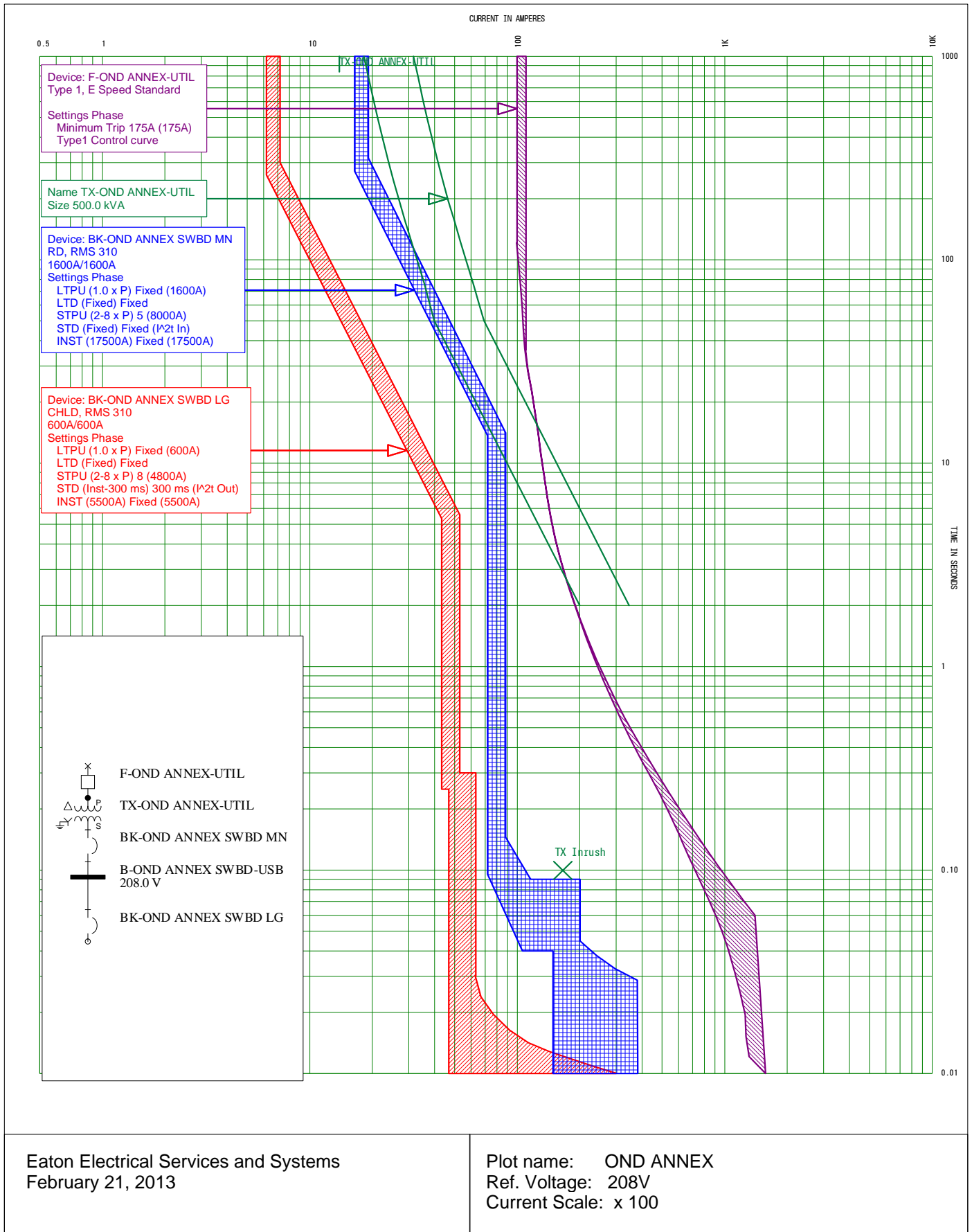
Eaton Electrical Services and Systems
February 21, 2013

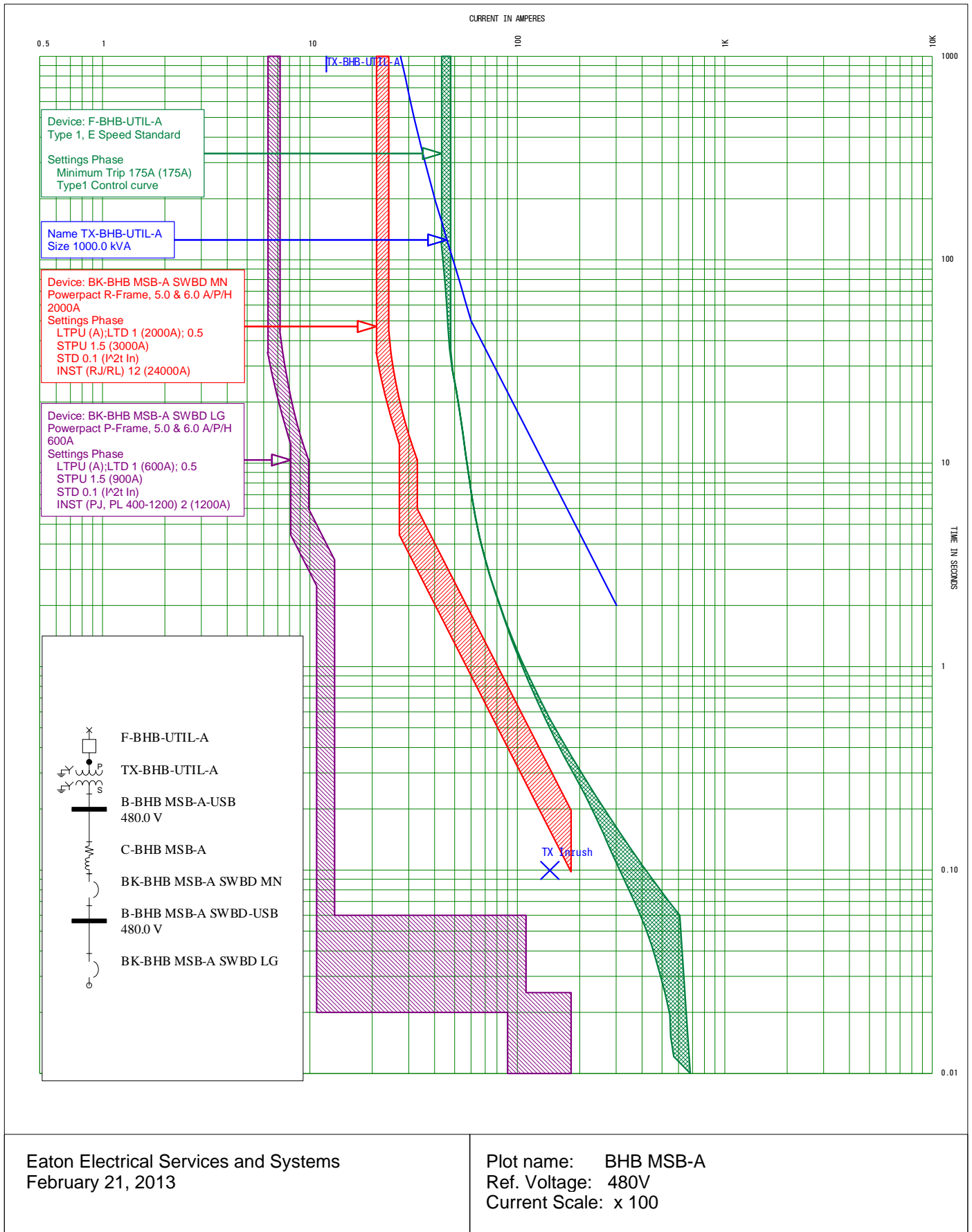
Plot name: OND MAIN
Ref. Voltage: 480V
Current Scale: x 100

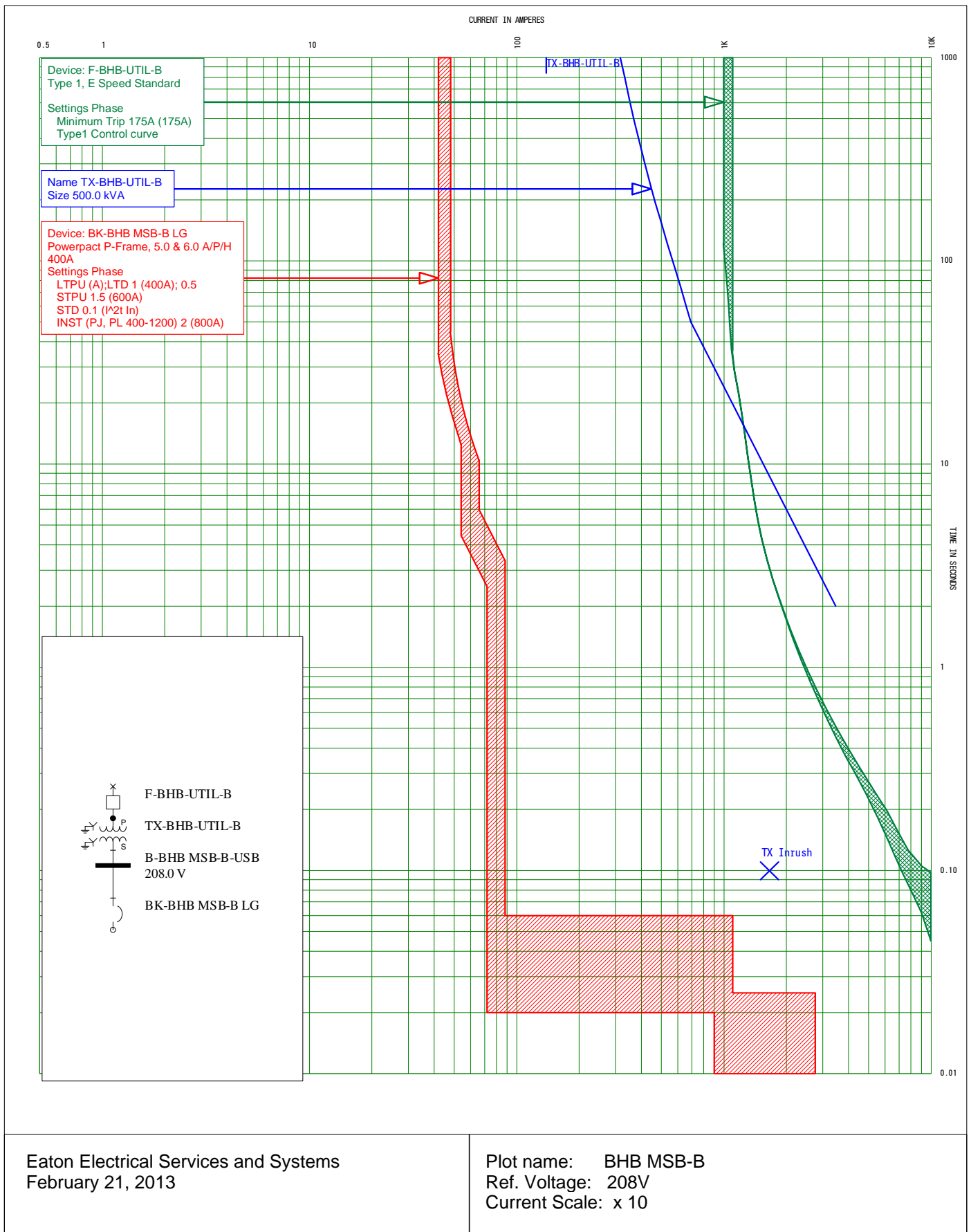


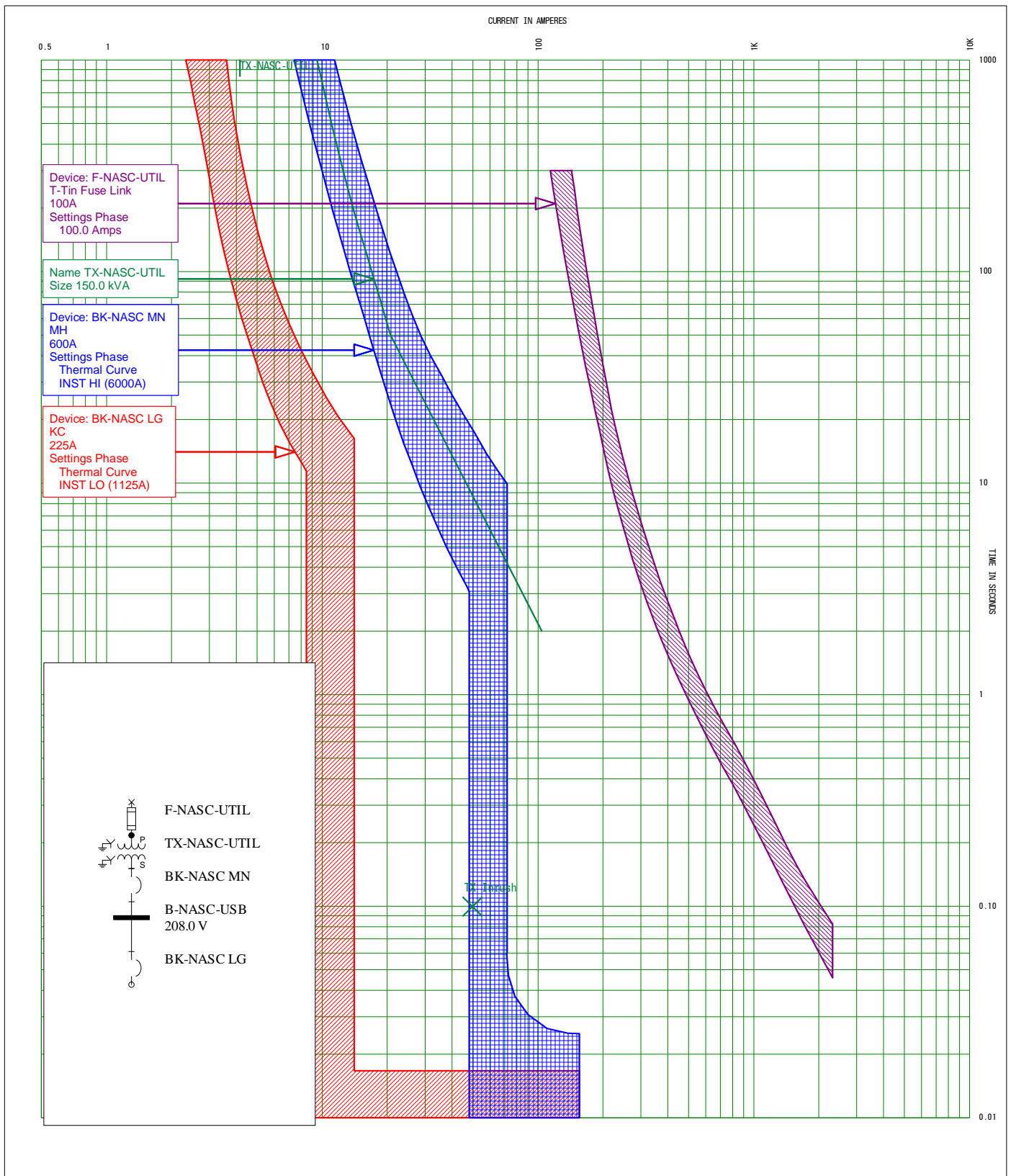
Eaton Electrical Services and Systems
February 21, 2013

Plot name: OND 15TH FLR
Ref. Voltage: 240V
Current Scale: x 100



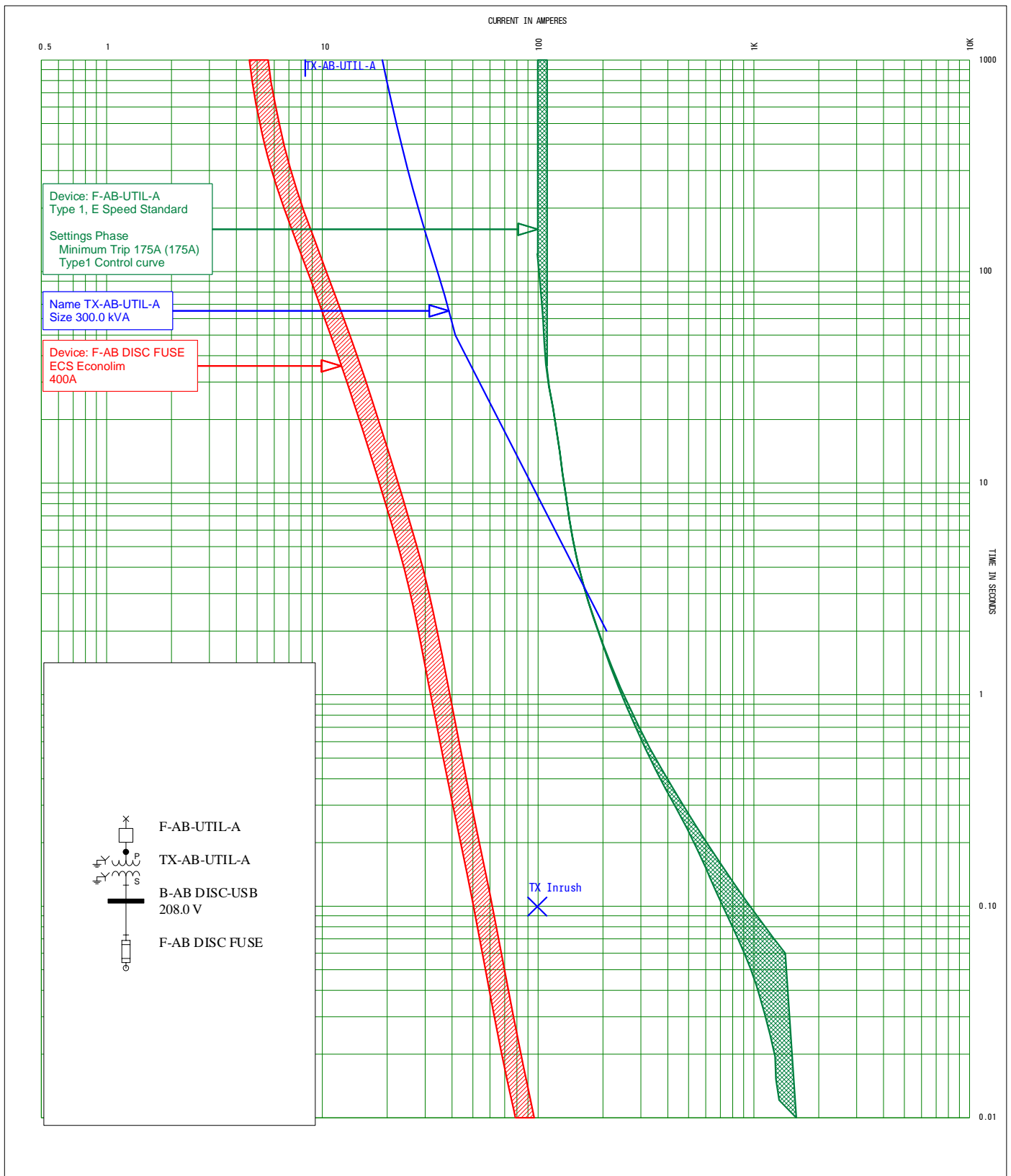






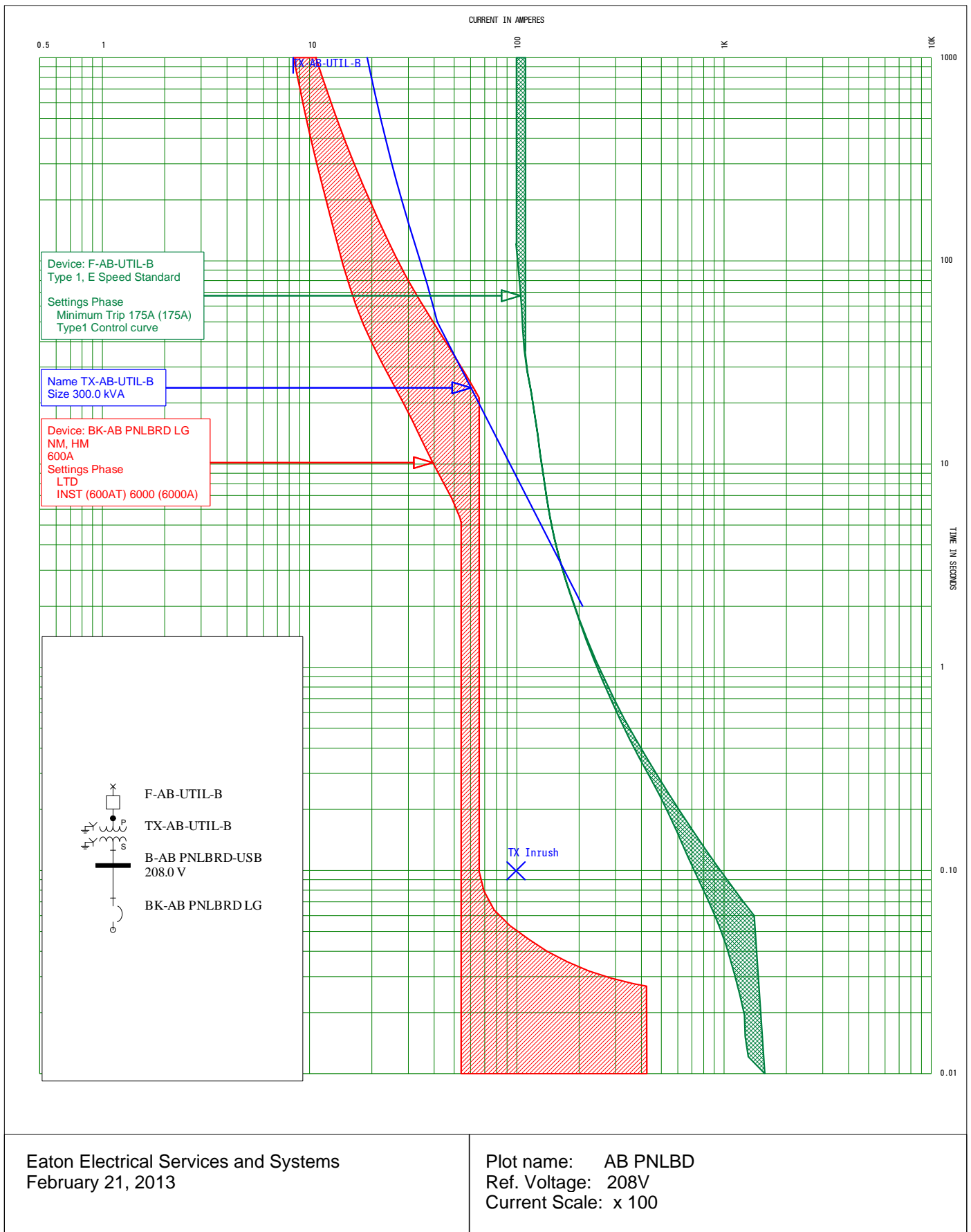
Eaton Electrical Services and Systems
February 21, 2013

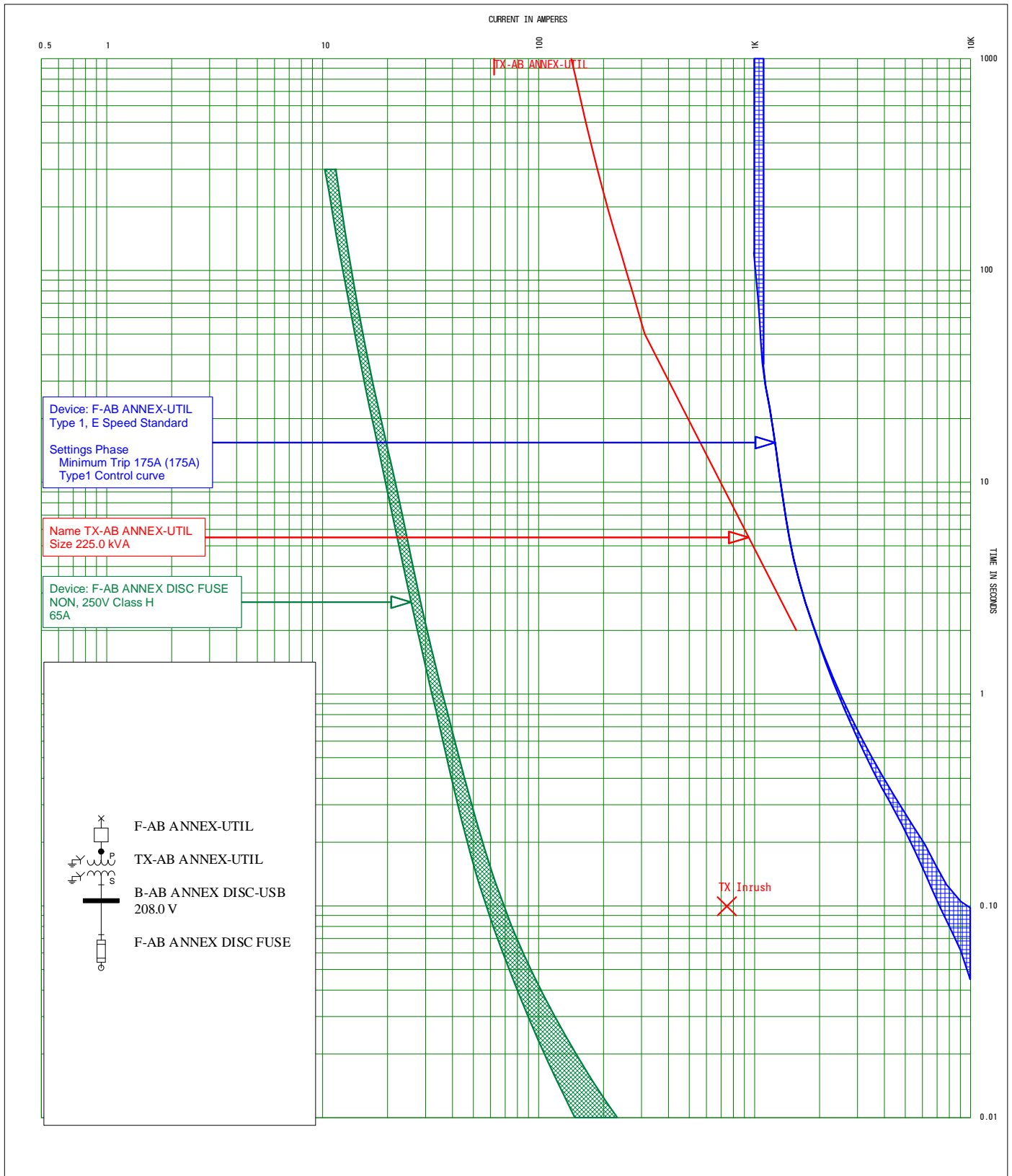
Plot name: NASC
Ref. Voltage: 208V
Current Scale: x 100



Eaton Electrical Services and Systems
February 21, 2013

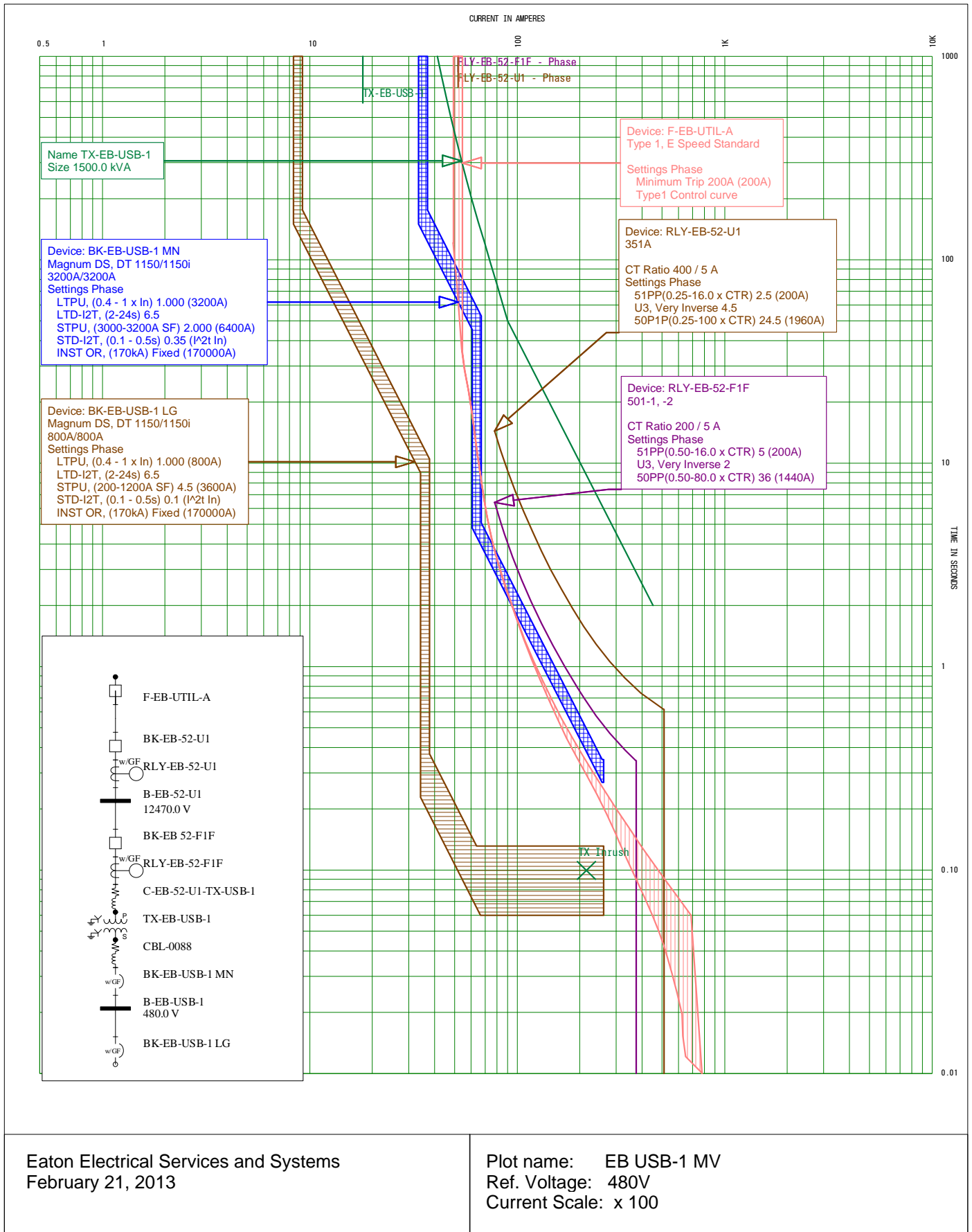
Plot name: AB DISC
Ref. Voltage: 208V
Current Scale: x 100





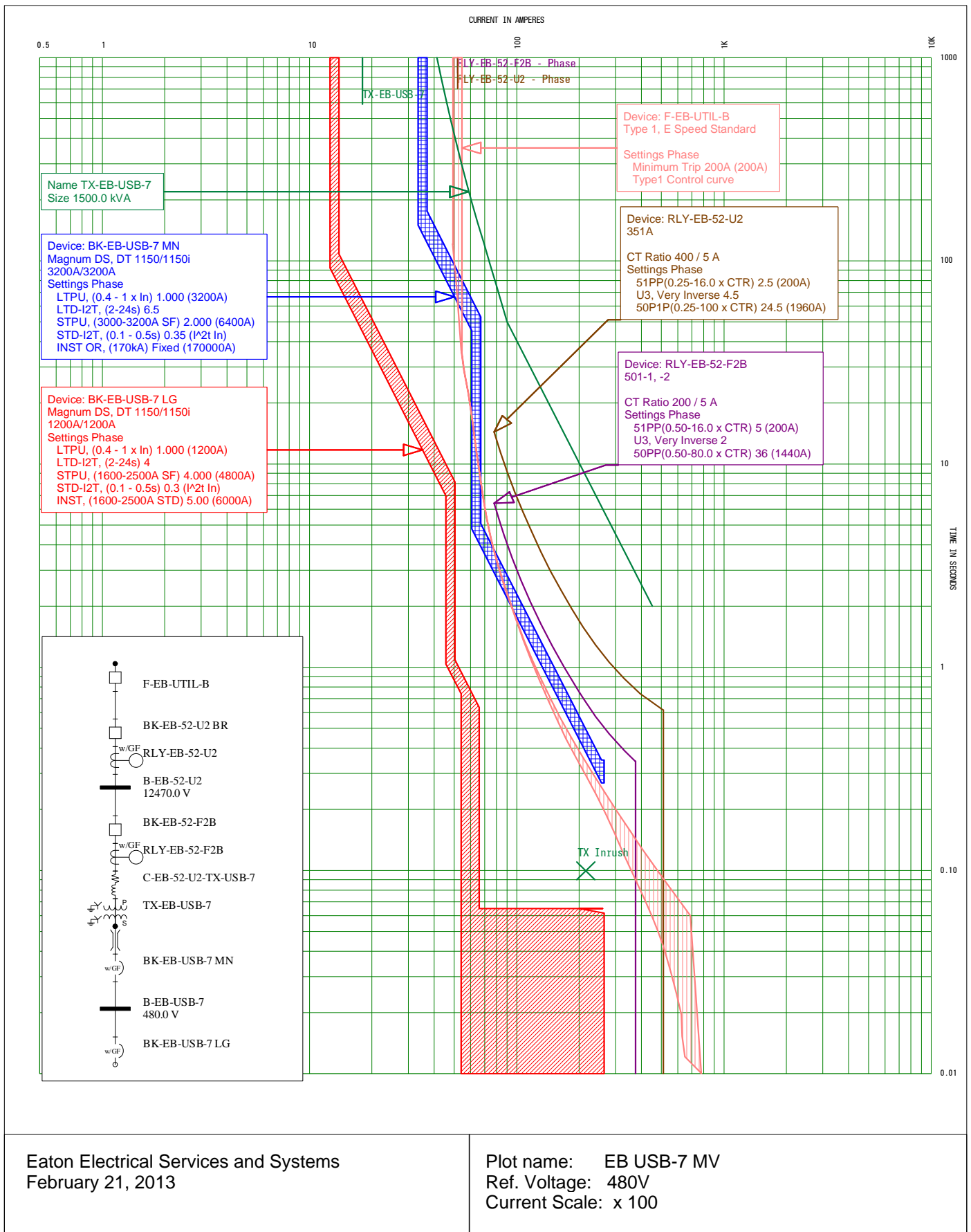
Eaton Electrical Services and Systems
February 21, 2013

Plot name: AB ANNEX
Ref. Voltage: 208V
Current Scale: x 10



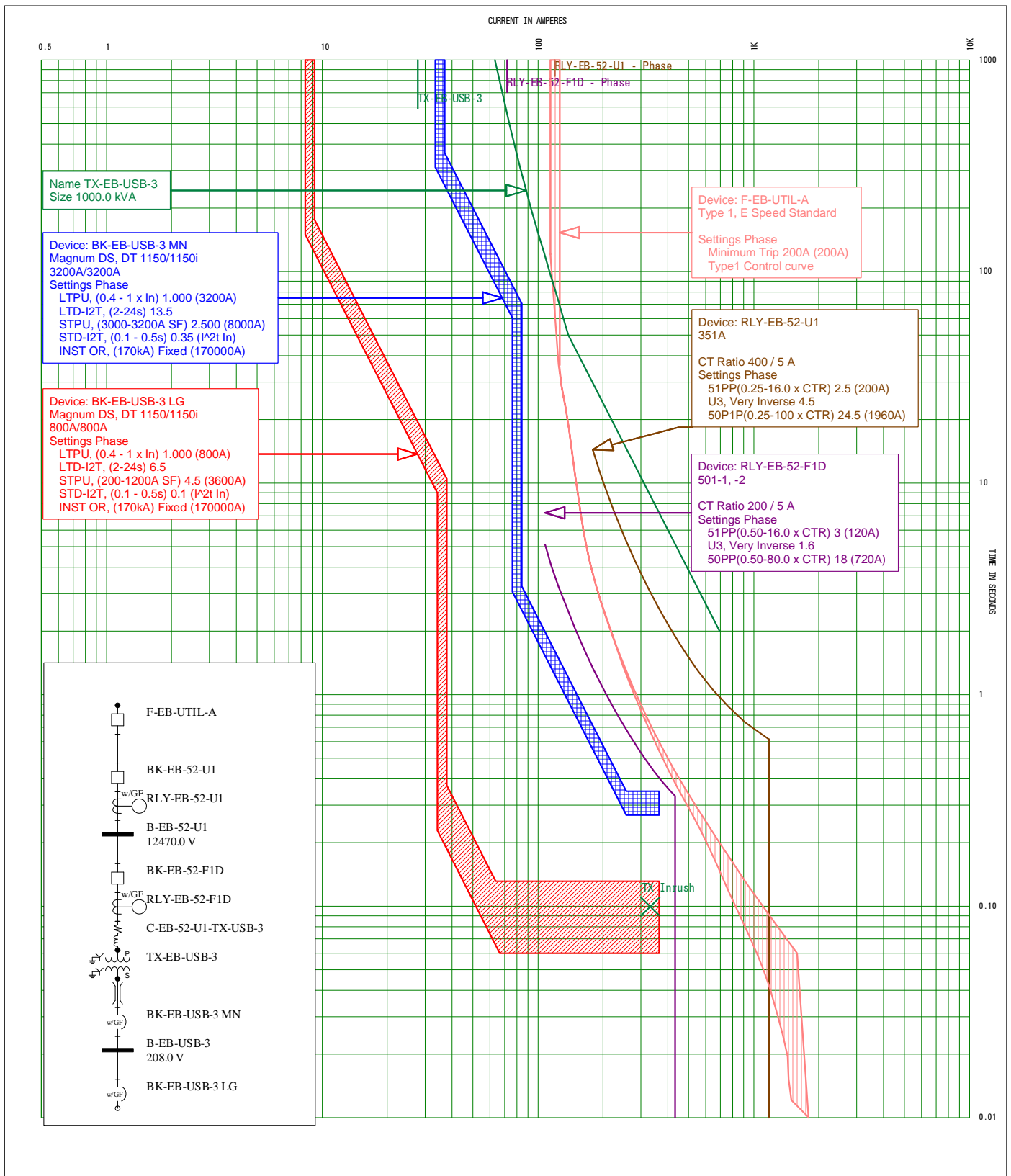
Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB USB-1 MV
Ref. Voltage: 480V
Current Scale: x 100



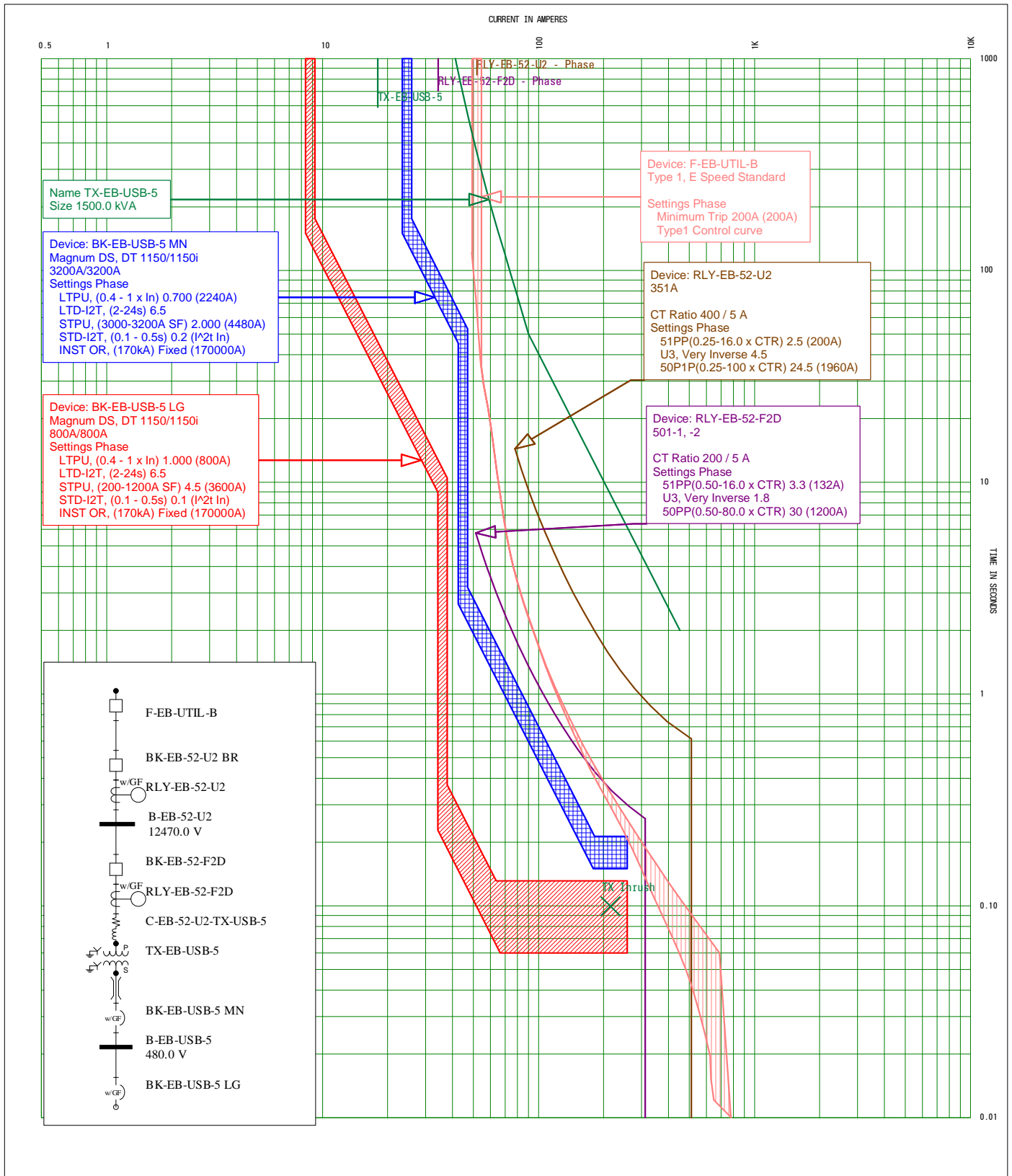
Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB USB-7 MV
Ref. Voltage: 480V
Current Scale: x 100



Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB USB-3
Ref. Voltage: 208V
Current Scale: x 100



Name TX-EB-USB-5
Size 1500.0 kVA

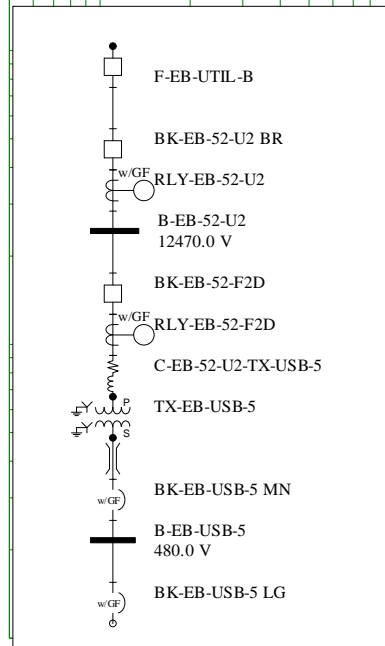
Device: BK-EB-USB-5 MN
Magnum DS, DT 1150/1150i
3200A/3200A
Settings Phase
LTPU, (0.4 - 1 x In) 0.700 (2240A)
LTD-I2T, (2-24s) 6.5
STPU, (3000-3200A SF) 2.000 (4480A)
STD-I2T, (0.1 - 0.5s) 0.2 (I²t In)
INST OR, (170kA) Fixed (170000A)

Device: BK-EB-USB-5 LG
Magnum DS, DT 1150/1150i
800A/800A
Settings Phase
LTPU, (0.4 - 1 x In) 1.000 (800A)
LTD-I2T, (2-24s) 6.5
STPU, (200-1200A SF) 4.5 (3600A)
STD-I2T, (0.1 - 0.5s) 0.1 (I²t In)
INST OR, (170kA) Fixed (170000A)

Device: F-EB-UTIL-B
Type 1, E Speed Standard
Settings Phase
Minimum Trip 200A (200A)
Type1 Control curve

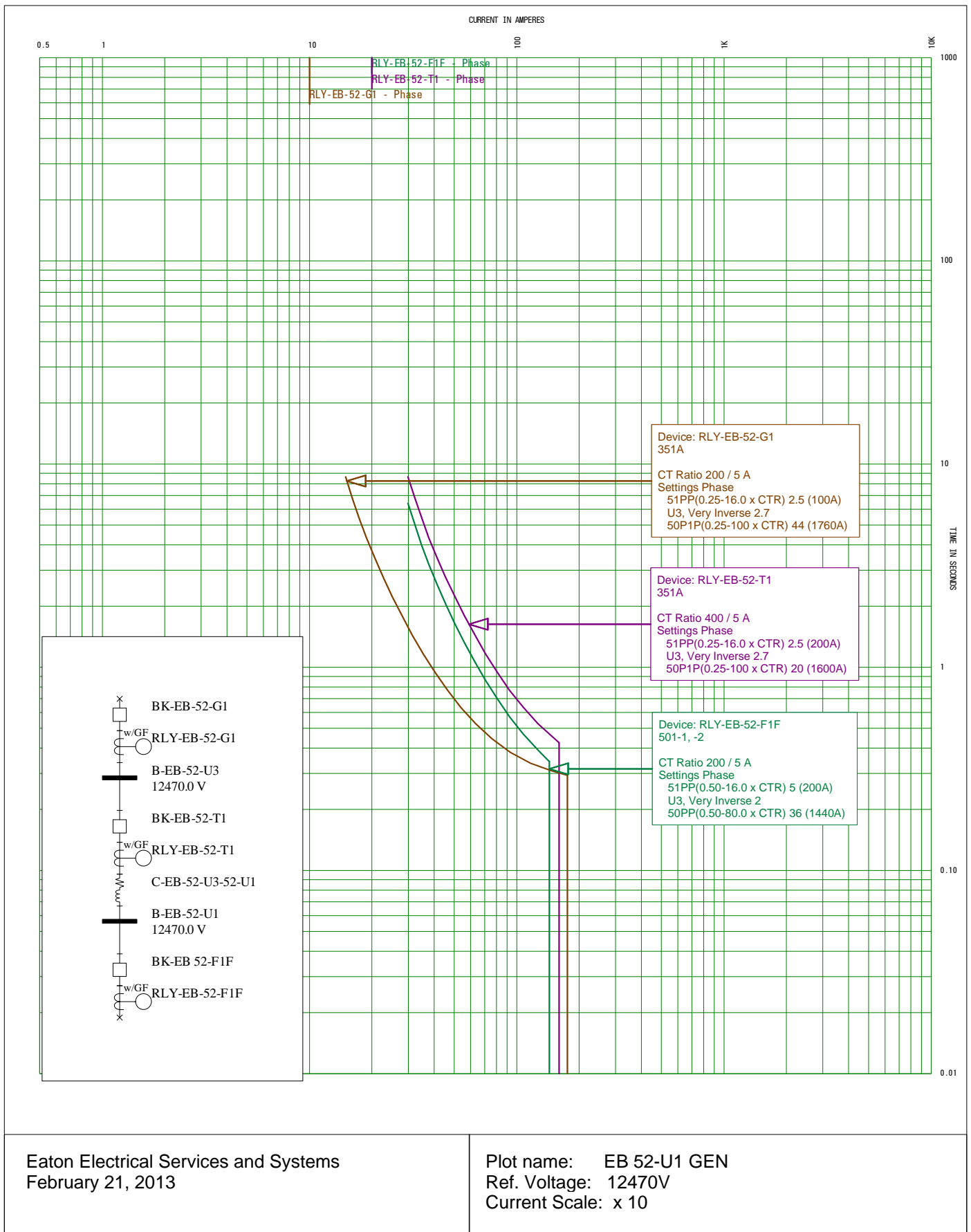
Device: RLY-EB-52-U2
351A
CT Ratio 400 / 5 A
Settings Phase
51PP(0.25-16.0 x CTR) 2.5 (200A)
U3, Very Inverse 4.5
50P1P(0.25-100 x CTR) 24.5 (1960A)

Device: RLY-EB-52-F2D
501-1, -2
CT Ratio 200 / 5 A
Settings Phase
51PP(0.50-16.0 x CTR) 3.3 (132A)
U3, Very Inverse 1.8
50P1P(0.25-80.0 x CTR) 30 (1200A)



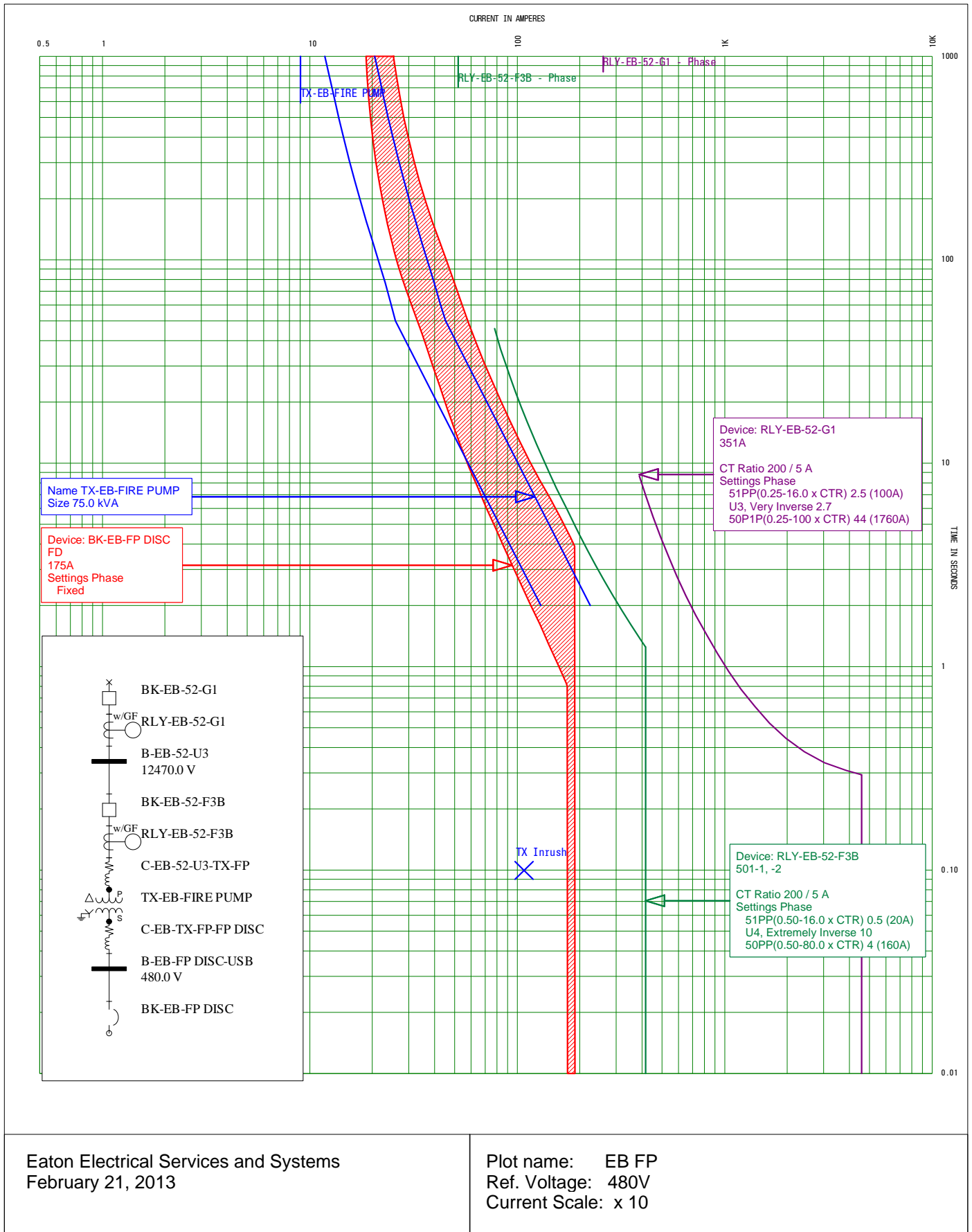
Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB USB-5
Ref. Voltage: 480V
Current Scale: x 100



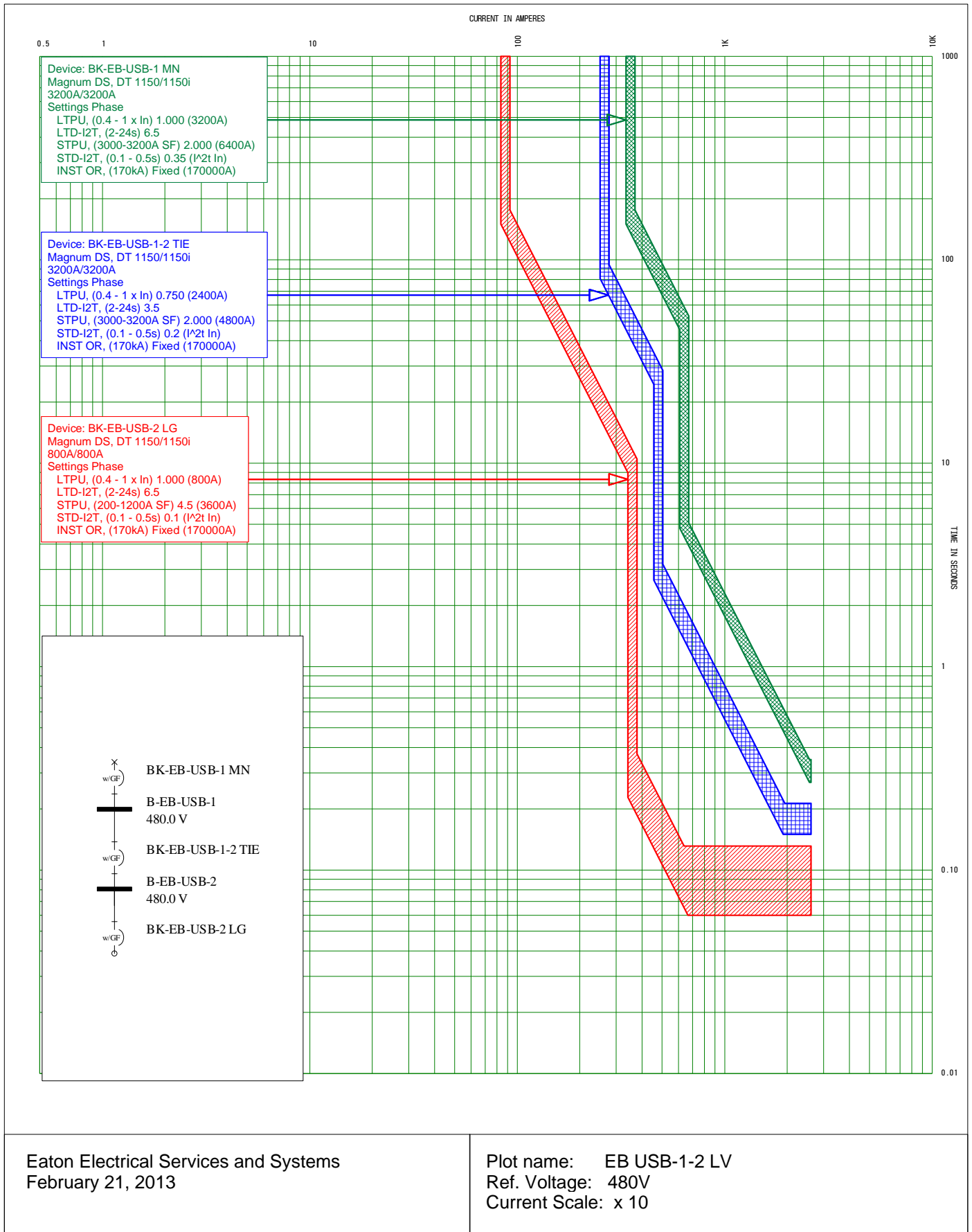
Eaton Electrical Services and Systems
February 21, 2013

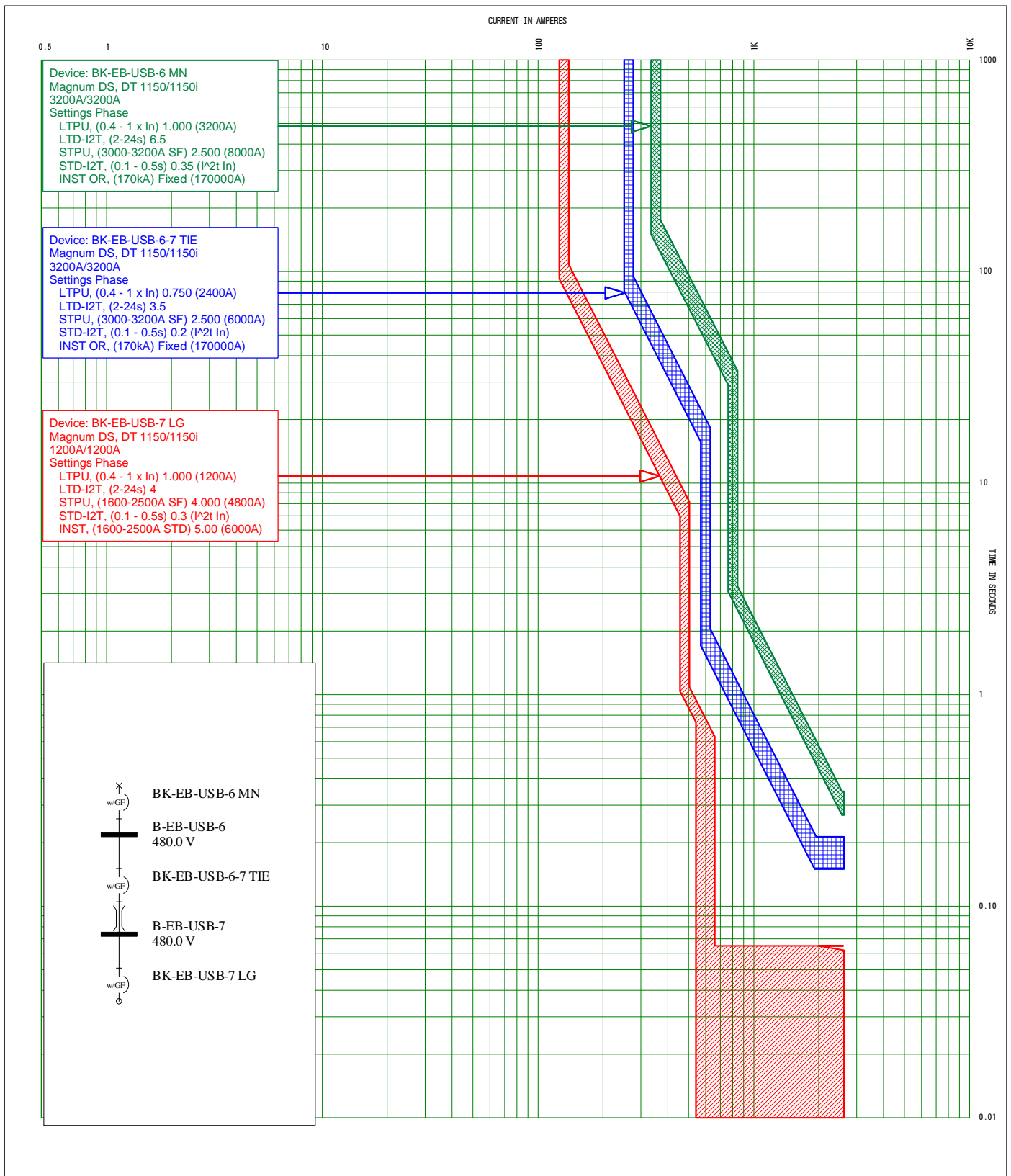
Plot name: EB 52-U1 GEN
Ref. Voltage: 12470V
Current Scale: x 10



Eaton Electrical Services and Systems
February 21, 2013

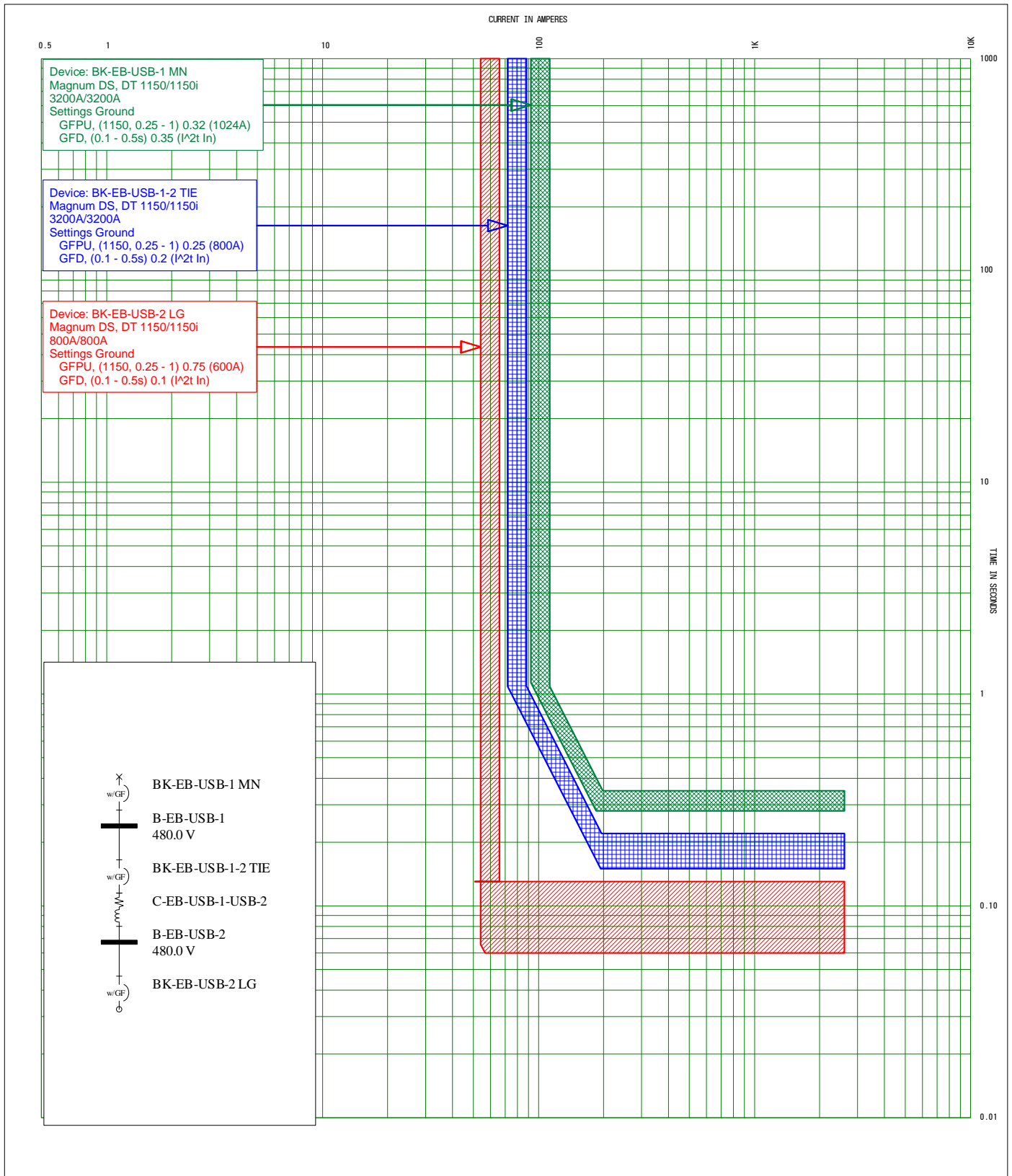
Plot name: EB FP
Ref. Voltage: 480V
Current Scale: x 10





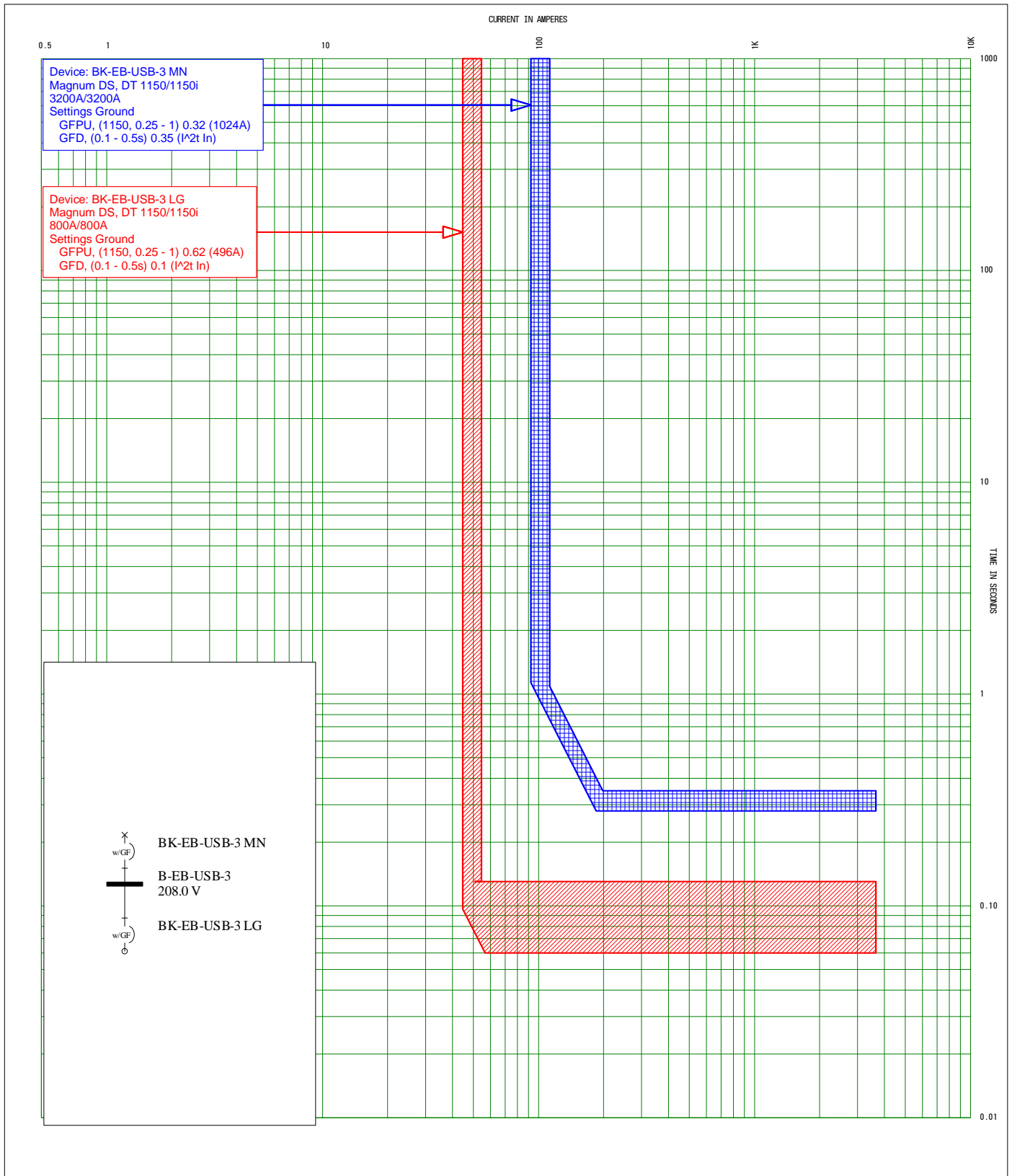
Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB USB-6-7 LV
Ref. Voltage: 480V
Current Scale: x 10



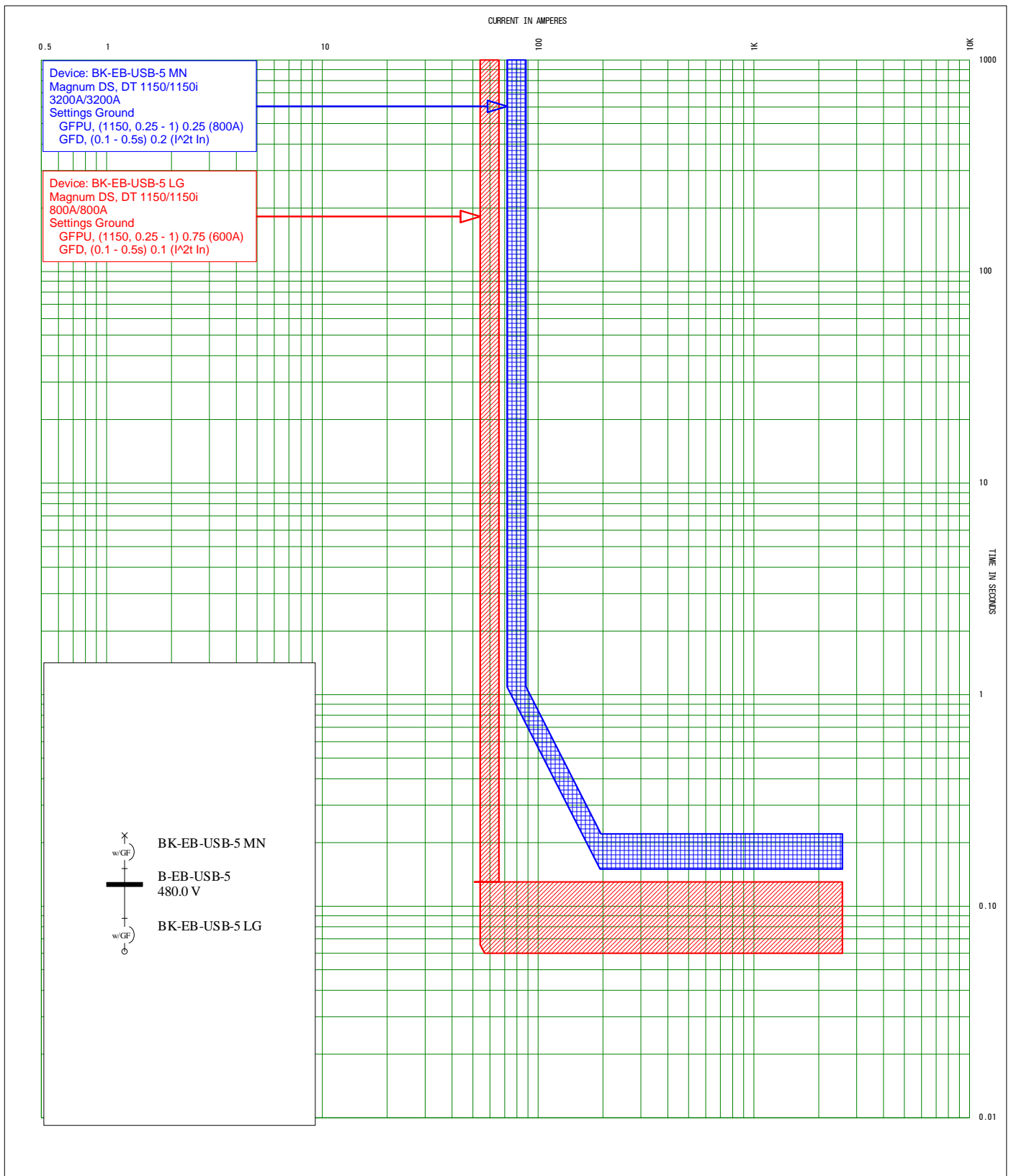
Eaton Electrical Services and Systems
 February 21, 2013

Plot name: EB USB-1-2 GF
 Ref. Voltage: 480V
 Current Scale: x 10



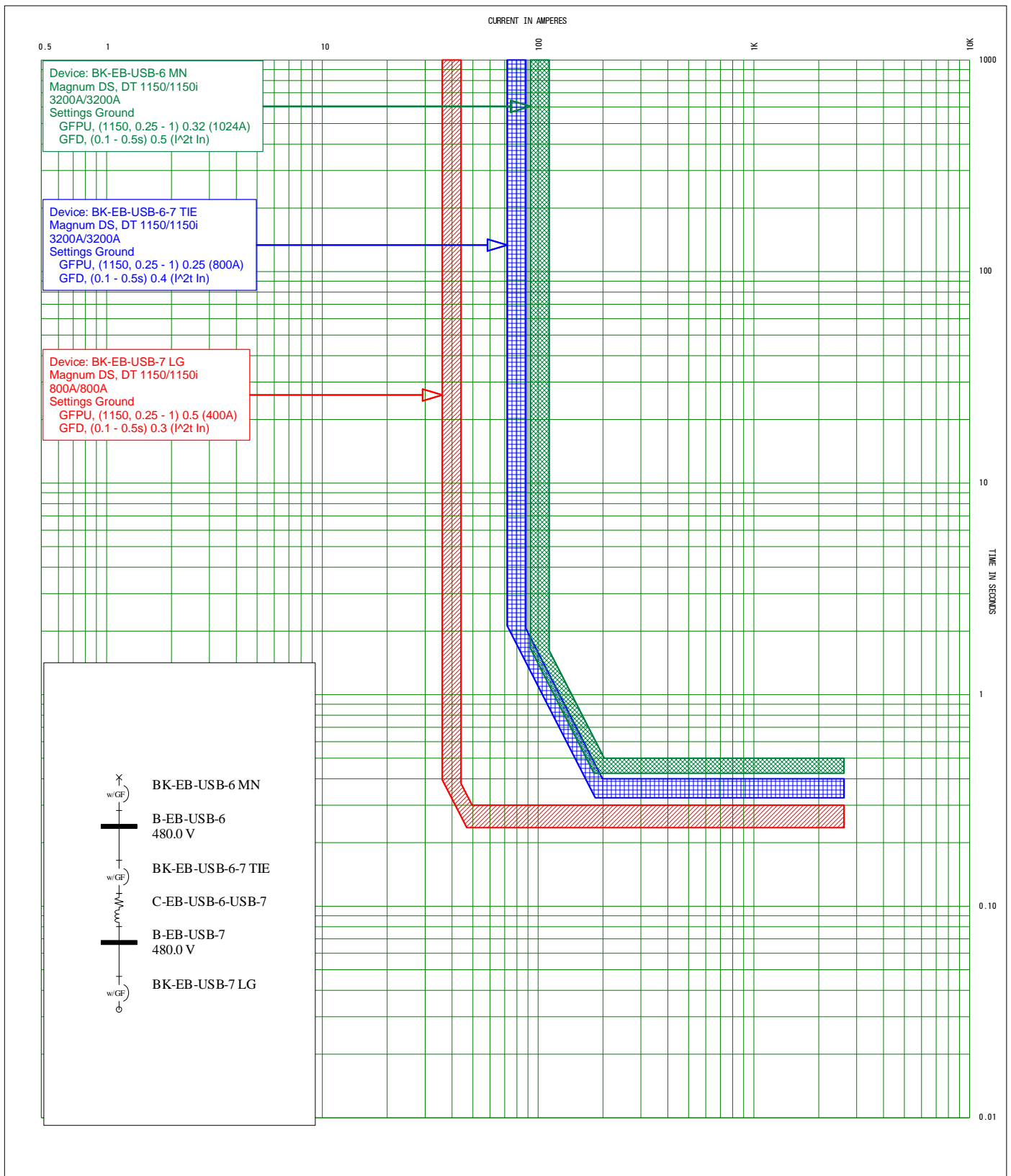
Eaton Electrical Services and Systems
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Plot name: EB USB-3 GF
 Ref. Voltage: 208V
 Current Scale: x 10



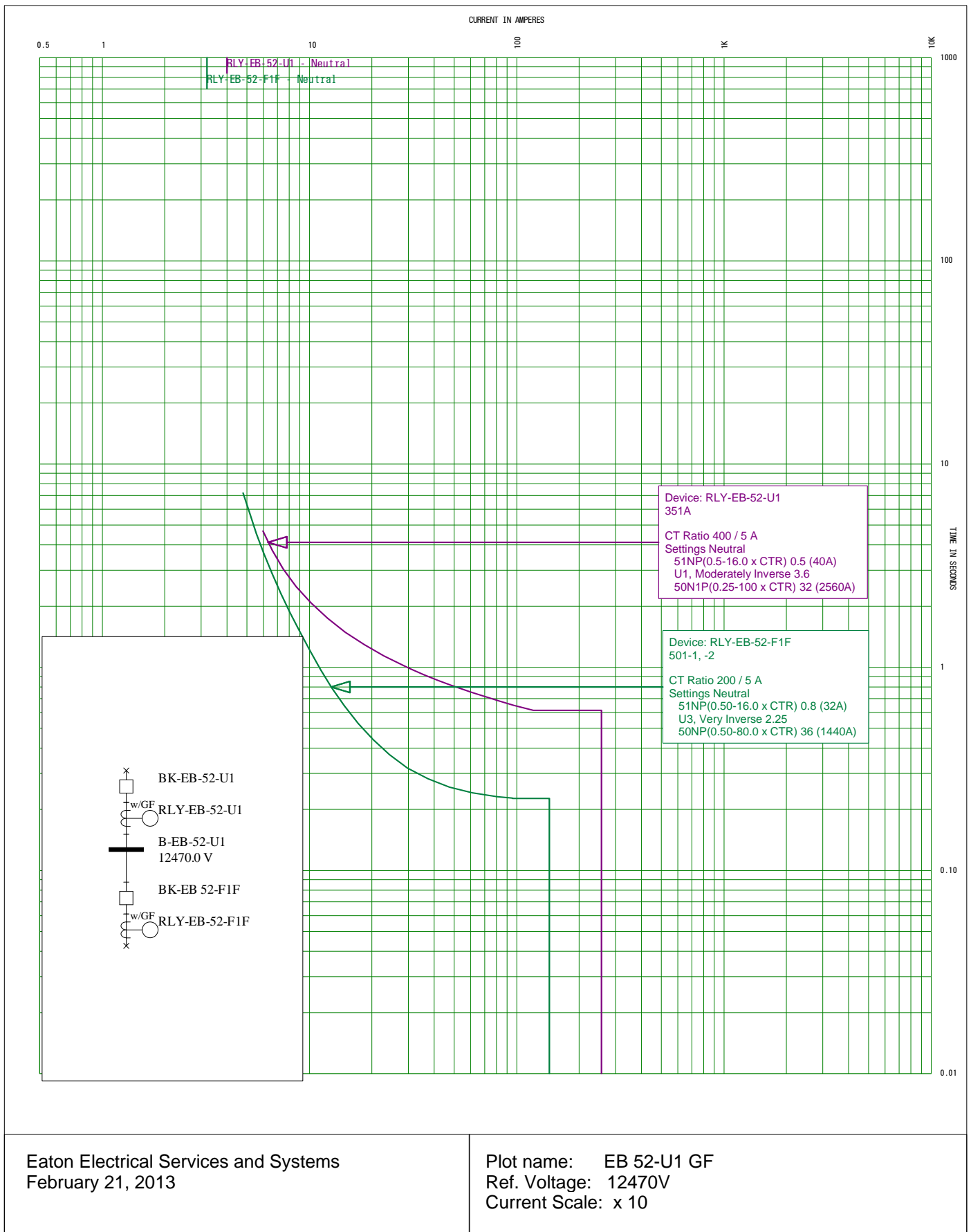
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Plot name: EB USB-5 GF
Ref. Voltage: 480V
Current Scale: x 10



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 February 21, 2013

Plot name: EB USB-6-7 GF
 Ref. Voltage: 480V
 Current Scale: x 10



Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB 52-U1 GF
Ref. Voltage: 12470V
Current Scale: x 10

CURRENT IN AMPERES

0.5

1

10

100

1K

10K

RLY-EB-52-T1 - Neutral
RLY-EB-52-F1F - Neutral
RLY-EB-52-G1 - Neutral

TIME IN SECONDS

100

10

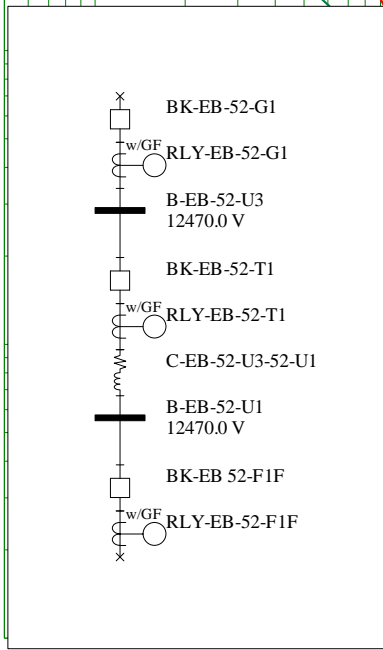
1

0.01

Device: RLY-EB-52-G1
351A
CT Ratio 200 / 5 A
Settings Neutral
51NP(0.5-16.0 x CTR) 0.5 (20A)
U1, Moderately Inverse 2.9
50NP(0.25-100 x CTR) 48 (1920A)

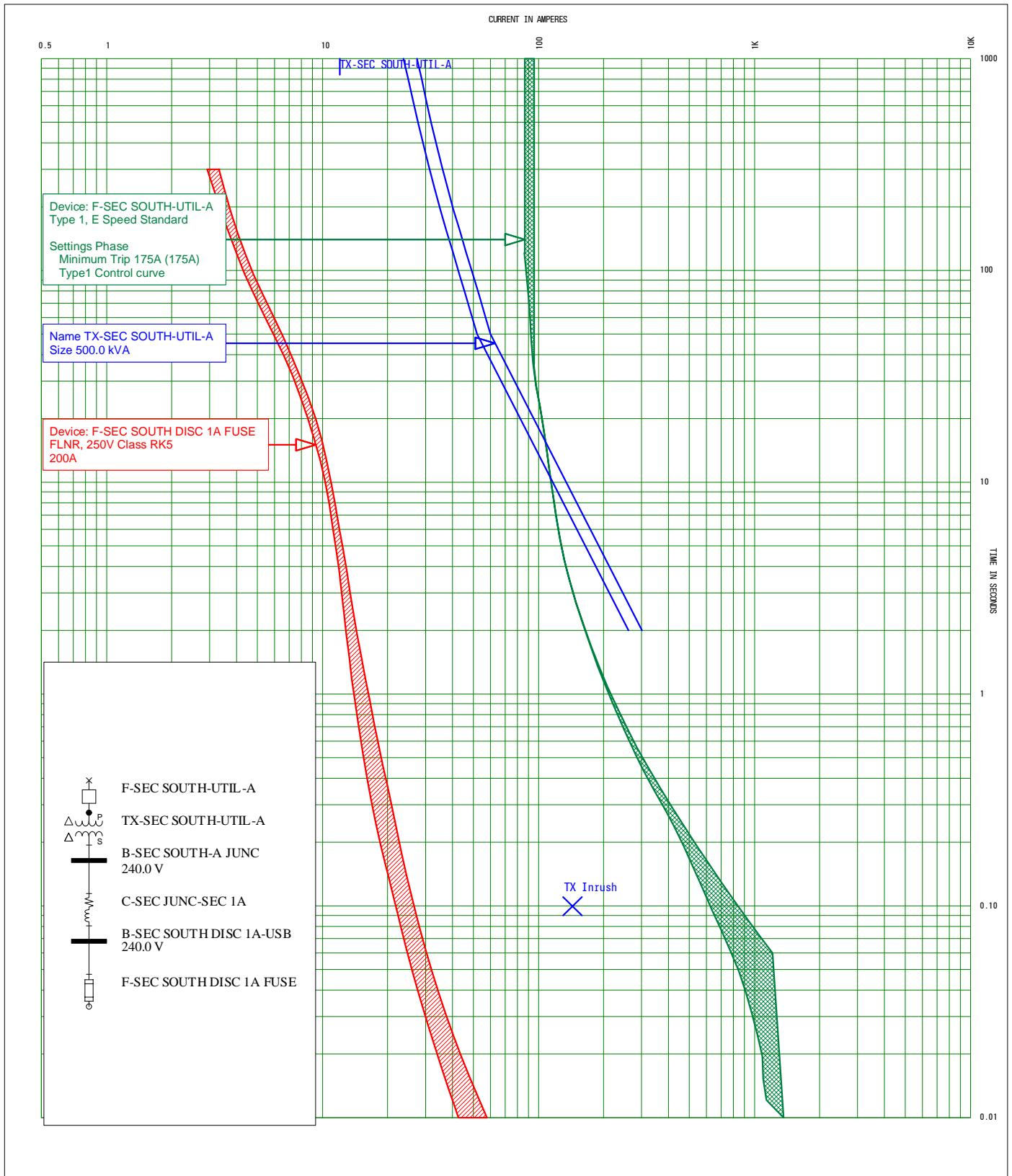
Device: RLY-EB-52-T1
351A
CT Ratio 400 / 5 A
Settings Neutral
51NP(0.5-16.0 x CTR) 0.5 (40A)
U1, Moderately Inverse 2.9
50NP(0.25-100 x CTR) 21.6 (1728A)

Device: RLY-EB-52-F1F
501-1, -2
CT Ratio 200 / 5 A
Settings Neutral
51NP(0.50-16.0 x CTR) 0.8 (32A)
U3, Very Inverse 2.25
50NP(0.50-80.0 x CTR) 36 (1440A)



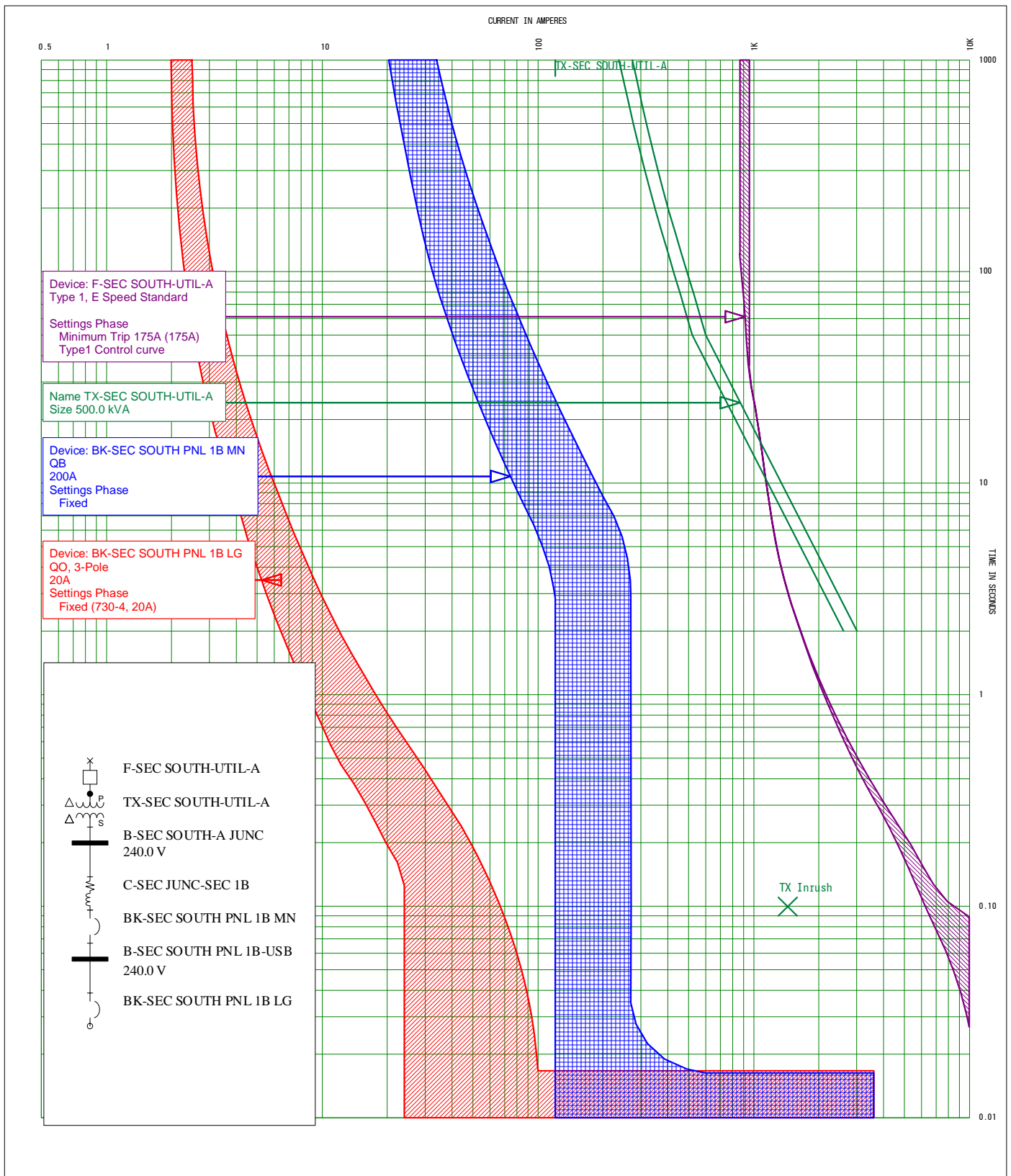
Eaton Electrical Services and Systems
February 21, 2013

Plot name: EB 52-U3 GF
Ref. Voltage: 12470V
Current Scale: x 10



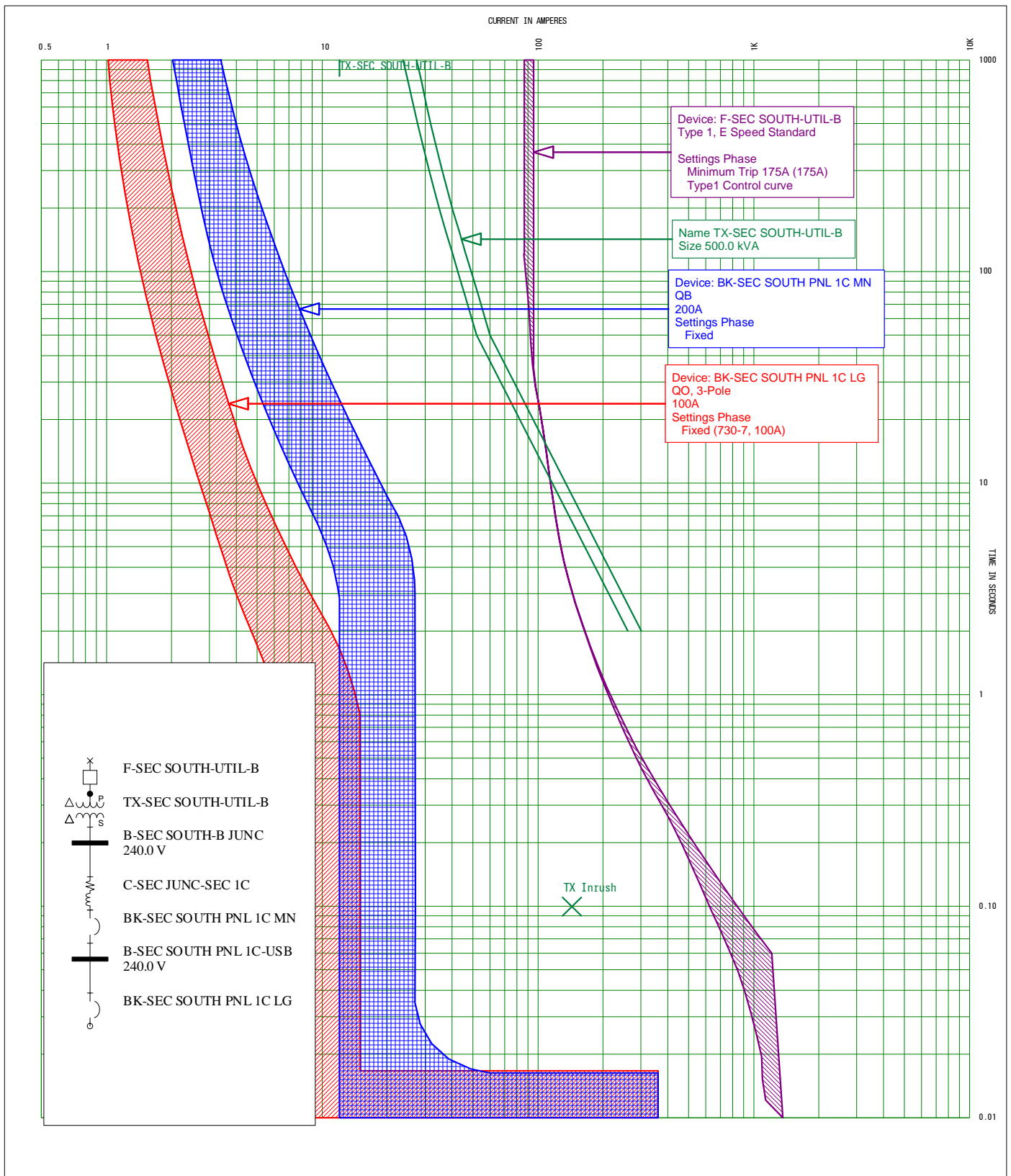
Eaton Electrical Services and Systems
February 21, 2013

Plot name: SEC SOUTH DISC 1A
Ref. Voltage: 240V
Current Scale: x 100



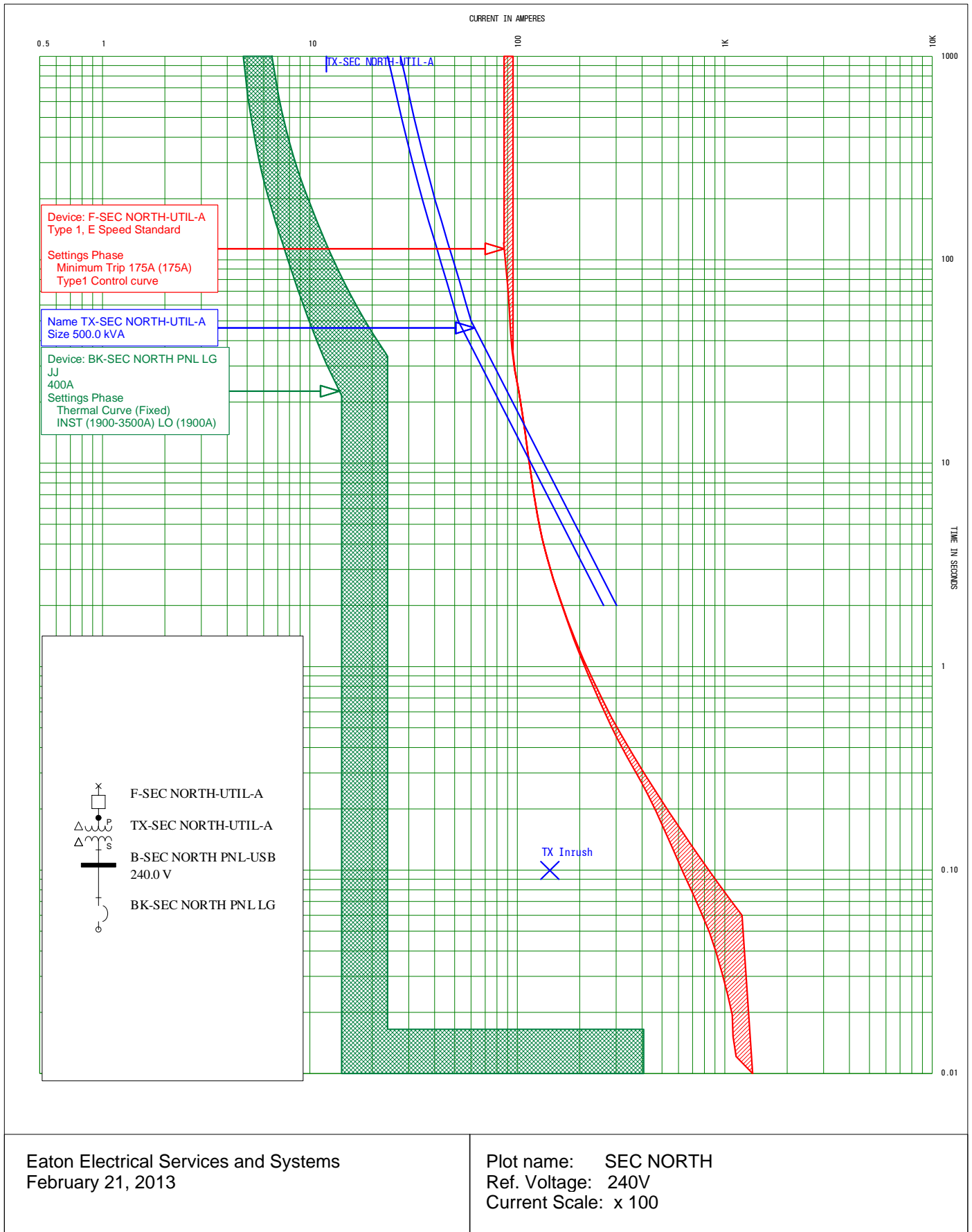
Eaton Electrical Services and Systems
February 21, 2013

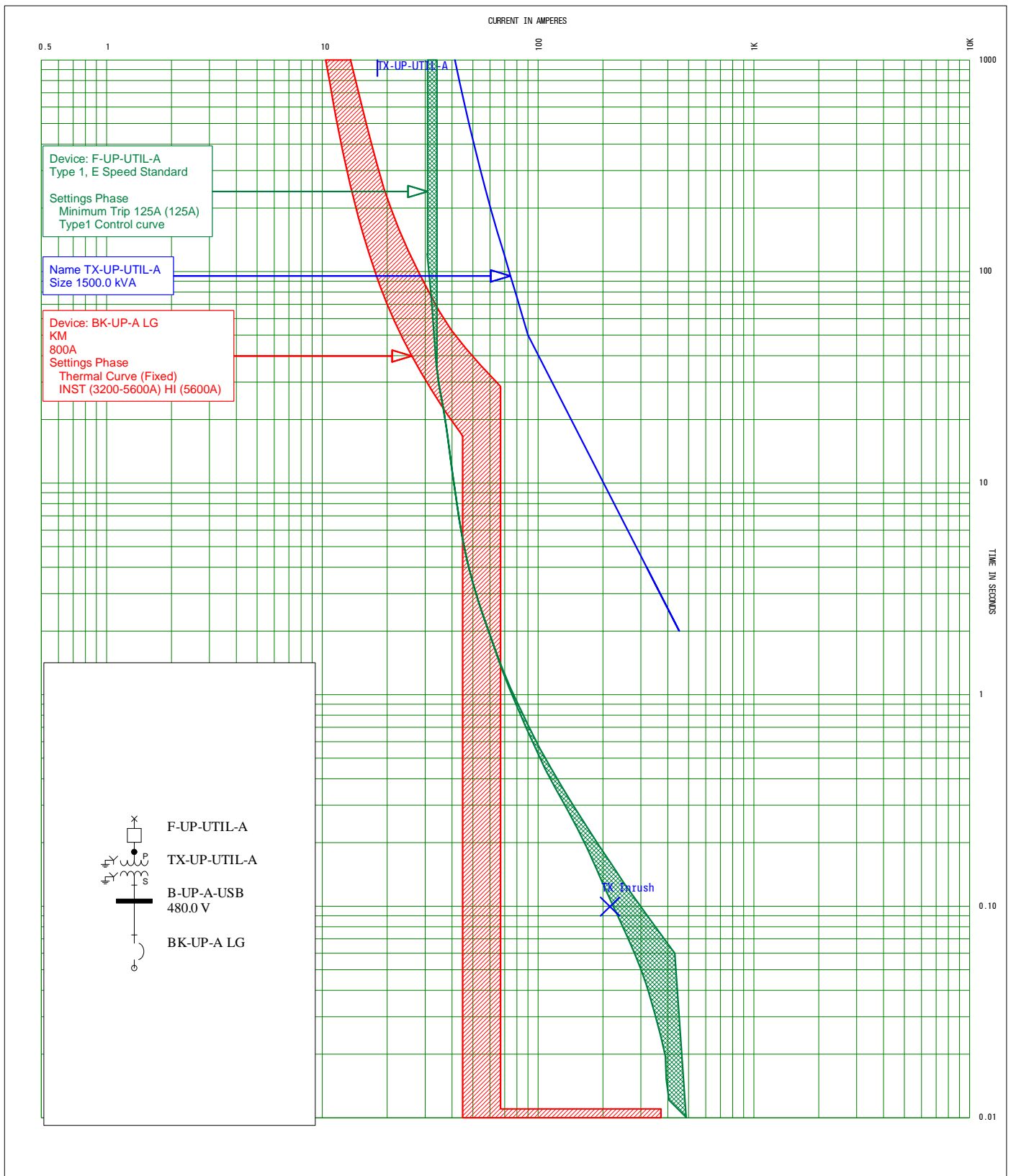
Plot name: SEC SOUTH PNL 1B
Ref. Voltage: 240V
Current Scale: x 10



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February 21, 2013

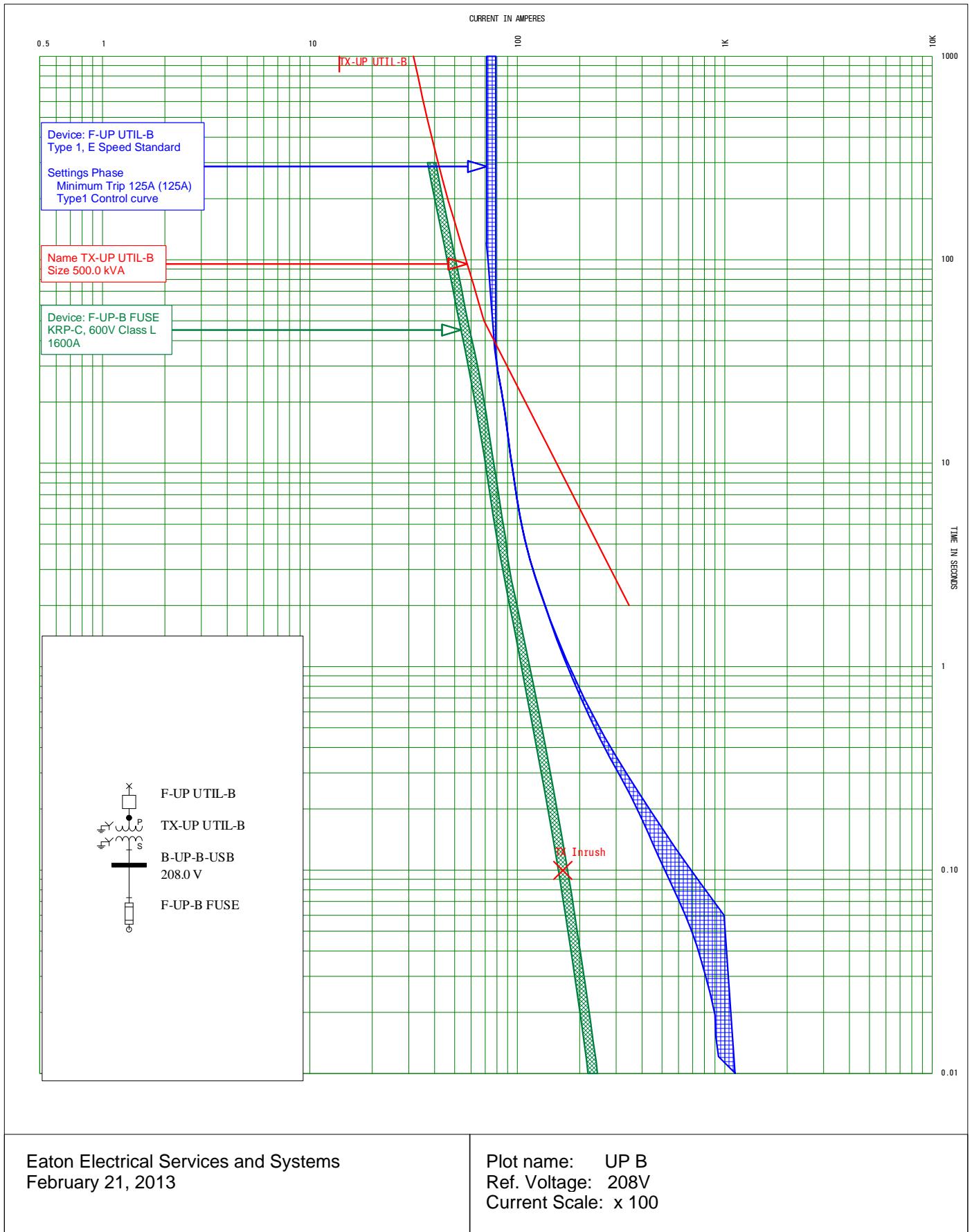
Plot name: SEC SOUTH PNL 1C
Ref. Voltage: 240V
Current Scale: x 100

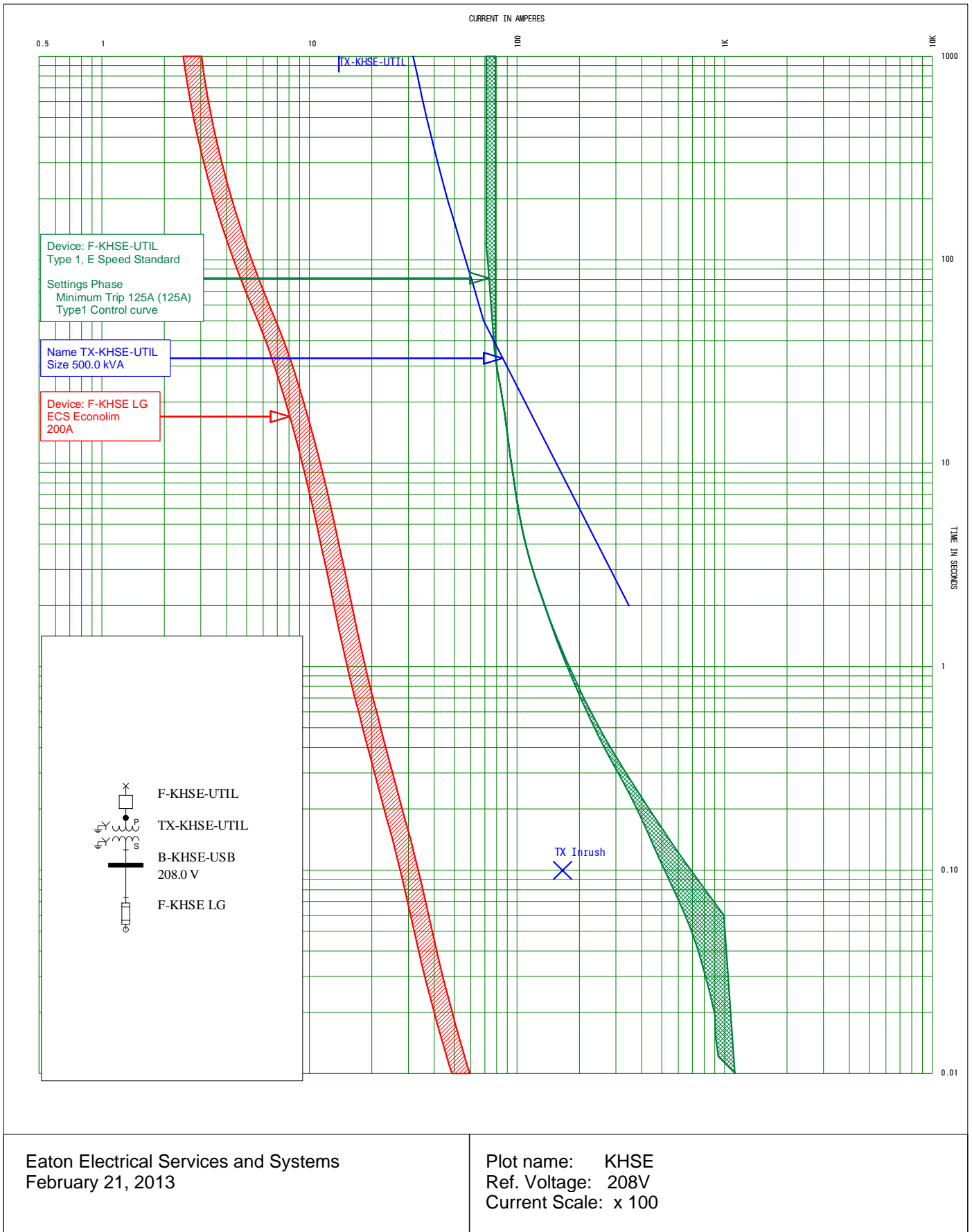


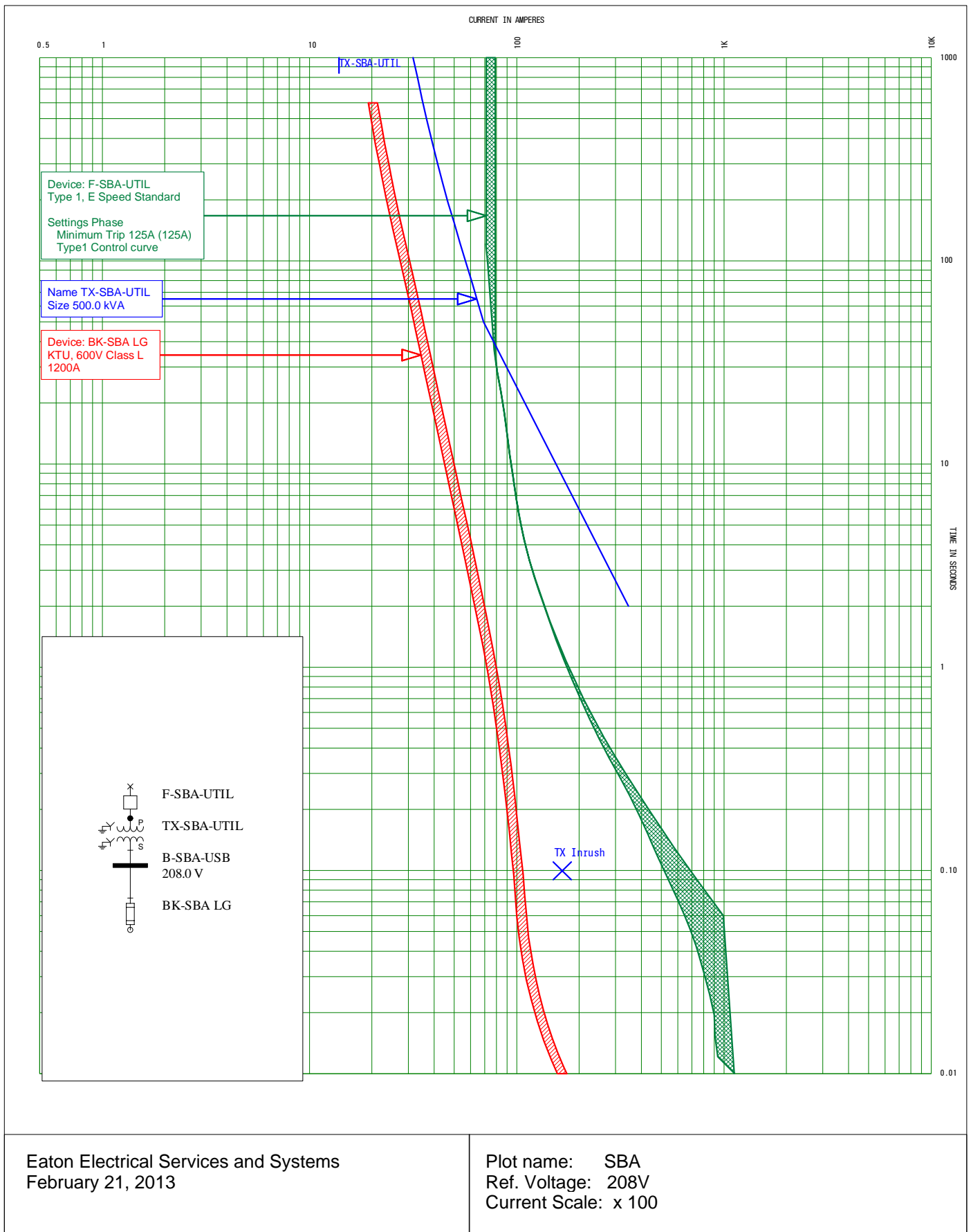


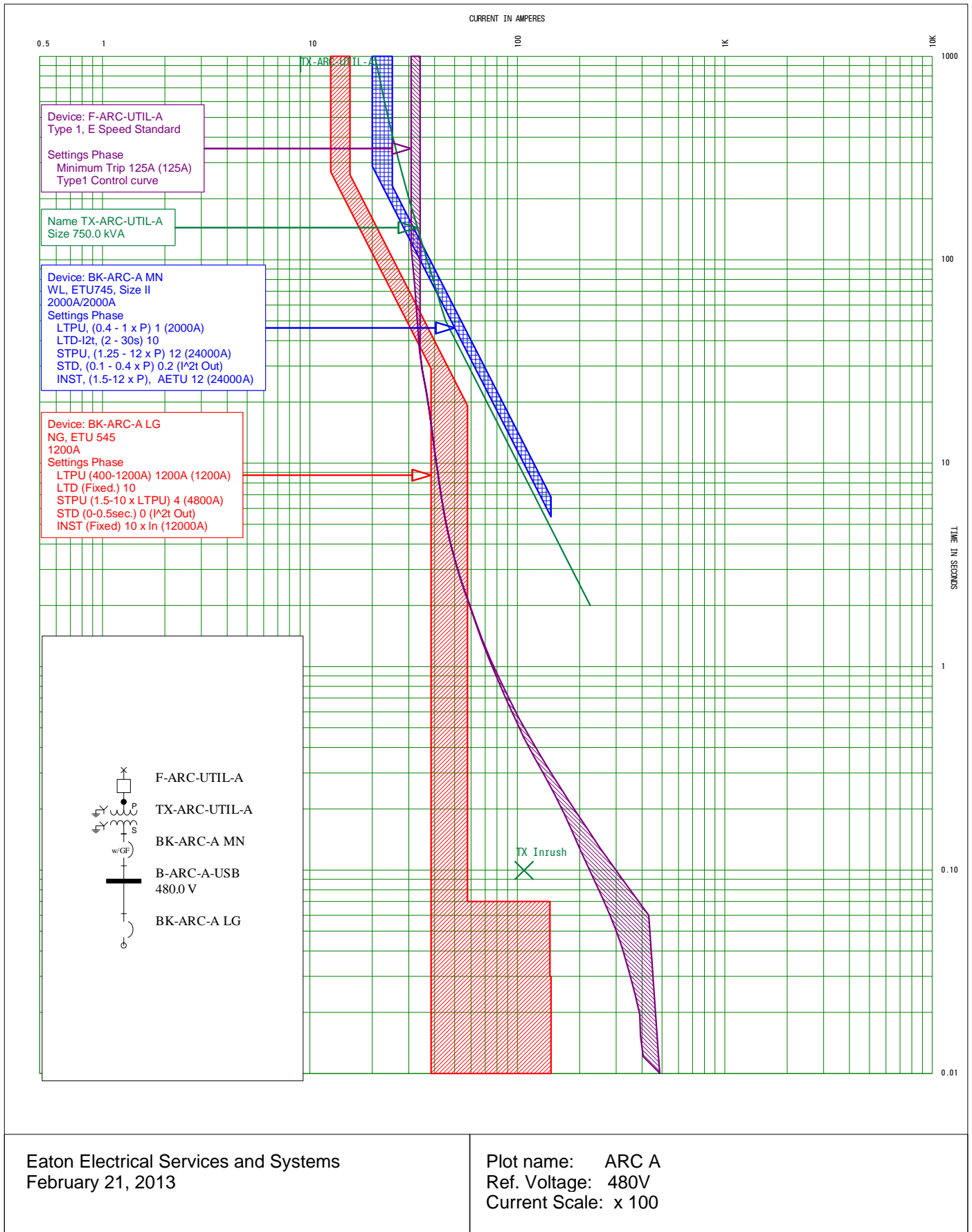
Eaton Electrical Services and Systems
February 21, 2013

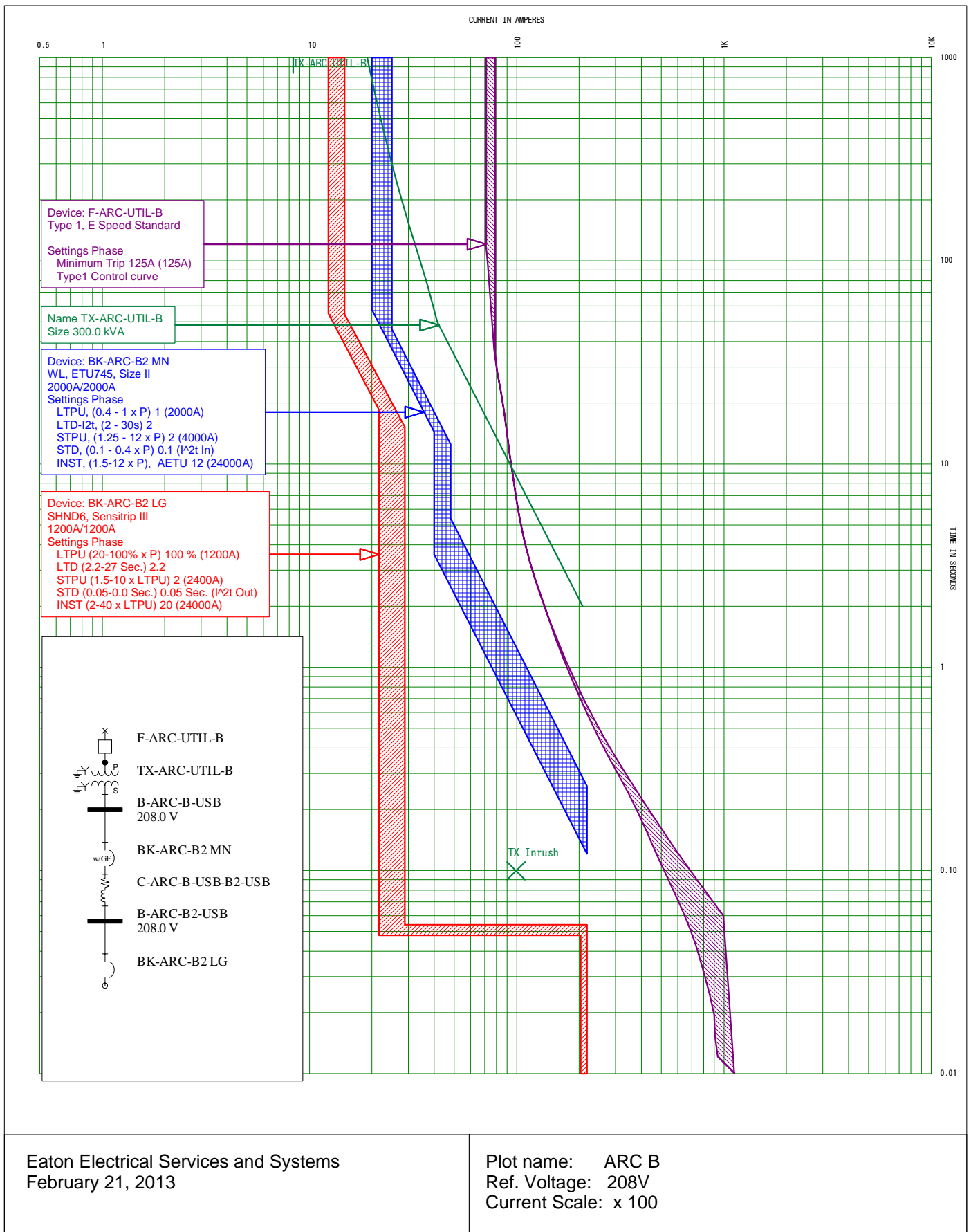
Plot name: UP A
Ref. Voltage: 480V
Current Scale: x 100

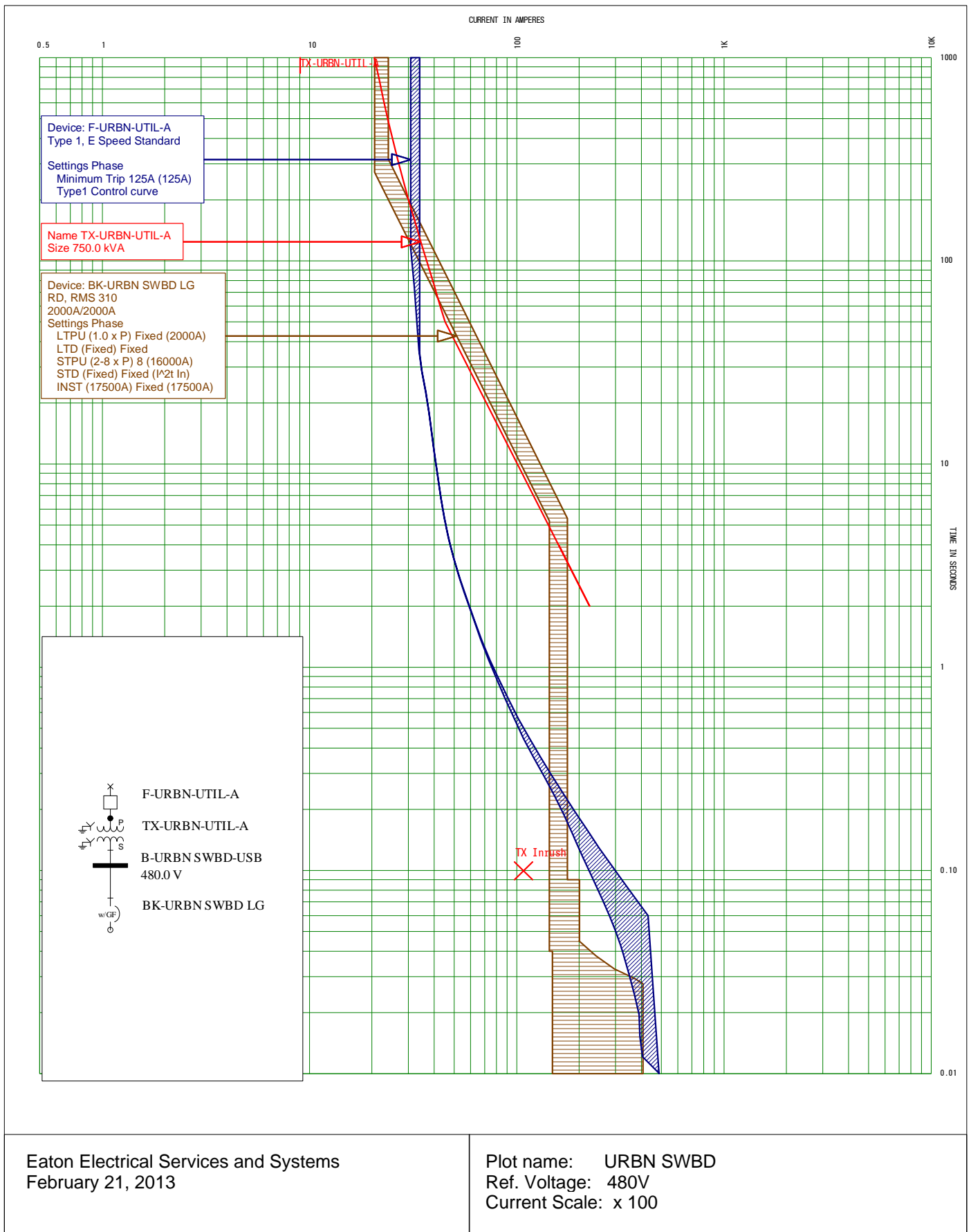


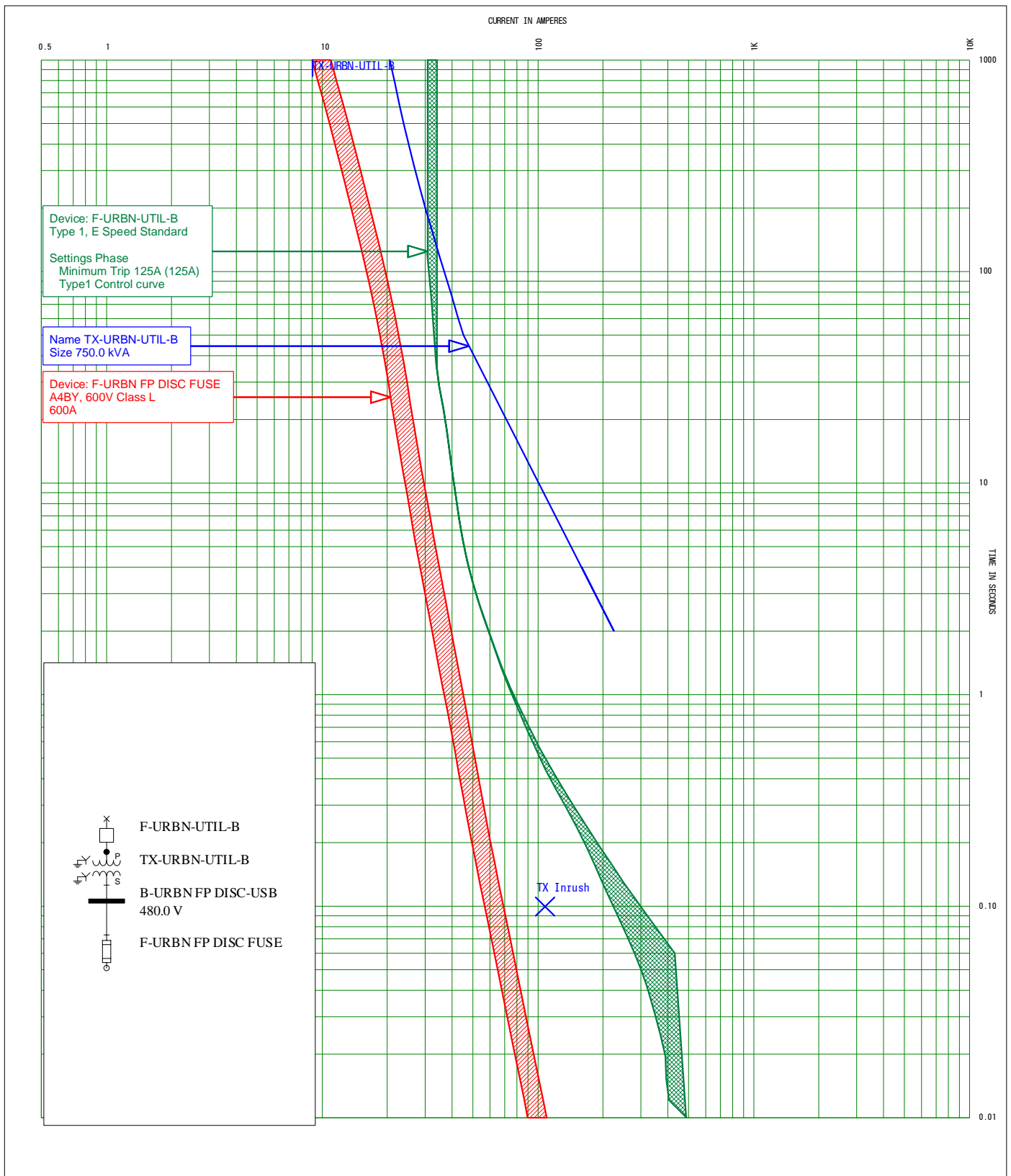






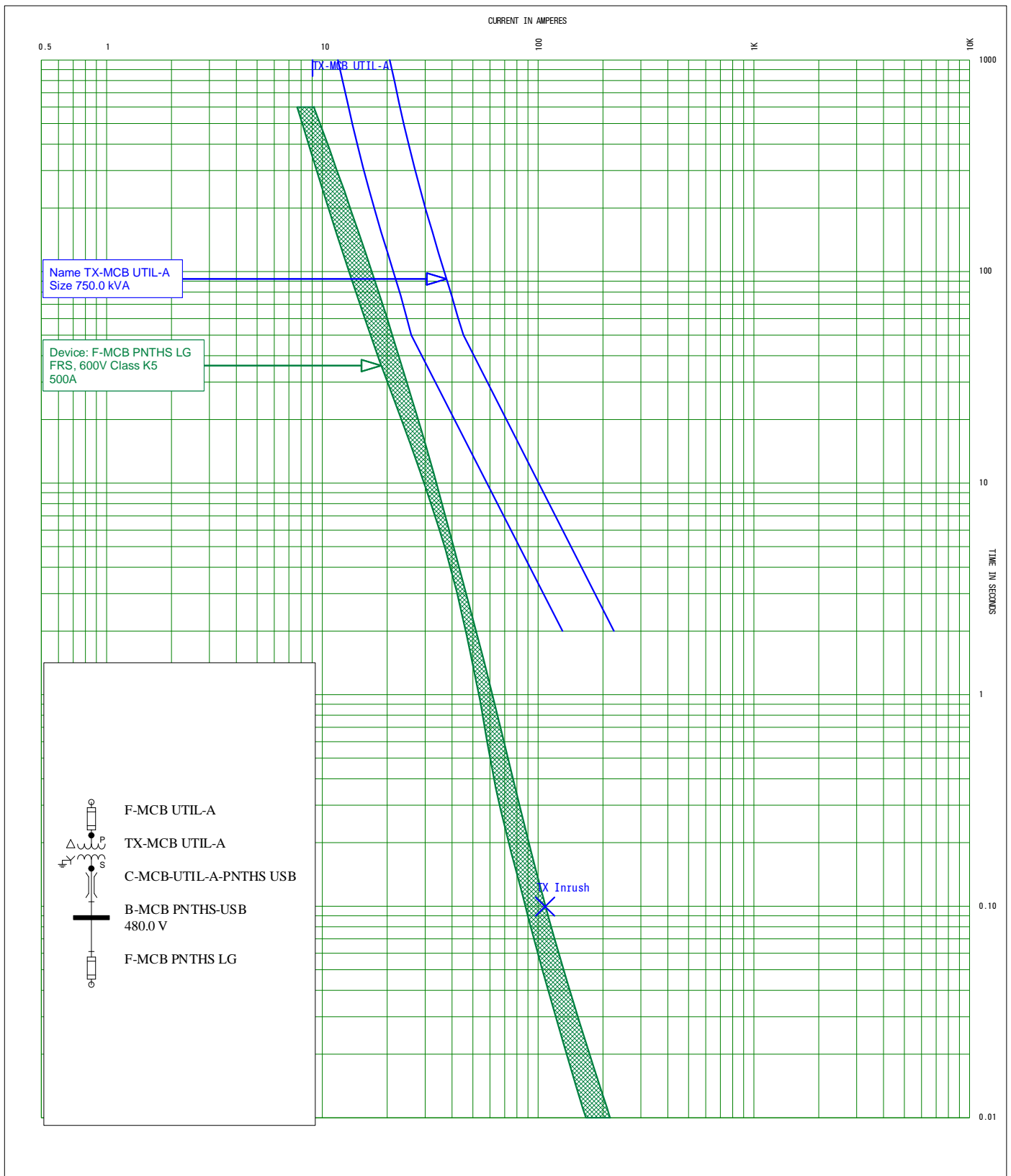






Eaton Electrical Services and Systems
February 21, 2013

Plot name: URBN FP
Ref. Voltage: 480V
Current Scale: x 100



Eaton Electrical Services and Systems
February 21, 2013

Plot name: MCB
Ref. Voltage: 480V
Current Scale: x 100

4.0 RECOMMENDED PROTECTIVE DEVICE SETTINGS

The following tables show a comprehensive summary of the recommended settings for the adjustable protective devices. The devices are grouped by system bus name/location. Refer to Appendix D for the system one-line diagrams.

Table 4.1 - Recommended Low-Voltage Protective Device Settings

BUS NUMBER	FEEDER BREAKER ID	BREAKER MODEL & MANUFACTURER	TRIP UNIT TYPE	CURRENT RATING		LONG DELAY		SHORT DELAY			INST.	GROUND		CURVE NAME
				FRAME	PLUG	PICKUP	TIME	PICKUP	TIME	I _t		PICKUP	TIME, I _t	
B-SH-USB	BK-SH MN Main Breaker	PowerBreak II GE	MVT Plus LSI	2000A	2000A	1 (?)	1 (?)	3.5 (?)	Min (?)	Out (?)	15 (?)	---	---	SH
B-OND ANNEX SWBD-USB	BK-OND ANNEX SWBD MN Main Breaker	RD Cutler-Hammer	RMS310 LSG	1600A	1600A	---	---	5 (4)	---	---	---	(F)	(0.15s, In)	OND ANNEX
B-BHB MSB-A SWBD-USB	BK-BHB MSB-A SWBD MN Main Breaker	RJ Square D	Micrologic 6.0A LSIG	2000A	2000A	1 (1)	0.5 (0.5)	1.5 (1.5)	0.1 (0.1)	In (In)	12 (2)	(A)	(0.1, Out)	BHB MSB-A
B-NASC-USB	BK-NASC MN Main Breaker	MH Square D	Thermal Magnetic	600A	600A	---	---	---	---	---	MAX (MIN)	---	---	NASC
B-EB-USB-1	BK-EB-USB-1 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	(1)	(6.5)	(2)	(0.35)	(In)	(OFF)	(0.32)	(0.35, In)	EB-USB-1-2 LV, EB-USB-1-2 GF
B-EB-USB-1	BK-EB-USB-1-2 TIE Tie Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	(0.75)	(3.5)	(2)	(0.2)	(In)	(OFF)	(0.25)	(0.2, In)	EB-USB-1-2 LV, EB-USB-1-2 GF
B-EB-USB-2	BK-EB-USB-2 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	(1)	(6.5)	(2)	(0.35)	(In)	(OFF)	(0.32)	(0.35, In)	EB-USB-1-2 LV, EB-USB-1-2 GF
B-EB-USB-3	BK-EB-USB-3 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	(1)	(13.5)	(2.5)	(0.35)	(In)	(OFF)	(0.32)	(0.35, In)	EB-USB-3, EB-USB-3 GF
B-EB-USB-5	BK-EB-USB-5 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	(0.70)	(6.5)	(2)	(0.2)	(In)	(OFF)	90.25)	(0.2, In)	EB-USB-5, EB-USB-5 GF
B-EB-USB-6	BK-EB-USB-6 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	1 (1)	6.5 (6.5)	2.5 (2)	0.35 (0.35)	In (In)	OFF (OFF)	0.32 (0.32)	0.5, In (0.35, In)	EB-USB-6-7 LV, EB-USB-6-7 GF,
B-EB-USB-6	BK-EB-USB-6-7 TIE Tie Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	0.75 (0.75)	3.5 (3.5)	2.5 (2)	0.2 (0.2)	In (In)	OFF (OFF)	0.25 (0.25)	0.4, In (0.2, In)	EB-USB-6-7 LV, EB-USB-6-7 GF
B-EB-USB-7	BK-EB-USB-7 MN Main Breaker	MDS-632 Eaton	Optim1150 LSIG	3200A	3200A	1 (1)	6.5 (6.5)	2.5 (2)	0.35 (0.35)	In (In)	OFF (OFF)	0.32 (0.32)	0.5, In (0.35, In)	EB-USB-6-7 LV, EB-USB-6-7 GF
B-ARC-A-USB	BK-ARC-A MN Main Breaker	WLL Siemens	ETU745 LSIA	2000A	2000A	1 (1)	10 (10)	12 (12)	0.2 (0.2)	Out (Out)	12 (4)	C (C)	0.3, In (0.3, In)	ARC A
B-ARC-B-USB	BK-ARC-B MN Main Breaker	WLL Siemens	ETU745 LSIA	2000A	2000A	1 (1)	2 (2)	2 (2)	0.1 (0.1)	In (In)	12 (8)	C (C)	0.3, In (0.3, In)	ARC B

Where available, existing settings are shown in parenthesis. If existing settings were unavailable, (?) is shown.

When breaker information was not available and an adjustable breaker was assumed, that breaker was set to its maximum. Settings for these breakers are not shown in this table.

Table 4.2 - Recommended Medium-Voltage Protective Device Settings

CIRCUIT IDENTIFICATION		PROTECTIVE DEVICE DESCRIPTION				RECOMMENDED SETTINGS						
BUS NUMBER	BREAKER ID / FEEDER	DEVICE FUNCTION	DEVICE MAKER	MODEL NUMBER	RELAY RANGES	CT RATIO	TAP (A)	TIME DIAL	CURVE TYPE	INST (A)	INST DELAY	CURVE
B-EB-52-U1	RLY-EB-52-U1	50 / 51 P	Schweitzer	SEL-351A	0.25 – 16 (Tap) 0.25 – 100 (INST)	400:5	2.5 (200 A)	4.5	U3, Very Inverse	24.5 (1960 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.25 – 100 (INST)	400:5	0.5 (40 A)	3.6	U1, Moderately Inverse	32 (2560 A)	---	EB 52-U1 GF
	RLY-EB-52-F1B	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	5 (200 A)	2	U3, Very Inverse	36 (1440 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.8 (32 A)	2.25	U3, Very Inverse	36 (1440 A)	---	EB 52-U1 GF
	RLY-EB-52-F1D	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	3 (120 A)	1.6	U3, Very Inverse	18 (720 A)	---	EB USB-3
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	1 (40 A)	1.87	U3, Very Inverse	16 (640 A)	---	EB 52-U1 GF
	RLY-EB-52-F1F	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	5 (200 A)	2	U3, Very Inverse	36 (1440 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.8 (32 A)	2.25	U3, Very Inverse	36 (1440 A)	---	EB 52-U1 GF
B-EB-52-U2	RLY-EB-52-U2	50 / 51 P	Schweitzer	SEL-351A	0.25 – 16 (Tap) 0.25 – 100 (INST)	400:5	2.5 (200 A)	4.5	U3, Very Inverse	24.5 (1960 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.25 – 100 (INST)	400:5	0.5 (40 A)	3.6	U1, Moderately Inverse	32 (2560 A)	---	EB 52-U1 GF
	RLY-EB-52-F2B	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	5 (200 A)	2	U3, Very Inverse	36 (1440 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.8 (32 A)	2.25	U3, Very Inverse	36 (1440 A)	---	EB 52-U1 GF
	RLY-EB-52-F2D	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	3.3 (132 A)	1.8	U3, Very Inverse	30 (1200 A)	---	EB USB-3
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.6 (24 A)	1.44	U1, Moderately Inverse	30.6 (1224 A)	---	EB 52-U1 GF
	RLY-EB-52-F2F	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	5 (200 A)	2	U3, Very Inverse	36 (1440 A)	---	EB USB-1 MV
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.8 (32 A)	2.25	U3, Very Inverse	36 (1440 A)	---	EB 52-U1 GF
B-EB-52-U3	RLY-EB-52-G1	50 / 51 P	Schweitzer	SEL-351A	0.25 – 16 (Tap) 0.25 – 100 (INST)	200:5	2.5 (100 A)	2.7	U3, Very Inverse	44 (1760 A)	---	EB 52-U1 GEN

CIRCUIT IDENTIFICATION		PROTECTIVE DEVICE DESCRIPTION					RECOMMENDED SETTINGS					
BUS NUMBER	BREAKER ID / FEEDER	DEVICE FUNCTION	DEVICE MAKER	MODEL NUMBER	RELAY RANGES	CT RATIO	TAP (A)	TIME DIAL	CURVE TYPE	INST (A)	INST DELAY	CURVE
B-EB-52-U3	RLY-EB-52-G1	50 / 51 P	Schweitzer	SEL-351A	0.5 – 16 (Tap) 0.25 – 100 (INST)	200:5	0.5 (20 A)	2.9	U1, Moderately Inverse	48 (1920 A)	---	EB 52-U3 GF
	RLY-EB-52-T1	50 / 51 P	Schweitzer	SEL-351A	0.25 – 16 (Tap) 0.25 – 100 (INST)	400:5	2.5 (200 A)	2.7	U3, Very Inverse	20 (1600 A)	---	EB 52-U1 GEN
		50 / 51 N			0.5 – 16 (Tap) 0.25 – 100 (INST)	400:5	0.5 (40 A)	2.9	U1, Moderately Inverse	21.6 (1728 A)	---	EB 52-U3 GF
	RLY-EB-52-T2	50 / 51 P	Schweitzer	SEL-351A	0.25 – 16 (Tap) 0.25 – 100 (INST)	400:5	2.5 (200 A)	2.7	U3, Very Inverse	20 (1600 A)	---	EB 52-U1 GEN
		50 / 51 N			0.5 – 16 (Tap) 0.25 – 100 (INST)	400:5	0.5 (40 A)	2.9	U1, Moderately Inverse	21.6 (1728 A)	---	EB 52-U3 GF
	RLY-EB-52-F3B	50 / 51 P	Schweitzer	SEL-501-2	0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.5 (20 A)	10	U4, Extremely Inverse	4 (160 A)	---	EB FP
		50 / 51 N			0.5 – 16 (Tap) 0.5 – 80 (INST)	200:5	0.5 (20 A)	4.22	U4, Extremely Inverse	16 (960 A)	---	EB 52-U3 GF

Table 4.2 is for informational purposes only and serves as a record of the relay settings used in calculation of the arc flash incident energies. All relay settings are as found and are not adjusted as part of this study. Any adjustment of settings must take place in cooperation with PGE Engineers.

5.0 ARC FLASH HAZARD ANALYSIS

This section of the report contains the interpretation for the arc flash hazard analysis. The calculations made in this arc flash hazard analysis conform to NFPA 70E, and are based on the information provided by the customer. Actual heat and radiation exposure may be more or less than reflected in the analysis.

Only qualified electricians who are familiar with the installation and maintenance of electrical distribution equipment should perform work associated with such products. All recommendations of the manufacturer, warnings and cautions relating to the safety of personnel and equipment should be followed. All applicable health and safety laws, codes, standards, and procedures should be adhered to. All equipment should be de-energized prior to any maintenance or service. OSHA 1910.333 requirements should be adhered to. All guidelines of NFPA 70E-2012 should be followed, and in particular appropriate personal protective equipment must be provided and worn.

Eaton Corporation will not be responsible for the misuse or misapplication of the information contained in this analysis. Those providing service for electrical equipment should contact an Eaton Electrical Services and Systems representative, or other qualified individual, if any questions arise.

5.1 Introduction

NFPA 70E-2012, Article 110.3(F) requires that an employer developed electrical safety program includes a hazard identification and risk evaluation procedure. This procedure is meant to be used before performing work on or near any equipment at or above 50 volts or any time work is being performed where an electrical hazard exists. This analysis presents only the results of an incident energy evaluation conducted in accordance with 130.5(B). The risk depends on a number of factors. These include the nature of the task being performed and the condition of the equipment. Selection of personal protective equipment (PPE) must be made based on the incident energy level that is presented in this report and a risk assessment to be made by the qualified person. NFPA 70E-2012, Article 130.7(A) requires that employees use and employers provide proper PPE for the tasks being performed. NFPA 70E-2012, Table H.3(b) provides guidance for the selection of PPE based on calculated incident energy exposure.

NFPA 70E-2012 and IEEE Std 1584-2002 provide equations and methods to accurately calculate the arc flash boundary and incident energy at specific locations within a facility's electrical system. Any location where work may be performed on or near energized electrical conductors and circuit parts is subject to the arc flash standards. PPE used to guard against arc flash hazard should be considered the last line of defense. It is also important to note that the use of PPE is not intended to prevent all injuries from an arc flash. The goal of determining PPE levels using the arc flash hazard

approach is to identify the level of protection required to limit the injury to the onset of a second degree burn in the event of an arc flash while avoiding the use of more protection than is needed so as to minimize hazards of heat stress, reduced visibility and limited body movement.

Although the arc flash calculation procedure is based upon NFPA 70E and IEEE Std 1584-2002 equations and methods, it is a relatively new approach to determining the degree of required PPE. The calculations are derived from theory and research involving arc current incident energy measurements conducted under a specific set of controlled test conditions. Therefore, calculation results may be more severe or less severe than the hazard presented by an actual arc flash exposure. Also, the arc flash hazard calculations do not take into account hazards associated with the splattering of molten metal, explosively propelled pieces of equipment and air pressure shock waves.

The results of this arc flash hazard analysis are not intended to imply that personnel be permitted to work on exposed energized equipment or circuits. OSHA 1910.333 restricts the situations in which work is to be performed near or on energized equipment or circuits by stating, "Live parts to which an employee may be exposed shall be deenergized before the employee works on or near them, unless the employer can demonstrate that deenergizing introduces additional or increased hazards or is infeasible due to equipment design or operational limitations."

Even if work is not being performed directly on energized equipment, it is important that the proper PPE be used during some load interruption actions, during visual verification of the state of disconnecting devices, and during lockout/tagout procedures.

5.2 Study Procedure

In accordance with NFPA 70E and IEEE Std 1584-2002, SKM Systems Analysis software provides the calculation of these values. The equations used in these calculations are based on actual test values. These tests measured the calories per square centimeter (cal/cm^2) radiating from a simulated arcing fault. The measurements were performed at a theorized working distance of 18 inches.

The intent of NFPA 70E and IEEE Std 1584-2002 guidelines is to establish standard calculations to determine an approach boundary that will prevent the onset of a second-degree burn to the face and the torso of the worker. An incident energy of $1.2 \text{ cal}/\text{cm}^2$ represents the onset of a second-degree burn.

NFPA 70E-2012, Article 130.7(A), Informational Note 3, states that greater consideration must be given to the decision to work within the limited approach boundary of energized electrical equipment when the incident energy exceeds $40 \text{ cal}/\text{cm}^2$. Locations with a calculated incident energy that exceeds $40 \text{ cal}/\text{cm}^2$ are shown in Table 5.2.

Before the arc flash equations can be applied, a comprehensive short-circuit and protective device coordination study must be completed to include all locations where work may be performed on or near energized components; e.g. motor control centers and power distribution panels. Since the short-circuit current must be calculated at every pertinent location and the clearing time of each location's upstream protective device is required, the arc flash circuit model is more detailed and extends deeper into the facility electrical distribution system than is typical of a basic short-circuit and protective device coordination study. Accurate fault currents and device clearing times are extremely important in deriving reliable results. A conservative (high) fault current value could yield a faster clearing time of a protective device, depending upon its curve shape, and the calculated incident energy may actually be less than the incident energy calculated for a lower magnitude of fault current and a longer clearing time.

1. Arc Flash Scenarios

Since the greatest arc flash hazards may not result from the highest fault current, multiple scenarios must be analyzed and compared. The following modes of operation have been evaluated in order to determine the worst-case incident energy at each location in the system. It is important to determine the available short-circuit current for modes of operation that provide both the maximum and minimum available short-circuit currents.

- Arc Flash Scenario 1 – 4th Avenue / Engineering Building system supplied from the Urban-Medical utility feed via Medium Voltage Switchgear B-EB-52-U1. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U2 are open.
- Arc Flash Scenario 2 – 4th Avenue / Engineering Building system supplied from the Urban-Gibbs utility feed via Medium Voltage Switchgear B-EB-52-U2. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U1 are open.
- Arc Flash Scenario 3 – 4th Avenue / Engineering Building system supplied from the Emergency Generator via Medium Voltage Switchgear B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-U1 and BK-EB-52-U2 are open.
- Arc Flash Scenario 4 – 4th Avenue / Engineering Building system supplied from the Urban-Medical utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U1 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U2 is open.
- Arc Flash Scenario 5 – 4th Avenue / Engineering Building system supplied from the Urban-Gibbs utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U2 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U1 is open.

- Arc Flash Scenario 6 – 4th Avenue / Engineering Building system supplied from 50% of the maximum of the Urban-Medical utility feed via Medium Voltage Switchgear B-EB-52-U1. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U2 are open.
- Arc Flash Scenario 7 – 4th Avenue / Engineering Building system supplied from 50% the maximum of the Urban-Gibbs utility feed via Medium Voltage Switchgear B-EB-52-U2. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breakers BK-EB-52-G1 and BK-EB-52-U1 are open.
- Arc Flash Scenario 8 – 4th Avenue / Engineering Building system supplied from 50% of the maximum of the Urban-Medical utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U1 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U2 is open.
- Arc Flash Scenario 9 – 4th Avenue / Engineering Building system supplied from 50% of the maximum of the Urban-Gibbs utility feed and Emergency Generator via Medium Voltage Switchgear B-EB-52-U2 and B-EB-52-U3. Tie breakers BK-EB-52-T1 and BK-EB-52-T2 are closed and the Main Breaker BK-EB-52-U1 is open.
- Arc Flash Scenario 10 – All locations other than the 4th Avenue / Engineering Building supplied with 50% of the utility maximum available fault current.

2. Assumptions

The following assumptions were used in performing the arc flash analysis and ensure conservative, worst-case results:

- The minimum available fault current at any location is equal to 50% of the fault current value provided by PGE.

For this arc flash hazard analysis of the Non-West Campus Loop at Portland State University, the circuit model included the service disconnects for all locations not supplied by the West Campus Loop. The analysis required energy and boundary calculations for approximately seventy-seven (77) locations.

5.3 Arc Flash Hazard Analysis Results

The incident energy associated with an arc flash is dependent upon the following parameters:

- The maximum “bolted fault” three-phase short-circuit current available at the equipment and the minimum fault level at which the arc will self-sustain.

- The total protective device clearing time (upstream of the prospective arc location) at the maximum short-circuit current and the minimum fault level at which the arc will self-sustain.
- The distance of the worker from the prospective arc for the task to be performed.

Table 5.3 is provided specifically at the request of Portland State University. It is their requirement that a second incident energy calculation be performed, with a greater working distance, for any location with an incident energy above 40 cal/cm². This is specifically to be used when a qualified person is performing non-contact voltage testing to ensure a piece of equipment is de-energized before performing work. All locations, not just those with an incident energy above 40 cal/cm², were included in Table 5.3 for reference.

The arc flash hazard analysis results shown in Table 5.1, Table 5.2, and Table 5.3 are based on a protective device clearing time that is capped at 2 seconds. This is based on IEEE Std 1584-2002 which states in Annex B, Instructions and Examples; *“If the time is longer than two seconds, consider how long a person is likely to remain in the location of the arc flash. It is likely that a person exposed to an arc flash will move away quickly if it is physically possible, and two seconds is a reasonable maximum time for calculations. A person in a bucket truck or a person who has crawled into equipment will need more time to move away.”*

Two calculations are typically provided for labels on locations where there is adequate separation between the line side terminals of the main protective device, and the work location. The “Load Side” calculation provides the incident energy based on the main protective device clearing in the event of an arc flash incident. If the work location or task is such that the main breaker may not trip in the event of an arc flash incident, then the “Line Side” calculation for incident energy should be observed. This could occur if the main breaker is being racked-out, and a fault occurred on the line terminals. For this case, the next upstream device is the one that must clear the fault.

One should always remember that the terms “Line Side” and “Load Side” are always in reference to the main protective device (see example below).

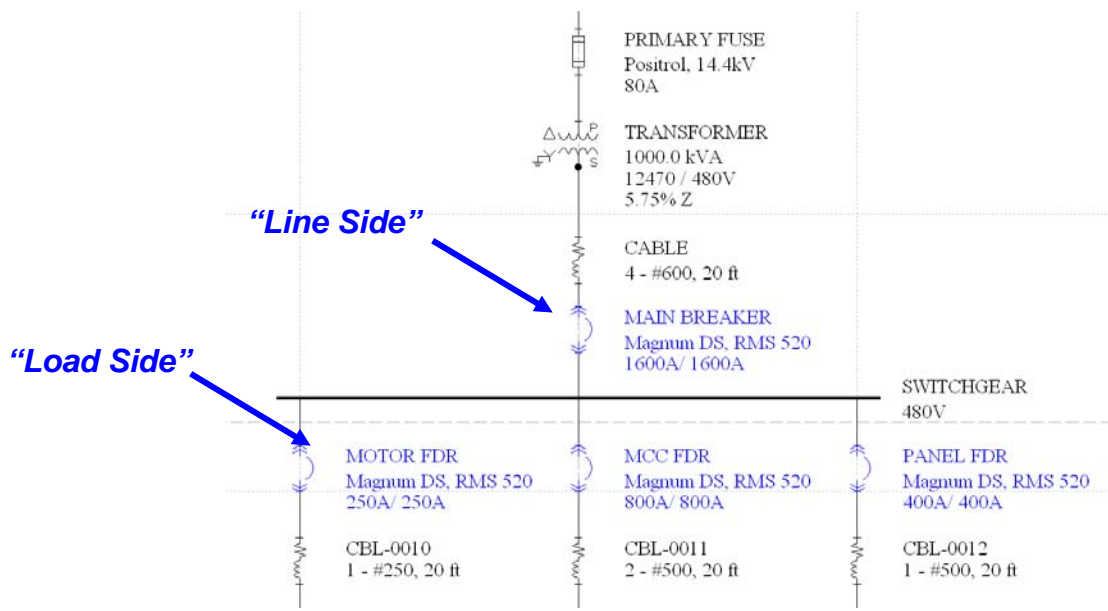


Figure 1: Line Side vs. Load Side

The fault current cannot easily be reduced nor can the working distance be easily increased to lessen the incident energy. In many locations the protective device setting can be adjusted or the trip unit upgraded to decrease the device interrupting time that will in turn decrease the incident energy. For a critical electrical distribution system, such as for Portland State University, it is essential that the system reliability not be compromised. Settings for protective devices cannot be adjusted if the chance of nuisance trips within critical circuits is introduced. *Each location where the hazard is determined to be unacceptable by Portland State University personnel must be individually evaluated to determine the most effective means of reducing the incident energy while maintaining the highest degree of reliability.*

All of the adjustable protective devices listed in Section 4 must be set per the recommended settings of this study to achieve the incident energy levels shown in Table 5.1, Table 5.2, and Table 5.3.

5.4 Arc Flash Summary Table Heading Descriptions

Table 5.1, Table 5.2, and Table 5.3 show results of the SKM PowerTools arc flash hazard analysis. The following column headings describe the results.

Column #1 - Bus Name: The names in this column correlate to the names implemented in the software system model (reference the one-lines included in Appendix D) These locations correspond to plant locations such as main switchboards, panelboards, enclosed breakers, etc.

Column #2 - Protective Device Name: This column lists the name of the device primarily responsible for clearing a potential fault at the associated bus. Again, these device names correlate to the system model.

Column #3 - Bus Voltage (kV): The values in this column show the nominal voltage of the bus location noted in Column #1.

Column #4 - Bus Bolted Fault (kA): This column shows the bolted fault current available for the bus location referenced in Column #1. This current value corresponds to the system operating conditions that will result in the worst-case calculated value for incident energy. (See Column # 14.)

Column #5 - Prot Dev Bolted Fault (kA): This column displays the portion of calculated bolted fault currents (See Column #4) that is contributed through the protective device referenced in Column #2.

Column #6 - Prot Dev Arcing Fault (kA): This column displays the portion of calculated arcing fault currents that is contributed through the protective device referenced in Column #2. These values demonstrate a reduction in available fault current due to the arc resistance.

Column #7 - Trip/Delay Time (sec): This column displays the length of time required by the protective device (See Column #2) to trip in the presence of the arcing fault current calculated in Column #6. For low voltage breakers and fuses, this time represents the total clearing time of the device.

Column #8 - Breaker Opening Time (sec): For circuit breakers tripped by a relay, this column shows the opening time of the breaker. This time is added to the Trip time (See Column #7) to determine the total clearing time used in the calculation of incident energy. (See Column #14.)

Column #9 - Gnd: This column indicates whether the fault location includes a path to ground. Systems with high-resistance or low-resistance grounds are assumed to be ungrounded in the arc flash calculations.

Column #10 - Equip Type: This column indicates whether the equipment is Switchgear, Panel, Cable or Open Air. The equipment type provides a default Gap value, and a distance exponent used in the IEEE incident energy equations.

Column #11 – Gap (mm): This column displays the spacing between bus bars or conductors at the arc location.

Column #12 - Arc Flash Boundary: This column displays the distance within which a person must be clothed in the appropriate PPE (Personal Protection Equipment.) (See Column #14.)

Column #13 - Working Distance: This distance indicates the typical working distance associated with the system location referenced in Column #1.

Column #14 - Incident Energy (cal/cm²): Based on the arcing fault current, the total clearing time of the protective device, the bus bar gap, the grounding method, and the typical working distance, the column displays the results of the arc flash calculations at the reference location. This energy level directly corresponds to the appropriate PPE required for each location. NFPA 70E-2012, Table H.3(b) provides guidance for the selection of PPE based on calculated incident energy exposure.

5.5 Arc Flash Hazard Analysis Recommendations

- 1) All of the adjustable protective devices listed in Section 4 must be set per the recommended settings to achieve the incident energy levels listed in Table 5.1, Table 5.2, and Table 5.3.
- 2) Each location where the arc flash hazard is unacceptable to Portland State University personnel should be individually evaluated to determine the most effective means of reducing the incident energy while maintaining the highest degree of reliability.

Table 5.1 – Arc Flash Analysis Summary Table

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-ARC-A-USB	F-ARC-UTIL-A	0.48	13.13	13.13	7.03	1.275	0.083	Yes	PNL	25	10' 10"	1' 6"	30.8
B-EB-52-U1	F-EB-UTIL-A	12.47	3.43	2.49	2.46	0.067	0.083	Yes	SWG	153	2' 3"	3'	0.9
B-EB-52-U2	F-EB-UTIL-B	12.47	3.43	2.49	2.46	0.067	0.083	Yes	SWG	153	2' 3"	3'	0.9
B-EB-52-U3	MaxTripTime @2.0s	12.47	0.95	0.95	0.95	2	0.000	Yes	SWG	153	5' 2"	3'	2.0
B-EB-USB-5	RLY-EB-52-G1	0.48	13.77	13.77	6.99	1.917	0.083	Yes	SWG	32	17' 3"	2'	28.6
B-MCB BSMT-USB	MaxTripTime @2.0s	0.48	8.00	8.00	5.42	2	0.000	Yes	PNL	25	11' 7"	1' 6"	34.2
B-NASC-USB	F-NASC-UTIL	0.208	15.56	15.56	5.93	2	0.000	Yes	PNL	25	12' 4"	1' 6"	37.8
B-PS3-USB	F-PS3-UTIL	0.208	16.29	16.29	6.13	1.917	0.083	Yes	PNL	25	12' 7"	1' 6"	39.1
B-SBH DISC A-USB	F-SBH-UTIL	0.240	9.36	9.36	4.35	1.917	0.083	No	PNL	25	11' 9"	1' 6"	35.1
B-SBH DISC B-USB	F-SBH-UTIL	0.240	9.36	9.36	4.35	1.917	0.083	No	PNL	25	11' 9"	1' 6"	35.1
B-UP-A-USB	F-UP-UTIL-A	0.48	28.02	28.02	13.44	0.35	0.083	Yes	PNL	25	8' 4"	1' 6"	19.8
B-URBN FP DISC-USB	F-URBN-UTIL-B	0.48	30.75	30.75	14.55	0.307	0.083	Yes	PNL	25	8' 2"	1' 6"	19.4
B-URBN SWBD-USB	F-URBN-UTIL-A	0.48	30.75	30.75	14.55	0.307	0.083	Yes	PNL	25	8' 2"	1' 6"	19.4
B-EB-FP DISC-USB	RLY-EB-52-F3B	0.48	1.90	1.90	1.58	1.917	0.083	Yes	PNL	25	5' 2"	1' 6"	9.1

Table 5.2 – Arc Flash Analysis Summary Table for Locations Greater Than 40 cal/cm²

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-AB ANNEX DISC-USB	F-AB ANNEX-UTIL	0.208	27.20	27.20	8.78	1.917	0.083	Yes	PNL	25	15' 11"	1' 6"	57.7
B-AB DISC-USB	F-AB-UTIL-A	0.208	42.53	42.53	12.02	1.917	0.083	Yes	PNL	25	19' 7"	1' 6"	81.0
B-AB PNLBRD-USB	F-AB-UTIL-B	0.208	42.53	42.53	12.02	1.917	0.083	Yes	PNL	25	19' 7"	1' 6"	81.0
B-ARC-B-USB	F-ARC-UTIL-B	0.208	21.87	21.87	7.53	1.917	0.083	Yes	PNL	25	14' 5"	1' 6"	48.9
B-BHB MSB-A-USB	F-BHB-UTIL-A	0.48	16.05	16.05	8.35	1.917	0.083	Yes	PNL	25	15' 5"	1' 6"	54.6
B-BHB MSB-B-USB	F-BHB-UTIL-B	0.208	27.65	27.65	8.88	1.917	0.083	Yes	PNL	25	16'	1' 6"	58.4
B-BHB MSB-C-USB	F-BHB-UTIL-C	0.208	27.65	27.65	8.88	1.917	0.083	Yes	PNL	25	16'	1' 6"	58.4
B-BLKS K-USB	F-BLKS-UTIL	0.240	31.32	31.32	10.39	1.917	0.083	No	PNL	25	20' 10"	1' 6"	89.7
B-BLKS L1-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.6
B-BLKS L2-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.6
B-BLKS L3-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.6
B-BLKS L4-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.6
B-BLKS L5-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.6
B-BLKS X-USB	F-BLKS-UTIL	0.240	27.94	27.94	9.57	1.917	0.083	No	PNL	25	19' 9"	1' 6"	82.1
B-EB-USB-1	RLY-EB-52-F1F	0.48	23.22	23.22	12.70	1.755	0.083	Yes	SWG	32	25' 3"	2'	50.2
B-EB-USB-2	RLY-EB-52-F2F	0.48	23.50	23.50	12.83	1.717	0.083	Yes	SWG	32	25' 1"	2'	49.7
B-EB-USB-3	RLY-EB-52-F1D	0.208	36.47	36.47	10.08	1.917	0.083	Yes	SWG	32	22' 7"	2'	42.5
B-EB-USB-6	RLY-EB-52-F1B	0.48	23.34	23.34	12.76	1.739	0.083	Yes	SWG	32	25' 3"	2'	50.0
B-EB-USB-7	RLY-EB-52-F2B	0.48	23.50	23.50	12.83	1.718	0.083	Yes	SWG	32	25' 1"	2'	49.7
B-EH A-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	1' 6"	69.9
B-EH B-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	1' 6"	69.9
B-EH C-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	1' 6"	69.9
B-EH E DISC-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	1' 6"	69.9
B-HGDC-USB	F-HGDC-UTIL	0.240	44.76	44.76	11.42	1.917	0.083	Yes	PNL	25	18' 11"	1' 6"	76.6
B-HH 1-USB	F-HH-UTIL	0.240	46.68	46.68	11.77	1.917	0.083	No	PNL	25	22' 8"	1' 6"	102.7

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-HH 2-USB	F-HH-UTIL	0.240	45.86	45.86	11.62	1.917	0.083	No	PNL	25	22' 5"	1' 6"	101.3
B-HOFF-USB	F-HOFF-UTIL	0.208	33.25	33.25	10.11	1.917	0.083	Yes	PNL	25	17' 6"	1' 6"	67.2
B-HSB-USB	F-HSB-UTIL	0.240	48.87	48.87	12.16	1.858	0.083	No	PNL	25	22' 9"	1' 6"	103.3
B-JCB-USB	F-JCB-UTIL	0.208	33.47	33.47	10.16	1.917	0.083	Yes	PNL	25	17' 6"	1' 6"	67.5
B-KHSE-USB	F-KHSE-UTIL	0.208	30.43	30.43	9.50	1.917	0.083	Yes	PNL	25	16' 9"	1' 6"	62.8
B-KNGA-USB	F-KNGA-UTIL	0.240	48.87	48.87	12.16	1.858	0.083	No	PNL	25	22' 9"	1' 6"	103.3
B-MCB PNTHS-USB	MaxTripTime @2.0s	0.48	32.03	32.03	17.73	2	0.000	Yes	PNL	25	25' 4"	1' 6"	123.3
B-MONT-USB	F-MONT-UTIL	0.240	38.00	38.00	11.94	1.917	0.083	No	PNL	25	22' 10"	1' 6"	104.3
B-OND 15 FLR-USB	F-OND-UTIL	0.240	21.35	21.35	7.88	1.917	0.083	No	PNL	25	17' 5"	1' 6"	66.6
B-OND ANNEX SWBD-USB	F-OND ANNEX-UTIL	0.208	38.17	38.17	11.14	1.917	0.083	Yes	PNL	25	18' 8"	1' 6"	74.6
B-OND MAIN SWBD-USB	F-OND-UTIL	0.48	15.96	15.96	8.31	1.917	0.083	Yes	PNL	25	15' 4"	1' 6"	54.4
B-PRKW L1-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-PRKW L2-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-PRKW L3-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-PRKW L4-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-PRKW L5-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-PRKW X-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	1' 6"	103.9
B-SBA-USB	F-SBA-UTIL	0.208	30.43	30.43	9.50	1.917	0.083	Yes	PNL	25	16' 9"	1' 6"	62.8
B-SEC NORTH ECB-USB	F-SEC NORTH-UTIL-B	0.240	40.61	40.61	12.52	1.917	0.083	No	PNL	25	23' 7"	1' 6"	109.8
B-SEC NORTH PNL-USB	F-SEC NORTH-UTIL-A	0.240	40.61	40.61	12.52	1.917	0.083	No	PNL	25	23' 7"	1' 6"	109.8
B-SEC SOUTH DISC 1A-USB	F-SEC SOUTH-UTIL-A	0.240	36.47	36.47	11.59	1.917	0.083	No	PNL	25	22' 5"	1' 6"	101.0
B-SEC SOUTH DISC 2A-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	1' 6"	100.1
B-SEC SOUTH DISC 2B-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	1' 6"	100.1
B-SEC SOUTH PNL 1B-USB	F-SEC SOUTH-UTIL-A	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	1' 6"	100.1
B-SEC SOUTH PNL 1C-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	1' 6"	100.1
B-SEC SOUTH PNL 1D-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	1' 6"	100.1
B-SEH-USB	F-SEH-UTIL	0.208	33.25	33.25	10.11	1.917	0.083	Yes	PNL	25	17' 6"	1' 6"	67.2

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-SH-USB	F-SH-UTIL	0.208	52.21	52.21	13.88	1.917	0.083	Yes	PNL	25	21' 6"	1' 6"	94.7
B-STFR-USB	F-STFR-UTIL	0.240	47.84	47.84	11.98	1.917	0.083	No	PNL	25	22' 11"	1' 6"	104.7
B-STHL L1-USB	F-STHL-UTIL	0.240	18.62	18.62	7.14	1.917	0.083	No	PNL	25	16' 3"	1' 6"	59.9
B-STHL L2-USB	F-STHL-UTIL	0.240	18.45	18.45	7.10	1.917	0.083	No	PNL	25	16' 3"	1' 6"	59.4
B-STHL L3-USB	F-STHL-UTIL	0.240	18.29	18.29	7.05	1.917	0.083	No	PNL	25	16' 2"	1' 6"	59.0
B-STHL L4-USB	F-STHL-UTIL	0.240	18.13	18.13	7.01	1.917	0.083	No	PNL	25	16'	1' 6"	58.6
B-STHL L5-USB	F-STHL-UTIL	0.240	17.97	17.97	6.96	1.917	0.083	No	PNL	25	16'	1' 6"	58.2
B-STHL X-USB	F-STHL-UTIL	0.240	17.81	17.81	6.92	1.917	0.083	No	PNL	25	15' 11"	1' 6"	57.8
B-UCB-USB	F-UCB-UTIL	0.208	31.92	31.92	9.83	1.917	0.083	Yes	PNL	25	17' 2"	1' 6"	65.2
B-UHP-USB	F-UHP-UTIL	0.240	15.55	15.55	6.27	1.917	0.083	No	PNL	25	14' 11"	1' 6"	52.0
B-UP-B-USB	F-UP UTIL-B	0.208	47.01	47.01	12.90	1.917	0.083	Yes	PNL	25	20' 6"	1' 6"	87.4

Table 5.3 – Arc Flash Analysis Summary Table for With Working Distance of 8’

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
<p>Table 5.3 illustrates the arc-flash incident energy at a working distance of 8’. This is the approximate distance the face and body of a qualified person would be from energized equipment when performing a task with a 6’ hot stick. It is important to note that the incident energy values in this table are only applicable when the body and torso are 8’ or over from energized equipment. For arc-flash incident energies at standard working distances as defined by IEEE 1584-2002, please refer to Table 5.1 and Table 5.2.</p>													
B-AB ANNEX DISC-USB	F-AB ANNEX-UTIL	0.208	27.20	27.20	8.78	1.917	0.083	Yes	PNL	25	15' 11"	8'	3.7
B-AB DISC-USB	F-AB-UTIL-A	0.208	42.53	42.53	12.02	1.917	0.083	Yes	PNL	25	19' 7"	8'	5.2
B-AB PNLBRD-USB	F-AB-UTIL-B	0.208	42.53	42.53	12.02	1.917	0.083	Yes	PNL	25	19' 7"	8'	5.2
B-ARC-A-USB	F-ARC-UTIL-A	0.48	13.13	13.13	7.03	1.275	0.083	Yes	PNL	25	10' 10"	8'	2.0
B-ARC-B-USB	F-ARC-UTIL-B	0.208	21.87	21.87	7.53	1.917	0.083	Yes	PNL	25	14' 5"	8'	3.1
B-BHB MSB-A-USB	F-BHB-UTIL-A	0.48	16.05	16.05	8.35	1.917	0.083	Yes	PNL	25	15' 5"	8'	3.5
B-BHB MSB-B-USB	F-BHB-UTIL-B	0.208	27.65	27.65	8.88	1.917	0.083	Yes	PNL	25	16'	8'	3.8
B-BHB MSB-C-USB	F-BHB-UTIL-C	0.208	27.65	27.65	8.88	1.917	0.083	Yes	PNL	25	16'	8'	3.8
B-BLKS K-USB	F-BLKS-UTIL	0.240	31.32	31.32	10.39	1.917	0.083	No	PNL	25	20' 10"	8'	5.8
B-BLKS L1-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	8'	6.6
B-BLKS L2-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	8'	6.6
B-BLKS L3-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	8'	6.6
B-BLKS L4-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	8'	6.6
B-BLKS L5-USB	F-BLKS-UTIL	0.240	37.68	37.68	11.87	1.917	0.083	No	PNL	25	22' 9"	8'	6.6
B-BLKS X-USB	F-BLKS-UTIL	0.240	27.94	27.94	9.57	1.917	0.083	No	PNL	25	19' 9"	8'	5.3
B-EB-52-U1	F-EB-UTIL-A	12.47	3.43	2.49	2.46	0.067	0.083	Yes	SWG	153	2' 3"	8'	0.4
B-EB-52-U2	F-EB-UTIL-B	12.47	3.43	2.49	2.46	0.067	0.083	Yes	SWG	153	2' 3"	8'	0.4
B-EB-52-U3	MaxTripTime @2.0s	12.47	0.95	0.95	0.95	2	0.000	Yes	SWG	153	5' 2"	8'	0.8
B-EB-USB-1	RLY-EB-52-F1F	0.48	23.22	23.22	12.70	1.755	0.083	Yes	SWG	32	25' 3"	8'	6.5

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-EB-USB-2	RLY-EB-52-F2F	0.48	23.50	23.50	12.83	1.717	0.083	Yes	SWG	32	25' 1"	8'	6.4
B-EB-USB-3	RLY-EB-52-F1D	0.208	36.47	36.47	10.08	1.917	0.083	Yes	SWG	32	22' 7"	8'	5.5
B-EB-USB-5	RLY-EB-52-G1	0.48	13.77	13.77	6.99	1.917	0.083	Yes	SWG	32	17' 3"	8'	3.7
B-EB-USB-6	RLY-EB-52-F1B	0.48	23.34	23.34	12.76	1.739	0.083	Yes	SWG	32	25' 3"	8'	6.5
B-EB-USB-7	RLY-EB-52-F2B	0.48	23.50	23.50	12.83	1.718	0.083	Yes	SWG	32	25' 1"	8'	6.5
B-EH A-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	8'	4.5
B-EH B-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	8'	4.5
B-EH C-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	8'	4.5
B-EH E DISC-USB	F-EH-UTIL	0.240	22.72	22.72	8.24	1.917	0.083	No	PNL	25	17' 11"	8'	4.5
B-HGDC-USB	F-HGDC-UTIL	0.240	44.76	44.76	11.42	1.917	0.083	Yes	PNL	25	18' 11"	8'	4.9
B-HH 1-USB	F-HH-UTIL	0.240	46.68	46.68	11.77	1.917	0.083	No	PNL	25	22' 8"	8'	6.6
B-HH 2-USB	F-HH-UTIL	0.240	45.86	45.86	11.62	1.917	0.083	No	PNL	25	22' 5"	8'	6.5
B-HOFF-USB	F-HOFF-UTIL	0.208	33.25	33.25	10.11	1.917	0.083	Yes	PNL	25	17' 6"	8'	4.3
B-HSB-USB	F-HSB-UTIL	0.240	48.87	48.87	12.16	1.858	0.083	No	PNL	25	22' 9"	8'	6.6
B-JCB-USB	F-JCB-UTIL	0.208	33.47	33.47	10.16	1.917	0.083	Yes	PNL	25	17' 6"	8'	4.3
B-KHSE-USB	F-KHSE-UTIL	0.208	30.43	30.43	9.50	1.917	0.083	Yes	PNL	25	16' 9"	8'	4.0
B-KNGA-USB	F-KNGA-UTIL	0.240	48.87	48.87	12.16	1.858	0.083	No	PNL	25	22' 9"	8'	6.6
B-MCB BSMT-USB	MaxTripTime @2.0s	0.48	8.00	8.00	5.42	2	0.000	Yes	PNL	25	11' 7"	8'	2.2
B-MCB PNTHS-USB	MaxTripTime @2.0s	0.48	32.03	32.03	17.73	2	0.000	Yes	PNL	25	25' 4"	8'	7.9
B-MONT-USB	F-MONT-UTIL	0.240	38.00	38.00	11.94	1.917	0.083	No	PNL	25	22' 10"	8'	6.7
B-NASC-USB	F-NASC-UTIL	0.208	15.56	15.56	5.93	2	0.000	Yes	PNL	25	12' 4"	8'	2.4
B-OND 15 FLR-USB	F-OND-UTIL	0.240	21.35	21.35	7.88	1.917	0.083	No	PNL	25	17' 5"	8'	4.3
B-OND ANNEX SWBD-USB	F-OND ANNEX-UTIL	0.208	38.17	38.17	11.14	1.917	0.083	Yes	PNL	25	18' 8"	8'	4.8
B-OND MAIN SWBD-USB	F-OND-UTIL	0.48	15.96	15.96	8.31	1.917	0.083	Yes	PNL	25	15' 4"	8'	3.5
B-PRKW L1-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7
B-PRKW L2-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7
B-PRKW L3-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-PRKW L4-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7
B-PRKW L5-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7
B-PRKW X-USB	F-PRKW-UTIL	0.240	37.80	37.80	11.89	1.917	0.083	No	PNL	25	22' 9"	8'	6.7
B-PS3-USB	F-PS3-UTIL	0.208	16.29	16.29	6.13	1.917	0.083	Yes	PNL	25	12' 7"	8'	2.5
B-SBA-USB	F-SBA-UTIL	0.208	30.43	30.43	9.50	1.917	0.083	Yes	PNL	25	16' 9"	8'	4.0
B-SBH DISC A-USB	F-SBH-UTIL	0.240	9.36	9.36	4.35	1.917	0.083	No	PNL	25	11' 9"	8'	2.3
B-SBH DISC B-USB	F-SBH-UTIL	0.240	9.36	9.36	4.35	1.917	0.083	No	PNL	25	11' 9"	8'	2.3
B-SEC NORTH ECB-USB	F-SEC NORTH-UTIL-B	0.240	40.61	40.61	12.52	1.917	0.083	No	PNL	25	23' 7"	8'	7.0
B-SEC NORTH PNL-USB	F-SEC NORTH-UTIL-A	0.240	40.61	40.61	12.52	1.917	0.083	No	PNL	25	23' 7"	8'	7.0
B-SEC SOUTH DISC 1A-USB	F-SEC SOUTH-UTIL-A	0.240	36.47	36.47	11.59	1.917	0.083	No	PNL	25	22' 5"	8'	6.5
B-SEC SOUTH DISC 2A-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	8'	6.4
B-SEC SOUTH DISC 2B-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	8'	6.4
B-SEC SOUTH PNL 1B-USB	F-SEC SOUTH-UTIL-A	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	8'	6.4
B-SEC SOUTH PNL 1C-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	8'	6.4
B-SEC SOUTH PNL 1D-USB	F-SEC SOUTH-UTIL-B	0.240	36.06	36.06	11.50	1.917	0.083	No	PNL	25	22' 3"	8'	6.4
B-SEH-USB	F-SEH-UTIL	0.208	33.25	33.25	10.11	1.917	0.083	Yes	PNL	25	17' 6"	8'	4.3
B-SH-USB	F-SH-UTIL	0.208	52.21	52.21	13.88	1.917	0.083	Yes	PNL	25	21' 6"	8'	6.1
B-STFR-USB	F-STFR-UTIL	0.240	47.84	47.84	11.98	1.917	0.083	No	PNL	25	22' 11"	8'	6.7
B-STHL L1-USB	F-STHL-UTIL	0.240	18.62	18.62	7.14	1.917	0.083	No	PNL	25	16' 3"	8'	3.8
B-STHL L2-USB	F-STHL-UTIL	0.240	18.45	18.45	7.10	1.917	0.083	No	PNL	25	16' 3"	8'	3.8
B-STHL L3-USB	F-STHL-UTIL	0.240	18.29	18.29	7.05	1.917	0.083	No	PNL	25	16' 2"	8'	3.8
B-STHL L4-USB	F-STHL-UTIL	0.240	18.13	18.13	7.01	1.917	0.083	No	PNL	25	16'	8'	3.8
B-STHL L5-USB	F-STHL-UTIL	0.240	17.97	17.97	6.96	1.917	0.083	No	PNL	25	16'	8'	3.7
B-STHL X-USB	F-STHL-UTIL	0.240	17.81	17.81	6.92	1.917	0.083	No	PNL	25	15' 11"	8'	3.7
B-UCB-USB	F-UCB-UTIL	0.208	31.92	31.92	9.83	1.917	0.083	Yes	PNL	25	17' 2"	8'	4.2
B-UHP-USB	F-UHP-UTIL	0.240	15.55	15.55	6.27	1.917	0.083	No	PNL	25	14' 11"	8'	3.3
B-UP-A-USB	F-UP-UTIL-A	0.48	28.02	28.02	13.44	0.35	0.083	Yes	PNL	25	8' 4"	8'	1.3

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-UP-B-USB	F-UP UTIL-B	0.208	47.01	47.01	12.90	1.917	0.083	Yes	PNL	25	20' 6"	8'	5.6
B-URBN FP DISC-USB	F-URBN-UTIL-B	0.48	30.75	30.75	14.55	0.307	0.083	Yes	PNL	25	8' 2"	8'	1.3
B-URBN SWBD-USB	F-URBN-UTIL-A	0.48	30.75	30.75	14.55	0.307	0.083	Yes	PNL	25	8' 2"	8'	1.3
B-EB-FP DISC-USB	RLY-EB-52-F3B	0.48	1.90	1.90	1.58	1.917	0.083	Yes	PNL	25	5' 2"	8'	0.6

A. APPENDIX A – SHORT-CIRCUIT INPUT REPORT

Input Report Interpretation

Input Data Tables are provided on the following pages. The following is a guide for interpreting the input data.

1. Generation Contribution Data

- Utility contribution data includes the available fault current in MVA and amps, per unit impedance on a 100 MVA base, X/R, and the line-to-line bus voltage.
- Generator data includes the generator kW rating, X”d, X/R, line-to-line voltage and per unit impedance on a 100 MVA base.

2. Motor Contribution Data

Motor Contribution Data includes the horsepower rating (base kVA rating), speed, subtransient reactance adjusted per the *First Cycle Duty* multipliers described in IEEE Std 141-1993 (Red Book), per-unit impedance on a 100 MVA base, and the bus voltage. X/R ratios for induction motors are obtained from IEEE Std C37.010-1999.

3. Feeder Data

Feeder data includes the following cable and bus data: length, impedance in ohms per 1,000 feet, and per-unit impedance on a 100 MVA base. Impedance values for conductors were obtained from Tables 4A-7 and 4A-8 of IEEE Std 141-1993 (Red Book). The impedance values are based on conductor temperatures of 75°C for Copper and 90°C for Aluminum.

4. Transformer Data

Transformer data includes the transformer kVA rating and per-unit impedance on a 100 MVA base. Unless otherwise provided, transformer X/R ratios are obtained from IEEE Std C37.010-1999.

Short-Circuit Input Report

PSU - Non-West Campus Loop
Portland, OR
ESE0008355 / TQSISE0008355.1
Feb 21, 2013 17:45:50

Page 1

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ALL PU VALUES ARE EXPRESSED ON A 100 MVA BASE.

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
BWY-ARC-B-USB-B2-USB	B-ARC-B-USB	B-ARC-B2-USB	1	208	1.000 FEET	2000	Copper
Duct Material: Busway							
+/- Impedance: 0.0066 + J 0.0035 Ohms/1000 ft 0.0153 + J 0.0081 PU							
Z0 Impedance: 0.0392 + J 0.0187 Ohms/1000 ft 0.0906 + J 0.0432 PU							
BWY-BHB MSB-A	B-BHB MSB-A-USB	B-BHB MSB-A SWBD-USB	1	480	5.0 FEET	2500	Copper
Duct Material: Busway							
+/- Impedance: 0.0055 + J 0.0031 Ohms/1000 ft 0.0119 + J 0.0067 PU							
Z0 Impedance: 0.1375 + J 0.0775 Ohms/1000 ft 0.2984 + J 0.1682 PU							
C-BLKS JUNC-BLKS K	B-BLKS JUNC	B-BLKS K-USB	1	240	8.0 FEET	2	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.2020 + J 0.0467 Ohms/1000 ft 2.81 + J 0.6486 PU							
Z0 Impedance: 0.3211 + J 0.1188 Ohms/1000 ft 4.46 + J 1.65 PU							
C-BLKS JUNC-BLKS L1	B-BLKS JUNC	B-BLKS L1-USB	1	240	5.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 0.6649 + J 0.3602 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.06 + J 0.9158 PU							
C-BLKS JUNC-BLKS L2	B-BLKS JUNC	B-BLKS L2-USB	1	240	5.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 0.6649 + J 0.3602 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.06 + J 0.9158 PU							
C-BLKS JUNC-BLKS L3	B-BLKS JUNC	B-BLKS L3-USB	1	240	5.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 0.6649 + J 0.3602 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.06 + J 0.9158 PU							
C-BLKS JUNC-BLKS L4	B-BLKS JUNC	B-BLKS L4-USB	1	240	5.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 0.6649 + J 0.3602 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.06 + J 0.9158 PU							
C-BLKS JUNC-BLKS L5	B-BLKS JUNC	B-BLKS L5-USB	1	240	5.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 0.6649 + J 0.3602 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.06 + J 0.9158 PU							
C-BLKS JUNC-BLKS X	B-BLKS JUNC	B-BLKS X-USB	1	240	5.0 FEET	6	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.5100 + J 0.0548 Ohms/1000 ft 4.43 + J 0.4757 PU							
Z0 Impedance: 0.8123 + J 0.1394 Ohms/1000 ft 7.05 + J 1.21 PU							

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-EB-52-U1-TX-USB-1	B-EB-52-U1	TX-EB-USB-1 P	1	12470	80.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0066 + J	0.0026	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0105 + J	0.0066	PU		
C-EB-52-U1-TX-USB-3	B-EB-52-U1	TX-EB-USB-3 P	1	12470	75.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0062 + J	0.0024	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0098 + J	0.0062	PU		
C-EB-52-U1-TX-USB-6	B-EB-52-U1	TX-EB-USB-6 P	1	12470	90.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0074 + J	0.0029	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0118 + J	0.0075	PU		
C-EB-52-U2-TX-USB-2	B-EB-52-U2	TX-EB-USB-2 P	1	12470	20.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0016 + J	0.00065	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0026 + J	0.0017	PU		
C-EB-52-U2-TX-USB-5	B-EB-52-U2	TX-EB-USB-5 P	1	12470	180.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0148 + J	0.0059	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0236 + J	0.0149	PU		
C-EB-52-U2-TX-USB-7	B-EB-52-U2	TX-EB-USB-7 P	1	12470	50.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0041 + J	0.0016	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0065 + J	0.0041	PU		
BWY-EB-52-U3-52-U1	B-EB-52-U3 Busway	B-EB-52-U1	1	12470	25.0 FEET	1200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0119 + J	0.0619 Ohms/1000 ft	0.00019 + J	0.00100	PU		
	Z0 Impedance: 0.0710 + J	0.3314 Ohms/1000 ft	0.0011 + J	0.0053	PU		
BWY-EB-52-U3-52-U2	B-EB-52-U3 Busway	B-EB-52-U2	1	12470	25.0 FEET	1200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0119 + J	0.0619 Ohms/1000 ft	0.00019 + J	0.00100	PU		
	Z0 Impedance: 0.0710 + J	0.3314 Ohms/1000 ft	0.0011 + J	0.0053	PU		
C-EB-52-U3-TX-FP	B-EB-52-U3	TX-EB-FIRE PUMP P	1	12470	25.0 FEET	2	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2020 + J	0.0547 Ohms/1000 ft	0.0032 + J	0.00088	PU		
	Z0 Impedance: 0.3211 + J	0.1392 Ohms/1000 ft	0.0052 + J	0.0022	PU		

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
BWY-EB-GEN-USB-8	G-EB BUS	USB-8 P	1	4160	150.0 FEET	1200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0119 + J 0.0619	Ohms/1000 ft 0.0103 + J 0.0537	PU				
	Z0 Impedance: 0.0710 + J 0.3314	Ohms/1000 ft 0.0615 + J 0.2872	PU				
C-EB-TX-FP-FP DISC	TX-EB-FIRE PUMP S	B-EB-FP DISC-USB	1	480	20.0 FEET	2	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2020 + J 0.0467	Ohms/1000 ft 1.75 + J 0.4054	PU				
	Z0 Impedance: 0.3211 + J 0.1188	Ohms/1000 ft 2.79 + J 1.03	PU				
BWY-EB-TX-USB-2-USB-2	TX-EB-USB-2 S	B-EB-USB-2	1	480	3.0 FEET	4000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0033 + J 0.0019	Ohms/1000 ft 0.0043 + J 0.0025	PU				
	Z0 Impedance: 0.0196 + J 0.0101	Ohms/1000 ft 0.0255 + J 0.0132	PU				
BWY-EB-TX-USB-3-USB-3	TX-EB-USB-3 S	B-EB-USB-3	1	208	3.0 FEET	4000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0033 + J 0.0019	Ohms/1000 ft 0.0229 + J 0.0132	PU				
	Z0 Impedance: 0.0196 + J 0.0101	Ohms/1000 ft 0.1359 + J 0.0700	PU				
BWY-EB-TX-USB-5-USB-5	TX-EB-USB-5 S	B-EB-USB-5	1	480	3.0 FEET	4000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0033 + J 0.0019	Ohms/1000 ft 0.0043 + J 0.0025	PU				
	Z0 Impedance: 0.0196 + J 0.0101	Ohms/1000 ft 0.0255 + J 0.0132	PU				
BWY-EB-TX-USB-7-USB-7	TX-EB-USB-7 S	B-EB-USB-7	1	480	3.0 FEET	4000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0033 + J 0.0019	Ohms/1000 ft 0.0043 + J 0.0025	PU				
	Z0 Impedance: 0.0196 + J 0.0101	Ohms/1000 ft 0.0255 + J 0.0132	PU				
BWY-EB-USB-1-USB-2	B-EB-USB-1	B-EB-USB-2	1	480	3.0 FEET	3200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0047 + J 0.0026	Ohms/1000 ft 0.0061 + J 0.0034	PU				
	Z0 Impedance: 0.1175 + J 0.0650	Ohms/1000 ft 0.1530 + J 0.0846	PU				
BWY-EB-USB-6-USB-7	B-EB-USB-6	B-EB-USB-7	1	480	3.0 FEET	3200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0047 + J 0.0026	Ohms/1000 ft 0.0061 + J 0.0034	PU				
	Z0 Impedance: 0.1175 + J 0.0650	Ohms/1000 ft 0.1530 + J 0.0846	PU				
C-EB-USB-8-52-U3	USB-8 S	B-EB-52-U3	1	12470	90.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0074 + J 0.0029	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0118 + J 0.0075	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-EH JUNC-EH A	B-EH JUNC	B-EH A-USB	1	240	15.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 1.99 + J 1.08	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 3.17 + J 2.75	PU				
C-EH JUNC-EH B	B-EH JUNC	B-EH B-USB	1	240	15.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 1.99 + J 1.08	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 3.17 + J 2.75	PU				
C-EH JUNC-EH C	B-EH JUNC	B-EH C-USB	1	240	15.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 1.99 + J 1.08	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 3.17 + J 2.75	PU				
C-EH JUNC-EH DISC	B-EH JUNC	B-EH E DISC-USB	1	240	15.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 1.99 + J 1.08	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 3.17 + J 2.75	PU				
C-HH 1-HH 2	B-HH JUNC	B-HH 2-USB	1	240	3.0 FEET	2	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.2020 + J 0.0585	Ohms/1000 ft 1.05 + J 0.3047	PU				
	Z0 Impedance: 0.6366 + J 0.1440	Ohms/1000 ft 3.32 + J 0.7500	PU				
C-HH JUNC-HH 1	B-HH JUNC	B-HH 1-USB	1	240	1.000 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.1398 + J 0.0901	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 0.4405 + J 0.2219	PU				
BWY-MCB-UTIL-A-PNTHS USB	TX-MCB UTIL-A S	B-MCB PNTHS-USB	1	480	50.0 FEET	2000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0076 + J 0.0039	Ohms/1000 ft 0.1649 + J 0.0846	PU				
	Z0 Impedance: 0.1900 + J 0.0975	Ohms/1000 ft 4.12 + J 2.12	PU				
BWY-MCB-UTIL-B-PNTHS USB	TX-MCB UTIL-B S	B-MCB PNTHS-USB	1	480	50.0 FEET	2000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0076 + J 0.0039	Ohms/1000 ft 0.1649 + J 0.0846	PU				
	Z0 Impedance: 0.1900 + J 0.0975	Ohms/1000 ft 4.12 + J 2.12	PU				
BWY-MCB-UTIL-BSMT-USB	TX-MCB BSMT UTIL S	B-MCB BSMT-USB	1	480	15.0 FEET	2000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0076 + J 0.0039	Ohms/1000 ft 0.0495 + J 0.0254	PU				
	Z0 Impedance: 0.1900 + J 0.0975	Ohms/1000 ft 1.24 + J 0.6348	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-PRKW JUNC-PRKW L1	PRKW JUNC	B-PRKW L1-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-PRKW JUNC-PRKW L2	PRKW JUNC	B-PRKW L2-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-PRKW JUNC-PRKW L3	PRKW JUNC	B-PRKW L3-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-PRKW JUNC-PRKW L4	PRKW JUNC	B-PRKW L4-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-PRKW JUNC-PRKW L5	PRKW JUNC	B-PRKW L5-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-PRKW JUNC-PRKW LX	PRKW JUNC	B-PRKW X-USB	1	240	10.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 1.40 + J 0.9010	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 4.40 + J 2.22	PU				
C-SBH JUNC-SBH A	B-SBH JUNC	B-SBH DISC A-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.7979 + J 0.4323	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 1.27 + J 1.10	PU				
C-SBH JUNC-SBH B	B-SBH JUNC	B-SBH DISC B-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.7979 + J 0.4323	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 1.27 + J 1.10	PU				
C-SEC JUNC-SEC 1A	B-SEC SOUTH-A JUNC	B-SEC SOUTH DISC 1A-USB	1	240	6.0 FEET	4/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0640 + J 0.0497	Ohms/1000 ft 0.6667 + J 0.5177	PU				
	Z0 Impedance: 0.2017 + J 0.1224	Ohms/1000 ft 2.10 + J 1.28	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-SEC JUNC-SEC 1B	B-SEC SOUTH-A JUNC	B-SEC SOUTH PNL 1B-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.8385 + J 0.5406	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 2.64 + J 1.33	PU				
C-SEC JUNC-SEC 1C	B-SEC SOUTH-B JUNC	B-SEC SOUTH PNL 1C-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.8385 + J 0.5406	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 2.64 + J 1.33	PU				
C-SEC JUNC-SEC 1D	B-SEC SOUTH-B JUNC	B-SEC SOUTH PNL 1D-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.8385 + J 0.5406	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 2.64 + J 1.33	PU				
C-SEC JUNC-SEC 2A	B-SEC SOUTH-B JUNC	B-SEC SOUTH DISC 2A-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.8385 + J 0.5406	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 2.64 + J 1.33	PU				
C-SEC JUNC-SEC 2B	B-SEC SOUTH-B JUNC	B-SEC SOUTH DISC 2B-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0805 + J 0.0519	Ohms/1000 ft 0.8385 + J 0.5406	PU				
	Z0 Impedance: 0.2537 + J 0.1278	Ohms/1000 ft 2.64 + J 1.33	PU				
C-STHL JUNC-STHL L1	B-STHL JUNC	B-STHL L1-USB	1	240	4.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.5319 + J 0.2882	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 0.8451 + J 0.7326	PU				
C-STHL JUNC-STHL L2	B-STHL JUNC	B-STHL L2-USB	1	240	5.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.6649 + J 0.3602	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 1.06 + J 0.9158	PU				
C-STHL JUNC-STHL L3	B-STHL JUNC	B-STHL L3-USB	1	240	6.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.7979 + J 0.4323	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 1.27 + J 1.10	PU				
C-STHL JUNC-STHL L4	B-STHL JUNC	B-STHL L4-USB	1	240	7.0 FEET	3/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0766 + J 0.0415	Ohms/1000 ft 0.9309 + J 0.5043	PU				
	Z0 Impedance: 0.1217 + J 0.1055	Ohms/1000 ft 1.48 + J 1.28	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-STHL JUNC-STHL L5	B-STHL JUNC	B-STHL L5-USB	1	240	8.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 1.06 + J 0.5764 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.69 + J 1.47 PU							
C-STHL JUNC-STHL X	B-STHL JUNC	B-STHL X-USB	1	240	9.0 FEET	3/0	Copper
Duct Material: Non-Magnetic							
+/- Impedance: 0.0766 + J 0.0415 Ohms/1000 ft 1.20 + J 0.6484 PU							
Z0 Impedance: 0.1217 + J 0.1055 Ohms/1000 ft 1.90 + J 1.65 PU							
BWY-UTIL-BK-EB-52-U2	EB-UTIL-B BUS	B-EB-52-U2	1	12470	3.0 FEET	1200	Copper
Duct Material: Busway							
+/- Impedance: 0.0119 + J 0.0619 Ohms/1000 ft 0.00002 + J 0.00012 PU							
Z0 Impedance: 0.0710 + J 0.3314 Ohms/1000 ft 0.00014 + J 0.00064 PU							

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-AB ANNEX-UTIL	TX-AB ANNEX-UTIL P	YG 12470.0	B-AB ANNEX DISC-USB	YG 208.00	225.00	225.00
	Pos. Seq. Z%: 0.522 + j 2.03	(Zpu 2.32 + j 9.04)	Shell Type			
	Zero Seq. Z%: 0.522 + j 2.03	(Pri - Sec: 2.32 + j 9.04)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-AB-UTIL-A	TX-AB-UTIL-A P	YG 12470.0	B-AB DISC-USB	YG 208.00	300.00	300.00
	Pos. Seq. Z%: 0.398 + j 1.65	(Zpu 1.33 + j 5.51)	Shell Type			
	Zero Seq. Z%: 0.398 + j 1.65	(Pri - Sec: 1.33 + j 5.51)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-AB-UTIL-B	TX-AB-UTIL-B P	YG 12470.0	B-AB PNLBRD-USB	YG 208.00	300.00	300.00
	Pos. Seq. Z%: 0.398 + j 1.65	(Zpu 1.33 + j 5.51)	Shell Type			
	Zero Seq. Z%: 0.398 + j 1.65	(Pri - Sec: 1.33 + j 5.51)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-ARC-UTIL-A	TX-ARC-UTIL-A P	YG 12470.0	B-ARC-A-USB	YG 480.00	750.00	750.00
	Pos. Seq. Z%: 1.04 + j 5.43	(Zpu 1.38 + j 7.24)	Shell Type			
	Zero Seq. Z%: 1.04 + j 5.43	(Pri - Sec: 1.38 + j 7.24)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-ARC-UTIL-B	TX-ARC-UTIL-B P	YG 12470.0	B-ARC-B-USB	YG 208.00	300.00	300.00
	Pos. Seq. Z%: 0.829 + j 3.44	(Zpu 2.76 + j 11.47)	Shell Type			
	Zero Seq. Z%: 0.829 + j 3.44	(Pri - Sec: 2.76 + j 11.47)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-BHB-UTIL-A	TX-BHB-UTIL-A P	YG 12470.0	B-BHB MSB-A-USB	YG 480.00	1000.00	1000.00
	Pos. Seq. Z%: 0.988 + j 5.64	(Zpu 0.988 + j 5.64)	Shell Type			
	Zero Seq. Z%: 0.988 + j 5.64	(Pri - Sec: 0.988 + j 5.64)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-BHB-UTIL-B	TX-BHB-UTIL-B P	YG 12470.0	B-BHB MSB-B-USB	YG	208.00	500.00
	Pos. Seq. Z%: 0.954 + J 4.48	(Zpu 1.91 + j 8.96)	Shell Type			
	Zero Seq. Z%: 0.954 + J 4.48	(Pri - Sec: 1.91 + j 8.96)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-BHB-UTIL-C	TX-BHB-UTIL-C P	YG 12470.0	B-BHB MSB-C-USB	YG	208.00	500.00
	Pos. Seq. Z%: 0.954 + J 4.48	(Zpu 1.91 + j 8.96)	Shell Type			
	Zero Seq. Z%: 0.954 + J 4.48	(Pri - Sec: 1.91 + j 8.96)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-BLKS-UTIL	TX-BLKS-UTIL P	D 12470.0	B-BLKS JUNC	D	240.00	300.00
	Pos. Seq. Z%: 0.374 + J 1.56	(Zpu 1.25 + j 5.18)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-EB-FIRE PUMP	TX-EB-FIRE PUMP P	D 12470.0	TX-EB-FIRE PUMP S	YG	480.00	75.00
	Pos. Seq. Z%: 1.40 + J 4.41	(Zpu 18.65 + j 58.85)	Shell Type			
	Zero Seq. Z%: 1.40 + J 4.41	(Sec 18.65 + j 58.85 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	30.00 Deg.			
TX-EB-USB-1	TX-EB-USB-1 P	YG 12470.0	TX-EB-USB-1 S	YG	480.00	1500.00
	Pos. Seq. Z%: 0.867 + J 5.67	(Zpu 0.578 + j 3.78)	Shell Type			
	Zero Seq. Z%: 0.867 + J 5.67	(Pri - Sec: 0.578 + j 3.78)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-EB-USB-2	TX-EB-USB-2 P	YG 12470.0	TX-EB-USB-2 S	YG	480.00	1500.00
	Pos. Seq. Z%: 0.854 + J 5.59	(Zpu 0.569 + j 3.72)	Shell Type			
	Zero Seq. Z%: 0.854 + J 5.59	(Pri - Sec: 0.569 + j 3.72)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-EB-USB-3	TX-EB-USB-3 P	YG 12470.0	TX-EB-USB-3 S	YG	208.00	1000.00
	Pos. Seq. Z%: 1.17 + j 6.71 (Zpu 1.17 + j 6.71)		Shell Type			
	Zero Seq. Z%: 1.17 + j 6.71 (Pri - Sec: 1.17 + j 6.71)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-EB-USB-5	TX-EB-USB-5 P	YG 12470.0	TX-EB-USB-5 S	YG	480.00	1500.00
	Pos. Seq. Z%: 0.878 + j 5.74 (Zpu 0.585 + j 3.83)		Shell Type			
	Zero Seq. Z%: 0.878 + j 5.74 (Pri - Sec: 0.585 + j 3.83)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-EB-USB-6	TX-EB-USB-6 P	YG 12470.0	TX-EB-USB-6 S	YG	480.00	1500.00
	Pos. Seq. Z%: 0.861 + j 5.63 (Zpu 0.574 + j 3.76)		Shell Type			
	Zero Seq. Z%: 0.861 + j 5.63 (Pri - Sec: 0.574 + j 3.76)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-EB-USB-7	TX-EB-USB-7 P	YG 12470.0	TX-EB-USB-7 S	YG	480.00	1500.00
	Pos. Seq. Z%: 0.854 + j 5.59 (Zpu 0.569 + j 3.72)		Shell Type			
	Zero Seq. Z%: 0.854 + j 5.59 (Pri - Sec: 0.569 + j 3.72)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-EB-USB-8	USB-8 P	D 4160.00	USB-8 S	YG	12470.0	2500.00
	Pos. Seq. Z%: 0.506 + j 5.31 (Zpu 0.202 + j 2.12)		Shell Type			
	Zero Seq. Z%: 0.506 + j 5.31 (Sec 0.202 + j 2.12 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-EH-UTIL	TX-EH-UTIL P	D 12470.0	B-EH JUNC	D	240.00	300.00
	Pos. Seq. Z%: 0.562 + j 2.33 (Zpu 1.87 + j 7.78)		Shell Type			
	Zero Seq. Z%: 9999. + j 9999. (Pri Open, Sec Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-HGDC-UTIL	TX-HGDC-UTIL P	YG 12470.0	B-HGDC-USB	YG 240.00	500.00	500.00
	Pos. Seq. Z%: 0.520 + J 2.45	(Zpu 1.04 + j 4.89)	Shell Type			
	Zero Seq. Z%: 0.520 + J 2.45	(Pri - Sec: 1.04 + j 4.89)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-HH-UTIL	TX-HH-UTIL P	D 12470.0	B-HH JUNC	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.437 + J 2.05	(Zpu 0.875 + j 4.11)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-HOFF-UTIL	TX-HOFF-UTIL P	YG 12470.0	B-HOFF-USB	YG 208.00	300.00	300.00
	Pos. Seq. Z%: 0.552 + J 2.29	(Zpu 1.84 + j 7.65)	Shell Type			
	Zero Seq. Z%: 0.552 + J 2.29	(Pri - Sec: 1.84 + j 7.65)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-HSB-UTIL	TX-HSB-UTIL P	D 12470.0	B-HSB-USB	D 240.00	300.00	300.00
	Pos. Seq. Z%: 0.316 + J 1.31	(Zpu 1.05 + j 4.37)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-JCB-UTIL	TX-JCB-UTIL P	YG 12470.0	B-JCB-USB	YG 208.00	750.00	750.00
	Pos. Seq. Z%: 1.11 + J 5.80	(Zpu 1.47 + j 7.73)	Shell Type			
	Zero Seq. Z%: 1.11 + J 5.80	(Pri - Sec: 1.47 + j 7.73)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				
TX-KHSE-UTIL	TX-KHSE-UTIL P	YG 12470.0	B-KHSE-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.854 + J 4.01	(Zpu 1.71 + j 8.02)	Shell Type			
	Zero Seq. Z%: 0.854 + J 4.01	(Pri - Sec: 1.71 + j 8.02)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 0.000 Deg.				

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-KNGA-UTIL	TX-KNGA-UTIL P	D 12470.0	B-KNGA-USB	D 240.00	300.00	300.00
	Pos. Seq. Z%: 0.316 + J 1.31	(Zpu 1.05 + j 4.37)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-MCB BSMT UTIL	TX-MCB BSMT UTIL P	D 12470.0	TX-MCB BSMT UTIL S	YG 480.00	300.00	300.00
	Pos. Seq. Z%: 4.50 + J 0.000	(Zpu 15.00 + j 0.000)	Shell Type			
	Zero Seq. Z%: 4.50 + J 0.000	(Sec 15.00 + j 0.000 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	30.00 Deg.			
TX-MONT-UTIL	TX-MONT-UTIL P	D 12470.0	B-MONT-USB	D 240.00	300.00	300.00
	Pos. Seq. Z%: 0.374 + J 1.56	(Zpu 1.25 + j 5.18)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-NASC-UTIL	TX-NASC-UTIL P	YG 12470.0	B-NASC-USB	YG 208.00	150.00	150.00
	Pos. Seq. Z%: 0.671 + J 2.41	(Zpu 4.48 + j 16.05)	Shell Type			
	Zero Seq. Z%: 0.671 + J 2.41	(Pri - Sec: 4.48 + j 16.05)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	0.000 Deg.			
TX-OND ANNEX-UTIL	TX-OND ANNEX-UTIL P	D 12470.0	B-OND ANNEX SWBD-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.666 + J 3.13	(Zpu 1.33 + j 6.26)	Shell Type			
	Zero Seq. Z%: 0.666 + J 3.13	(Sec 1.33 + j 6.26 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	30.00 Deg.			
TX-OND-UTIL MAIN	TX-OND-UTIL P	D 12470.0	B-OND MAIN SWBD-USB	YG 480.00	300.00	300.00
	Pos. Seq. Z%: 0.468 + J 1.94	(Zpu 1.56 + j 6.48)	Shell Type			
	Zero Seq. Z%: 0.468 + J 1.94	(Sec 1.56 + j 6.48 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.):	30.00 Deg.			

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-OND-UTIL UPSTAIRS	TX-OND-UTIL P	D 12470.0	B-OND 15 FLR-USB	D 240.00	500.00	500.00
	Pos. Seq. Z%: 1.37 + J 5.02	(Zpu 2.74 + j 10.03)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-PRKW-UTIL	TX-PRKW-UTIL P	D 12470.0	PRKW JUNC	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.437 + J 2.05	(Zpu 0.875 + j 4.11)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-PS3-UTIL	TX-PS3-UTIL P	YG 12470.0	B-PS3-USB	YG 208.00	150.00	150.00
	Pos. Seq. Z%: 0.671 + J 2.41	(Zpu 4.48 + j 16.05)	Shell Type			
	Zero Seq. Z%: 0.671 + J 2.41	(Pri - Sec: 4.48 + j 16.05)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SBA-UTIL	TX-SBA-UTIL P	YG 12470.0	B-SBA-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.854 + J 4.01	(Zpu 1.71 + j 8.02)	Shell Type			
	Zero Seq. Z%: 0.854 + J 4.01	(Pri - Sec: 1.71 + j 8.02)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SBH-UTIL	TX-SBH-UTIL S	D 12470.0	B-SBH JUNC	D 240.00	75.00	75.00
	Pos. Seq. Z%: 0.645 + J 1.71	(Zpu 8.61 + j 22.83)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SEC NORTH-UTIL-A	TX-SEC NORTH-UTIL-A P	D 12470.0	B-SEC NORTH PNL-USB	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.527 + J 2.47	(Zpu 1.05 + j 4.95)	Shell Type			
	Zero Seq. Z%: 9999. + J 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-SEC NORTH-UTIL-B	TX-SEC NORTH-UTIL-B P	D 12470.0	B-SEC NORTH ECB-USB	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.527 + j 2.47	(Zpu 1.05 + j 4.95)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SEC SOUTH-UTIL-A	TX-SEC SOUTH-UTIL-A P	D 12470.0	B-SEC SOUTH-A JUNC	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.527 + j 2.47	(Zpu 1.05 + j 4.95)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SEC SOUTH-UTIL-B	TX-SEC SOUTH-UTIL-B P	D 12470.0	B-SEC SOUTH-B JUNC	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.527 + j 2.47	(Zpu 1.05 + j 4.95)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SEH-UTIL	TX-SEH-UTIL P	YG 12470.0	B-SEH-USB	YG 208.00	300.00	300.00
	Pos. Seq. Z%: 0.552 + j 2.29	(Zpu 1.84 + j 7.65)	Shell Type			
	Zero Seq. Z%: 0.552 + j 2.29	(Pri - Sec: 1.84 + j 7.65)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-SH-UTIL	TX-SH-UTIL P	YG 12470.0	B-SH-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.458 + j 2.15	(Zpu 0.916 + j 4.30)	Shell Type			
	Zero Seq. Z%: 0.458 + j 2.15	(Pri - Sec: 0.916 + j 4.30)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-STFR-UTIL	TX-STFR-UTIL P	D 12470.0	B-STFR-USB	D 240.00	500.00	500.00
	Pos. Seq. Z%: 0.437 + j 2.05	(Zpu 0.875 + j 4.11)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-STHL-UTIL	TX-STHL-UTIL P	D 12470.0	B-STHL JUNC	D 240.00	150.00	150.00
	Pos. Seq. Z%: 0.577 + j 1.70	(Zpu 3.85 + j 11.36)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-UCB-UTIL	TX-UCB-UTIL P	YG 12470.0	B-UCB-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.812 + j 3.81	(Zpu 1.63 + j 7.63)	Shell Type			
	Zero Seq. Z%: 0.812 + j 3.81	(Pri - Sec: 1.63 + j 7.63)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-UHP-UTIL	TX-UHP-UTIL P	D 12470.0	B-UHP-USB	D 240.00	225.00	225.00
	Pos. Seq. Z%: 0.845 + j 3.29	(Zpu 3.76 + j 14.64)	Shell Type			
	Zero Seq. Z%: 9999. + j 9999.	(Pri Open, Sec Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-UP-UTIL-A	TX-UP-UTIL-A P	YG 12470.0	B-UP-A-USB	YG 480.00	1500.00	1500.00
	Pos. Seq. Z%: 0.498 + j 3.26	(Zpu 0.332 + j 2.17)	Shell Type			
	Zero Seq. Z%: 0.498 + j 3.26	(Pri - Sec: 0.332 + j 2.17)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-UP UTIL-B	TX-UP UTIL-B P	YG 12470.0	B-UP-B-USB	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.395 + j 1.86	(Zpu 0.791 + j 3.72)	Shell Type			
	Zero Seq. Z%: 0.395 + j 1.86	(Pri - Sec: 0.791 + j 3.72)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					
TX-URBN-UTIL-A	TX-URBN-UTIL-A P	YG 12470.0	B-URBN SWBD-USB	YG 480.00	750.00	750.00
	Pos. Seq. Z%: 0.281 + j 1.47	(Zpu 0.374 + j 1.96)	Shell Type			
	Zero Seq. Z%: 0.281 + j 1.47	(Pri - Sec: 0.374 + j 1.96)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.					

TRANSFORMER INPUT DATA

```

=====
TRANSFORMER          PRIMARY RECORD          VOLTS * SECONDARY RECORD          VOLTS FULL-LOAD NOMINAL
NAME                 NO NAME                 L-L      NO NAME                 L-L    KVA      KVA
=====
TX-URBN-UTIL-B      TX-URBN-UTIL-B P      YG 12470.0  B-URBN FP DISC-USB      YG   480.00  750.00   750.00
Pos. Seq. Z%:      0.281 + j 1.47      (Zpu 0.374 + j 1.96 ) Shell Type
Zero Seq. Z%:      0.281 + j 1.47      ( Pri - Sec: 0.374 + j 1.96 )
Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 0.000 Deg.
  
```

GENERATION CONTRIBUTION DATA

=====						
BUS	CONTRIBUTION		VOLTAGE			
NAME	NAME		L-L	MVA	X*d	X/R
=====						
EB-UTIL-B BUS	EB-UTIL-B		12470.0	107.74		
	Three Phase	Contribution:	4988.33 AMPS		3.27	
	Single Line to Ground	Contribution:	4210.97 AMPS		2.56	
	Pos Sequence Impedance (100 MVA Base)		0.2712 + J		0.8876 PU	
	Zero Sequence Impedance (100 MVA Base)		0.6572 + J		1.30 PU	
G-EB BUS	G-EB GEN		4160.00	3.75	0.1000	27.58
	KG: 0.9434	xdsat: 1.60	Excitation Limit: 1.30	Ik -	ON	
	Pos Sequence Impedance (100 MVA Base)		0.0967 + J		2.67 PU	
TX-AB ANNEX-UTIL P	AB ANNEX-UTIL		12470.0	114.64		
	Three Phase	Contribution:	5307.96 AMPS		3.57	
	Single Line to Ground	Contribution:	4401.36 AMPS		2.90	
	Pos Sequence Impedance (100 MVA Base)		0.2355 + J		0.8399 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5581 + J		1.30 PU	
TX-AB-UTIL-A P	AB-UTIL-A		12470.0	116.40		
	Three Phase	Contribution:	5388.99 AMPS		3.92	
	Single Line to Ground	Contribution:	4471.73 AMPS		3.15	
	Pos Sequence Impedance (100 MVA Base)		0.2124 + J		0.8325 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5137 + J		1.30 PU	
TX-AB-UTIL-B P	AB-UTIL-B		12470.0	116.40		
	Three Phase	Contribution:	5388.99 AMPS		3.92	
	Single Line to Ground	Contribution:	4471.73 AMPS		3.15	
	Pos Sequence Impedance (100 MVA Base)		0.2124 + J		0.8325 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5137 + J		1.30 PU	
TX-ARC-UTIL-A P	ARC-UTIL-A		12470.0	111.89		
	Three Phase	Contribution:	5180.19 AMPS		4.28	
	Single Line to Ground	Contribution:	4330.91 AMPS		3.09	
	Pos Sequence Impedance (100 MVA Base)		0.2033 + J		0.8703 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5795 + J		1.31 PU	
TX-ARC-UTIL-B P	ARC-UTIL-B		12470.0	111.89		
	Three Phase	Contribution:	5180.19 AMPS		4.28	
	Single Line to Ground	Contribution:	4330.91 AMPS		3.09	
	Pos Sequence Impedance (100 MVA Base)		0.2033 + J		0.8703 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5795 + J		1.31 PU	
TX-BHB-UTIL-A P	BHB-UTIL-A		12470.0	113.21		
	Three Phase	Contribution:	5241.57 AMPS		3.83	
	Single Line to Ground	Contribution:	4375.25 AMPS		3.03	
	Pos Sequence Impedance (100 MVA Base)		0.2229 + J		0.8547 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5502 + J		1.30 PU	
TX-BHB-UTIL-B P	BHB-UTIL-B		12470.0	113.65		
	Three Phase	Contribution:	5261.72 AMPS		3.98	
	Single Line to Ground	Contribution:	4397.84 AMPS		3.12	
	Pos Sequence Impedance (100 MVA Base)		0.2143 + J		0.8534 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5347 + J		1.30 PU	
TX-BHB-UTIL-C P	BHB-UTIL-C		12470.0	113.65		
	Three Phase	Contribution:	5261.72 AMPS		3.98	
	Single Line to Ground	Contribution:	4397.84 AMPS		3.12	
	Pos Sequence Impedance (100 MVA Base)		0.2143 + J		0.8534 PU	
	Zero Sequence Impedance (100 MVA Base)		0.5347 + J		1.30 PU	

GENERATION CONTRIBUTION DATA

=====					
BUS	CONTRIBUTION	VOLTAGE			
NAME	NAME	L-L	MVA	X*d	X/R
=====					
TX-BLKS-UTIL P	BLKS-UTIL	12470.0	168.23		
	Three Phase Contribution:	7788.97 AMPS	0.8433		
	Single Line to Ground Contribution:	6234.71 AMPS	0.7047		
	Pos Sequence Impedance (100 MVA Base)	0.4544 + J	0.3832 PU		
	Zero Sequence Impedance (100 MVA Base)	0.9123 + J	0.5168 PU		
TX-EH-UTIL P	EH-UTIL	12470.0	108.17		
	Three Phase Contribution:	5008.20 AMPS	2.70		
	Single Line to Ground Contribution:	4114.65 AMPS	2.25		
	Pos Sequence Impedance (100 MVA Base)	0.3215 + J	0.8667 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7257 + J	1.35 PU		
TX-HGDC-UTIL P	HGDC-UTIL	12470.0	258.06		
	Three Phase Contribution:	11948.0 AMPS	1.92		
	Single Line to Ground Contribution:	10455.4 AMPS	1.39		
	Pos Sequence Impedance (100 MVA Base)	0.1792 + J	0.3436 PU		
	Zero Sequence Impedance (100 MVA Base)	0.4186 + J	0.3904 PU		
TX-HH-UTIL P	HH-UTIL	12470.0	230.13		
	Three Phase Contribution:	10654.6 AMPS	1.64		
	Single Line to Ground Contribution:	8885.03 AMPS	1.16		
	Pos Sequence Impedance (100 MVA Base)	0.2264 + J	0.3709 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5674 + J	0.4427 PU		
TX-HOFF-UTIL P	HOFF-UTIL	12470.0	171.36		
	Three Phase Contribution:	7933.67 AMPS	0.8630		
	Single Line to Ground Contribution:	6360.29 AMPS	0.7187		
	Pos Sequence Impedance (100 MVA Base)	0.4418 + J	0.3813 PU		
	Zero Sequence Impedance (100 MVA Base)	0.8898 + J	0.5119 PU		
TX-HSB-UTIL P	HSB-UTIL	12470.0	214.85		
	Three Phase Contribution:	9947.58 AMPS	1.21		
	Single Line to Ground Contribution:	8189.81 AMPS	0.9537		
	Pos Sequence Impedance (100 MVA Base)	0.2963 + J	0.3589 PU		
	Zero Sequence Impedance (100 MVA Base)	0.6347 + J	0.4527 PU		
TX-JCB-UTIL P	JCB-UTIL	12470.0	201.46		
	Three Phase Contribution:	9327.21 AMPS	1.09		
	Single Line to Ground Contribution:	7635.09 AMPS	0.8700		
	Pos Sequence Impedance (100 MVA Base)	0.3363 + J	0.3651 PU		
	Zero Sequence Impedance (100 MVA Base)	0.6998 + J	0.4639 PU		
TX-KHSE-UTIL P	KHSE-UTIL	12470.0	108.03		
	Three Phase Contribution:	5001.52 AMPS	3.03		
	Single Line to Ground Contribution:	4153.36 AMPS	2.41		
	Pos Sequence Impedance (100 MVA Base)	0.2904 + J	0.8790 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7029 + J	1.33 PU		
TX-KNGA-UTIL P	KNGA-UTIL	12470.0	214.85		
	Three Phase Contribution:	9947.58 AMPS	1.21		
	Single Line to Ground Contribution:	8189.81 AMPS	0.9537		
	Pos Sequence Impedance (100 MVA Base)	0.2963 + J	0.3589 PU		
	Zero Sequence Impedance (100 MVA Base)	0.6347 + J	0.4527 PU		

GENERATION CONTRIBUTION DATA

=====					
BUS	CONTRIBUTION	VOLTAGE			
NAME	NAME	L-L	MVA	X*d	X/R
=====					
TX-MCB BSMT UTIL S	MCB BSMT INF UTIL	480.00	6.67		
	Three Phase Contribution:	8018.80 AMPS	4.15		
	Single Line to Ground Contribution:	8018.80 AMPS	4.15		
	Pos Sequence Impedance (100 MVA Base)	3.51 + J	14.58 PU		
	Zero Sequence Impedance (100 MVA Base)	3.51 + J	14.58 PU		
TX-MCB UTIL-A S	MCB INF UTIL-A	480.00	13.16		
	Three Phase Contribution:	15826.5 AMPS	5.24		
	Single Line to Ground Contribution:	15826.5 AMPS	5.24		
	Pos Sequence Impedance (100 MVA Base)	1.42 + J	7.47 PU		
	Zero Sequence Impedance (100 MVA Base)	1.42 + J	7.47 PU		
TX-MCB UTIL-B S	MCB INF UTIL-B	480.00	13.89		
	Three Phase Contribution:	16705.7 AMPS	5.24		
	Single Line to Ground Contribution:	16705.7 AMPS	5.24		
	Pos Sequence Impedance (100 MVA Base)	1.35 + J	7.07 PU		
	Zero Sequence Impedance (100 MVA Base)	1.35 + J	7.07 PU		
TX-MONT-UTIL P	MONT-UTIL	12470.0	168.23		
	Three Phase Contribution:	7788.97 AMPS	0.8433		
	Single Line to Ground Contribution:	6234.71 AMPS	0.7047		
	Pos Sequence Impedance (100 MVA Base)	0.4544 + J	0.3832 PU		
	Zero Sequence Impedance (100 MVA Base)	0.9123 + J	0.5168 PU		
TX-NASC-UTIL P	NASC-UTIL	12470.0	83.50		
	Three Phase Contribution:	3865.93 AMPS	1.84		
	Single Line to Ground Contribution:	2909.51 AMPS	1.88		
	Pos Sequence Impedance (100 MVA Base)	0.5713 + J	1.05 PU		
	Zero Sequence Impedance (100 MVA Base)	1.10 + J	2.11 PU		
TX-OND ANNEX-UTIL P	OND ANNEX-UTIL	12470.0	114.55		
	Three Phase Contribution:	5303.73 AMPS	4.16		
	Single Line to Ground Contribution:	4430.33 AMPS	3.25		
	Pos Sequence Impedance (100 MVA Base)	0.2042 + J	0.8487 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5143 + J	1.30 PU		
TX-OND-UTIL P	OND-UTIL	12470.0	115.07		
	Three Phase Contribution:	5327.72 AMPS	4.37		
	Single Line to Ground Contribution:	4457.23 AMPS	3.38		
	Pos Sequence Impedance (100 MVA Base)	0.1938 + J	0.8471 PU		
	Zero Sequence Impedance (100 MVA Base)	0.4957 + J	1.29 PU		
TX-PRKW-UTIL P	PRKW-UTIL	12470.0	230.13		
	Three Phase Contribution:	10654.6 AMPS	1.64		
	Single Line to Ground Contribution:	8885.03 AMPS	1.16		
	Pos Sequence Impedance (100 MVA Base)	0.2264 + J	0.3709 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5674 + J	0.4427 PU		
TX-PS3-UTIL P	PS3-UTIL	12470.0	262.81		
	Three Phase Contribution:	12167.8 AMPS	2.04		
	Single Line to Ground Contribution:	10726.3 AMPS	1.46		
	Pos Sequence Impedance (100 MVA Base)	0.1672 + J	0.3418 PU		
	Zero Sequence Impedance (100 MVA Base)	0.3970 + J	0.3850 PU		

GENERATION CONTRIBUTION DATA

=====					
BUS	CONTRIBUTION	VOLTAGE			
NAME	NAME	L-L	MVA	X*d	X/R
=====					
TX-SBA-UTIL P	SBA-UTIL	12470.0	108.03		
	Three Phase Contribution:	5001.52 AMPS	3.03		
	Single Line to Ground Contribution:	4153.36 AMPS	2.41		
	Pos Sequence Impedance (100 MVA Base)	0.2904 + J	0.8790 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7029 + J	1.33 PU		
TX-SBH-UTIL S	SBH-UTIL	12470.0	144.92		
	Three Phase Contribution:	6709.76 AMPS	0.7733		
	Single Line to Ground Contribution:	5527.95 AMPS	0.6695		
	Pos Sequence Impedance (100 MVA Base)	0.5458 + J	0.4221 PU		
	Zero Sequence Impedance (100 MVA Base)	0.9962 + J	0.5536 PU		
TX-SEC NORTH-UTIL-A P	SEC NORTH-UTIL-A	12470.0	115.57		
	Three Phase Contribution:	5350.72 AMPS	3.67		
	Single Line to Ground Contribution:	4430.20 AMPS	2.98		
	Pos Sequence Impedance (100 MVA Base)	0.2277 + J	0.8348 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5413 + J	1.30 PU		
TX-SEC NORTH-UTIL-B P	SEC NORTH-UTIL-B	12470.0	115.57		
	Three Phase Contribution:	5350.72 AMPS	3.67		
	Single Line to Ground Contribution:	4430.20 AMPS	2.98		
	Pos Sequence Impedance (100 MVA Base)	0.2277 + J	0.8348 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5413 + J	1.30 PU		
TX-SEC SOUTH-UTIL-A P	SEC SOUTH-UTIL-A	12470.0	115.57		
	Three Phase Contribution:	5350.72 AMPS	3.67		
	Single Line to Ground Contribution:	4430.20 AMPS	2.98		
	Pos Sequence Impedance (100 MVA Base)	0.2277 + J	0.8348 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5413 + J	1.30 PU		
TX-SEC SOUTH-UTIL-B P	SEC SOUTH-UTIL-B	12470.0	115.57		
	Three Phase Contribution:	5350.72 AMPS	3.67		
	Single Line to Ground Contribution:	4430.20 AMPS	2.98		
	Pos Sequence Impedance (100 MVA Base)	0.2277 + J	0.8348 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5413 + J	1.30 PU		
TX-SEH-UTIL P	SEH-UTIL	12470.0	171.36		
	Three Phase Contribution:	7933.67 AMPS	0.8630		
	Single Line to Ground Contribution:	6360.29 AMPS	0.7187		
	Pos Sequence Impedance (100 MVA Base)	0.4418 + J	0.3813 PU		
	Zero Sequence Impedance (100 MVA Base)	0.8898 + J	0.5119 PU		
TX-SH-UTIL P	SH-UTIL	12470.0	108.17		
	Three Phase Contribution:	5008.20 AMPS	2.70		
	Single Line to Ground Contribution:	4114.65 AMPS	2.25		
	Pos Sequence Impedance (100 MVA Base)	0.3215 + J	0.8667 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7257 + J	1.35 PU		
TX-STFR-UTIL P	STFR-UTIL	12470.0	230.13		
	Three Phase Contribution:	10654.6 AMPS	1.64		
	Single Line to Ground Contribution:	8885.03 AMPS	1.16		
	Pos Sequence Impedance (100 MVA Base)	0.2264 + J	0.3709 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5674 + J	0.4427 PU		

GENERATION CONTRIBUTION DATA

=====					
BUS	CONTRIBUTION	VOLTAGE			
NAME	NAME	L-L	MVA	X*d	X/R
=====					
TX-STHL-UTIL P	STHL-UTIL	12470.0	199.62		
	Three Phase Contribution:	9242.35 AMPS	1.15		
	Single Line to Ground Contribution:	7834.35 AMPS	0.9399		
	Pos Sequence Impedance (100 MVA Base)	0.3279 + J	0.3787 PU		
	Zero Sequence Impedance (100 MVA Base)	0.6361 + J	0.4568 PU		
TX-UCB-UTIL P	UCB-UTIL	12470.0	111.72		
	Three Phase Contribution:	5172.33 AMPS	4.24		
	Single Line to Ground Contribution:	4319.57 AMPS	3.06		
	Pos Sequence Impedance (100 MVA Base)	0.2057 + J	0.8712 PU		
	Zero Sequence Impedance (100 MVA Base)	0.5872 + J	1.31 PU		
TX-UHP-UTIL P	UHP-UTIL	12470.0	279.04		
	Three Phase Contribution:	12919.1 AMPS	2.53		
	Single Line to Ground Contribution:	11530.1 AMPS	1.73		
	Pos Sequence Impedance (100 MVA Base)	0.1315 + J	0.3334 PU		
	Zero Sequence Impedance (100 MVA Base)	0.3387 + J	0.3768 PU		
TX-UP-UTIL-A P	UP-UTIL-A	12470.0	94.79		
	Three Phase Contribution:	4388.84 AMPS	2.95		
	Single Line to Ground Contribution:	3447.73 AMPS	2.57		
	Pos Sequence Impedance (100 MVA Base)	0.3388 + J	0.9990 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7829 + J	1.76 PU		
TX-UP UTIL-B P	UP UTIL-B	12470.0	94.61		
	Three Phase Contribution:	4380.19 AMPS	2.91		
	Single Line to Ground Contribution:	3439.67 AMPS	2.54		
	Pos Sequence Impedance (100 MVA Base)	0.3434 + J	0.9997 PU		
	Zero Sequence Impedance (100 MVA Base)	0.7911 + J	1.76 PU		
TX-URBN-UTIL-A P	URBN-UTIL-A	12470.0	103.49		
	Three Phase Contribution:	4791.28 AMPS	2.39		
	Single Line to Ground Contribution:	3932.60 AMPS	1.97		
	Pos Sequence Impedance (100 MVA Base)	0.3727 + J	0.8916 PU		
	Zero Sequence Impedance (100 MVA Base)	0.8511 + J	1.37 PU		
TX-URBN-UTIL-B P	URBN-UTIL-B	12470.0	103.49		
	Three Phase Contribution:	4791.28 AMPS	2.39		
	Single Line to Ground Contribution:	3932.60 AMPS	1.97		
	Pos Sequence Impedance (100 MVA Base)	0.3727 + J	0.8916 PU		
	Zero Sequence Impedance (100 MVA Base)	0.8511 + J	1.37 PU		

B. APPENDIX B – SHORT-CIRCUIT RESULTS

PSU - Non-West Campus Loop
Portland, OR
ESE0008355 / TQISE0008355.1
Feb 21, 2013 17:45:50

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SKM POWER*TOOLS FOR WINDOWS
A_FAULT SHORT CIRCUIT ANALYSIS REPORT
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T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

B-AB ANNEX DISC-USB	3P Duty: 27.199 KA AT -75.49 DEG (9.80 MVA)	X/R:	3.86
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0011 + J 0.0043 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 27.199 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 27.199 KA			
TX-AB ANNEX-UTIL	TX-AB ANNEX-UTIL P	27.199 KA	ANG: 104.51
B-AB DISC-USB	3P Duty: 42.535 KA AT -76.35 DEG (15.32 MVA)	X/R:	4.12
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0007 + J 0.0027 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 42.535 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 42.535 KA			
TX-AB-UTIL-A	TX-AB-UTIL-A P	42.535 KA	ANG: 103.65
B-AB PNLBRD-USB	3P Duty: 42.535 KA AT -76.35 DEG (15.32 MVA)	X/R:	4.12
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0007 + J 0.0027 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 42.535 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 42.535 KA			
TX-AB-UTIL-B	TX-AB-UTIL-B P	42.535 KA	ANG: 103.65
B-ARC-A-USB	3P Duty: 14.551 KA AT -78.94 DEG (12.10 MVA)	X/R:	5.12
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0037 + J 0.0187 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 14.551 KA			
MOLDED CASE CIRCUIT BREAKER < 20KA 16.341 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 14.690 KA			
TX-ARC-UTIL-A	TX-ARC-UTIL-A P	14.551 KA	ANG: 101.06
B-ARC-B-USB	3P Duty: 21.867 KA AT -76.48 DEG (7.88 MVA)	X/R:	4.16
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0013 + J 0.0053 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 21.867 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 21.867 KA			
TX-ARC-UTIL-B	TX-ARC-UTIL-B P	21.867 KA	ANG: -256.48
B-BHB MSB-A-USB	3P Duty: 18.195 KA AT -79.44 DEG (15.13 MVA)	X/R:	5.37
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0028 + J 0.0150 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 18.195 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 18.555 KA			
TX-BHB-UTIL-A	TX-BHB-UTIL-A P	18.195 KA	ANG: -259.44
B-BHB MSB-B-USB	3P Duty: 27.648 KA AT -77.79 DEG (9.96 MVA)	X/R:	4.62
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0009 + J 0.0042 OHMS			
LOW VOLTAGE POWER CIRCUIT BREAKER 27.648 KA			
MOLDED CASE CIRCUIT BREAKER > 20KA 27.648 KA			
TX-BHB-UTIL-B	TX-BHB-UTIL-B P	27.648 KA	ANG: -257.79

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-BHB MSB-C-USB          3P Duty: 27.648 KA AT -77.79 DEG ( 9.96 MVA) X/R: 4.62
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0009 + J 0.0042 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 27.648 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 27.648 KA
TX-BHB-UTIL-C          TX-BHB-UTIL-C P          27.648 KA    ANG: 102.21

B-BLKS K-USB            3P Duty: 31.323 KA AT -54.05 DEG ( 13.02 MVA) X/R: 1.38
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0026 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 31.323 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 31.323 KA
C-BLKS JUNC-BLKS K          B-BLKS JUNC          31.323 KA    ANG: -54.05

B-BLKS L1-USB          3P Duty: 37.681 KA AT -68.22 DEG ( 15.66 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.681 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.681 KA
C-BLKS JUNC-BLKS L1          B-BLKS JUNC          37.681 KA    ANG: 111.78

B-BLKS L2-USB          3P Duty: 37.681 KA AT -68.22 DEG ( 15.66 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.681 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.681 KA
C-BLKS JUNC-BLKS L2          B-BLKS JUNC          37.681 KA    ANG: -68.22

B-BLKS L3-USB          3P Duty: 37.681 KA AT -68.22 DEG ( 15.66 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.681 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.681 KA
C-BLKS JUNC-BLKS L3          B-BLKS JUNC          37.681 KA    ANG: -68.22

B-BLKS L4-USB          3P Duty: 37.681 KA AT -68.22 DEG ( 15.66 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.681 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.681 KA
C-BLKS JUNC-BLKS L4          B-BLKS JUNC          37.681 KA    ANG: -68.22

B-BLKS L5-USB          3P Duty: 37.681 KA AT -68.22 DEG ( 15.66 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.681 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.681 KA
C-BLKS JUNC-BLKS L5          B-BLKS JUNC          37.681 KA    ANG: -68.22

B-BLKS X-USB            3P Duty: 27.943 KA AT -44.59 DEG ( 11.62 MVA) X/R: 0.99
  
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THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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	VOLTAGE: 240.	EQUIV. IMPEDANCE=	0.0035 + J 0.0035	OHMS	
	LOW VOLTAGE POWER CIRCUIT BREAKER		27.943 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA		27.943 KA		
	C-BLKS JUNC-BLKS X	B-BLKS JUNC	27.943 KA	ANG: -44.59	
B-EB-52-U1	3P Duty: 5.907 KA AT -75.14 DEG (127.58 MVA)	X/R:	5.14		
	VOLTAGE: 12470.	EQUIV. IMPEDANCE=	0.3126 + J 1.1781	OHMS	
	C-EB-52-U3-52-U1	B-EB-52-U3	5.907 KA	ANG: -75.14	
B-EB-52-U2	3P Duty: 5.920 KA AT -75.13 DEG (127.86 MVA)	X/R:	5.13		
	VOLTAGE: 12470.	EQUIV. IMPEDANCE=	0.3122 + J 1.1755	OHMS	
	C-UTIL-BK-EB-52-U2	EB-UTIL-B BUS	4.988 KA	ANG: -253.01	
	C-EB-52-U3-52-U2	B-EB-52-U3	0.953 KA	ANG: -86.25	
B-EB-52-U3	3P Duty: 5.914 KA AT -75.13 DEG (127.74 MVA)	X/R:	5.14		
	VOLTAGE: 12470.	EQUIV. IMPEDANCE=	0.3123 + J 1.1765	OHMS	
	C-EB-USB-8-52-U3	USB-8 S	0.953 KA	ANG: 93.74	
	C-EB-52-U3-52-U2	B-EB-52-U2	4.982 KA	ANG: -253.02	
B-EB-USB-1	3P Duty: 26.415 KA AT -80.11 DEG (21.96 MVA)	X/R:	6.16		
	VOLTAGE: 480.	EQUIV. IMPEDANCE=	0.0018 + J 0.0103	OHMS	
	LOW VOLTAGE POWER CIRCUIT BREAKER		26.415 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA		27.691 KA		
	C-EB-USB-1-USB-2	B-EB-USB-2	26.415 KA	ANG: -260.11	
B-EB-USB-2	3P Duty: 26.441 KA AT -80.18 DEG (21.98 MVA)	X/R:	6.20		
	VOLTAGE: 480.	EQUIV. IMPEDANCE=	0.0018 + J 0.0103	OHMS	
	LOW VOLTAGE POWER CIRCUIT BREAKER		26.441 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA		27.758 KA		
	C-EB-TX-USB-2-USB-2	TX-EB-USB-2 S	26.441 KA	ANG: -260.18	
B-EB-USB-3	3P Duty: 36.465 KA AT -79.37 DEG (13.14 MVA)	X/R:	5.54		
	VOLTAGE: 208.	EQUIV. IMPEDANCE=	0.0006 + J 0.0032	OHMS	
	LOW VOLTAGE POWER CIRCUIT BREAKER		36.465 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA		37.431 KA		
	C-EB-TX-USB-3-USB-3	TX-EB-USB-3 S	36.465 KA	ANG: -259.37	
B-EB-USB-5	3P Duty: 25.794 KA AT -80.06 DEG (21.44 MVA)	X/R:	6.11		
	VOLTAGE: 480.	EQUIV. IMPEDANCE=	0.0019 + J 0.0106	OHMS	
	LOW VOLTAGE POWER CIRCUIT BREAKER		25.794 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA		27.000 KA		
	C-EB-TX-USB-5-USB-5	TX-EB-USB-5 S	25.794 KA	ANG: -260.05	
B-EB-USB-6	3P Duty: 26.407 KA AT -80.08 DEG (21.95 MVA)	X/R:	6.14		

THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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	VOLTAGE: 480.	EQUIV. IMPEDANCE= 0.0018 + J 0.0103 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	26.407 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	27.666 KA		
	C-EB-USB-6-USB-7	B-EB-USB-7	26.407 KA	ANG: -260.08
B-EB-USB-7	3P Duty: 26.432 KA AT -80.15 DEG (21.98 MVA)		X/R: 6.19	
	VOLTAGE: 480.	EQUIV. IMPEDANCE= 0.0018 + J 0.0103 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	26.432 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	27.733 KA		
	C-EB-TX-USB-7-USB-7	TX-EB-USB-7 S	26.432 KA	ANG: -260.15
B-EH A-USB	3P Duty: 22.718 KA AT -66.69 DEG (9.44 MVA)		X/R: 2.32	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0024 + J 0.0056 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	22.718 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	22.718 KA		
	C-EH JUNC-EH A	B-EH JUNC	22.718 KA	ANG: -246.69
B-EH B-USB	3P Duty: 22.718 KA AT -66.69 DEG (9.44 MVA)		X/R: 2.32	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0024 + J 0.0056 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	22.718 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	22.718 KA		
	C-EH JUNC-EH B	B-EH JUNC	22.718 KA	ANG: -66.69
B-EH C-USB	3P Duty: 22.718 KA AT -66.69 DEG (9.44 MVA)		X/R: 2.32	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0024 + J 0.0056 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	22.718 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	22.718 KA		
	C-EH JUNC-EH C	B-EH JUNC	22.718 KA	ANG: -66.69
B-EH E DISC-USB	3P Duty: 22.718 KA AT -66.69 DEG (9.44 MVA)		X/R: 2.32	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0024 + J 0.0056 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	22.718 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	22.718 KA		
	C-EH JUNC-EH DISC	B-EH JUNC	22.718 KA	ANG: -66.69
B-HGDC-USB	3P Duty: 44.761 KA AT -76.87 DEG (18.61 MVA)		X/R: 4.29	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0007 + J 0.0030 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER	44.761 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	44.761 KA		
	TX-HGDC-UTIL	TX-HGDC-UTIL P	44.761 KA	ANG: 103.13
B-HH 1-USB	3P Duty: 50.812 KA AT -74.80 DEG (21.12 MVA)		X/R: 3.68	
	VOLTAGE: 240.	EQUIV. IMPEDANCE= 0.0007 + J 0.0026 OHMS		

THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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	LOW VOLTAGE POWER CIRCUIT BREAKER	50.812 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	50.812 KA		
	C-HH JUNC-HH 1	B-HH JUNC	50.812 KA	ANG: -254.80
B-HH 2-USB	3P Duty: 45.858 KA AT -65.76 DEG (19.06 MVA)		X/R: 2.22	
	VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0028 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	45.858 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	45.858 KA		
	C-HH 1-HH 2	B-HH JUNC	45.858 KA	ANG: -65.76
B-HOFF-USB	3P Duty: 33.251 KA AT -74.12 DEG (11.98 MVA)		X/R: 3.51	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0010 + J 0.0035 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	33.251 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	33.251 KA		
	TX-HOFF-UTIL	TX-HOFF-UTIL P	33.251 KA	ANG: 105.88
B-HSB-USB	3P Duty: 48.870 KA AT -74.07 DEG (20.31 MVA)		X/R: 3.50	
	VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0008 + J 0.0027 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	48.870 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	48.870 KA		
	TX-HSB-UTIL	TX-HSB-UTIL P	48.870 KA	ANG: 105.93
B-JCB-USB	3P Duty: 33.473 KA AT -77.39 DEG (12.06 MVA)		X/R: 4.47	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0008 + J 0.0035 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	33.473 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	33.473 KA		
	TX-JCB-UTIL	TX-JCB-UTIL P	33.473 KA	ANG: 102.61
B-KHSE-USB	3P Duty: 30.433 KA AT -77.34 DEG (10.96 MVA)		X/R: 4.45	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0009 + J 0.0039 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	30.433 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	30.433 KA		
	TX-KHSE-UTIL	TX-KHSE-UTIL P	30.433 KA	ANG: 102.66
B-KNGA-USB	3P Duty: 48.870 KA AT -74.07 DEG (20.31 MVA)		X/R: 3.50	
	VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0008 + J 0.0027 OHMS			
	LOW VOLTAGE POWER CIRCUIT BREAKER	48.870 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA	48.870 KA		
	TX-KNGA-UTIL	TX-KNGA-UTIL P	48.870 KA	ANG: 105.93
B-MCB BSMT-USB	3P Duty: 7.999 KA AT -76.29 DEG (6.65 MVA)		X/R: 4.10	
	VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0082 + J 0.0337 OHMS			

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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LOW VOLTAGE POWER CIRCUIT BREAKER	7.999 KA				
MOLDED CASE CIRCUIT BREAKER < 20KA	8.538 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	7.999 KA				
C-MCB-UTIL-BSMT-USB	TX-MCB BSMT UTIL S	7.999 KA	ANG:	103.71	
B-MCB PNTHS-USB	3P Duty: 32.032 KA AT -78.08 DEG (26.63 MVA)	X/R:	4.74		
VOLTAGE:	480. EQUIV. IMPEDANCE= 0.0018 + J 0.0085 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	32.032 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	32.032 KA				
C-MCB-UTIL-B-PNTHS USB	TX-MCB UTIL-B S	16.442 KA	ANG:	-258.05	
C-MCB-UTIL-A-PNTHS USB	TX-MCB UTIL-A S	15.590 KA	ANG:	101.89	
B-MONT-USB	3P Duty: 41.312 KA AT -72.99 DEG (17.17 MVA)	X/R:	3.27		
VOLTAGE:	240. EQUIV. IMPEDANCE= 0.0010 + J 0.0032 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	41.312 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	41.312 KA				
TX-MONT-UTIL	TX-MONT-UTIL P	41.312 KA	ANG:	107.01	
B-NASC-USB	3P Duty: 15.562 KA AT -73.56 DEG (5.61 MVA)	X/R:	3.39		
VOLTAGE:	208. EQUIV. IMPEDANCE= 0.0022 + J 0.0074 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	15.562 KA				
MOLDED CASE CIRCUIT BREAKER < 20KA	15.827 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	15.562 KA				
TX-NASC-UTIL	TX-NASC-UTIL P	15.562 KA	ANG:	106.44	
B-OND 15 FLR-USB	3P Duty: 21.349 KA AT -74.91 DEG (8.87 MVA)	X/R:	3.71		
VOLTAGE:	240. EQUIV. IMPEDANCE= 0.0017 + J 0.0063 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	21.349 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	21.349 KA				
TX-OND-UTIL UPSTAIRS	TX-OND-UTIL P	21.349 KA	ANG:	105.09	
B-OND ANNEX SWBD-USB	3P Duty: 38.166 KA AT -77.79 DEG (13.75 MVA)	X/R:	4.62		
VOLTAGE:	208. EQUIV. IMPEDANCE= 0.0007 + J 0.0031 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	38.166 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	38.166 KA				
TX-OND ANNEX-UTIL	TX-OND ANNEX-UTIL P	38.166 KA	ANG:	-257.79	
B-OND MAIN SWBD-USB	3P Duty: 15.962 KA AT -76.53 DEG (13.27 MVA)	X/R:	4.17		
VOLTAGE:	480. EQUIV. IMPEDANCE= 0.0040 + J 0.0169 OHMS				
LOW VOLTAGE POWER CIRCUIT BREAKER	15.962 KA				
MOLDED CASE CIRCUIT BREAKER < 20KA	17.111 KA				
MOLDED CASE CIRCUIT BREAKER > 20KA	15.962 KA				
TX-OND-UTIL MAIN	TX-OND-UTIL P	15.962 KA	ANG:	103.47	

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-PRKW L1-USB          3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW L1          PRKW JUNC          40.555 KA    ANG: -65.08

B-PRKW L2-USB          3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW L2          PRKW JUNC          40.555 KA    ANG: -65.08

B-PRKW L3-USB          3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW L3          PRKW JUNC          40.555 KA    ANG: -65.08

B-PRKW L4-USB          3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW L4          PRKW JUNC          40.555 KA    ANG: -65.08

B-PRKW L5-USB          3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW L5          PRKW JUNC          40.555 KA    ANG: -65.08

B-PRKW X-USB           3P Duty: 40.555 KA AT -65.08 DEG ( 16.86 MVA) X/R: 2.15
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0014 + J 0.0031 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.555 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.555 KA
C-PRKW JUNC-PRKW LX          PRKW JUNC          40.555 KA    ANG: -65.08

B-PS3-USB              3P Duty: 16.289 KA AT -74.18 DEG ( 5.87 MVA) X/R: 3.53
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0020 + J 0.0071 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 16.289 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 16.744 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 16.289 KA
TX-PS3-UTIL              TX-PS3-UTIL P          16.289 KA    ANG: 105.82
  
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T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-SBA-USB          3P Duty: 30.433 KA AT -77.34 DEG ( 10.96 MVA) X/R: 4.45
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0009 + J 0.0039 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 30.433 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 30.433 KA
TX-SBA-UTIL          TX-SBA-UTIL P          30.433 KA    ANG: 102.66

B-SBH DISC A-USB  3P Duty: 9.363 KA AT -67.21 DEG ( 3.89 MVA) X/R: 2.38
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0057 + J 0.0136 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 9.363 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 9.363 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 9.363 KA
C-SBH JUNC-SBH A          B-SBH JUNC          9.363 KA    ANG: 112.79

B-SBH DISC B-USB  3P Duty: 9.363 KA AT -67.21 DEG ( 3.89 MVA) X/R: 2.38
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0057 + J 0.0136 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 9.363 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 9.363 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 9.363 KA
C-SBH JUNC-SBH B          B-SBH JUNC          9.363 KA    ANG: -67.21

B-SBH JUNC        3P Duty: 9.626 KA AT -68.52 DEG ( 4.00 MVA) X/R: 2.54
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0053 + J 0.0134 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 9.626 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 9.626 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 9.626 KA
TX-SBH-UTIL          TX-SBH-UTIL S          9.626 KA    ANG: 111.48

B-SEC NORTH ECB-USB 3P Duty: 40.607 KA AT -77.50 DEG ( 16.88 MVA) X/R: 4.51
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0007 + J 0.0033 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.607 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.607 KA
TX-SEC NORTH-UTIL-B          TX-SEC NORTH-UTIL-B P          40.607 KA    ANG: -257.50

B-SEC NORTH PNL-USB 3P Duty: 40.607 KA AT -77.50 DEG ( 16.88 MVA) X/R: 4.51
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0007 + J 0.0033 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.607 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.607 KA
TX-SEC NORTH-UTIL-A          TX-SEC NORTH-UTIL-A P          40.607 KA    ANG: -257.50

B-SEC SOUTH DISC 1A-USB 3P Duty: 36.472 KA AT -72.82 DEG ( 15.16 MVA) X/R: 3.23
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0011 + J 0.0036 OHMS
  
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THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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LOW VOLTAGE POWER CIRCUIT BREAKER 36.472 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.472 KA
C-SEC JUNC-SEC 1A B-SEC SOUTH-A JUNC 36.472 KA ANG: 107.18

B-SEC SOUTH DISC 2A-USB 3P Duty: 36.064 KA AT -71.46 DEG ( 14.99 MVA) X/R: 2.98
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 36.064 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.064 KA
C-SEC JUNC-SEC 2A B-SEC SOUTH-B JUNC 36.064 KA ANG: 108.54

B-SEC SOUTH DISC 2B-USB 3P Duty: 36.064 KA AT -71.46 DEG ( 14.99 MVA) X/R: 2.98
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 36.064 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.064 KA
C-SEC JUNC-SEC 2B B-SEC SOUTH-B JUNC 36.064 KA ANG: -71.46

B-SEC SOUTH PNL 1B-USB 3P Duty: 36.064 KA AT -71.46 DEG ( 14.99 MVA) X/R: 2.98
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 36.064 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.064 KA
C-SEC JUNC-SEC 1B B-SEC SOUTH-A JUNC 36.064 KA ANG: -71.46

B-SEC SOUTH PNL 1C-USB 3P Duty: 36.064 KA AT -71.46 DEG ( 14.99 MVA) X/R: 2.98
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 36.064 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.064 KA
C-SEC JUNC-SEC 1C B-SEC SOUTH-B JUNC 36.064 KA ANG: -71.46

B-SEC SOUTH PNL 1D-USB 3P Duty: 36.064 KA AT -71.46 DEG ( 14.99 MVA) X/R: 2.98
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0012 + J 0.0036 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 36.064 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 36.064 KA
C-SEC JUNC-SEC 1D B-SEC SOUTH-B JUNC 36.064 KA ANG: -71.46

B-SEH-USB 3P Duty: 33.251 KA AT -74.12 DEG ( 11.98 MVA) X/R: 3.51
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0010 + J 0.0035 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 33.251 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 33.251 KA
TX-SEH-UTIL TX-SEH-UTIL P 33.251 KA ANG: 105.88

B-SH-USB 3P Duty: 52.211 KA AT -76.53 DEG ( 18.81 MVA) X/R: 4.18
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0005 + J 0.0022 OHMS
  
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THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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LOW VOLTAGE POWER CIRCUIT BREAKER 52.211 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 52.211 KA
TX-SH-UTIL TX-SH-UTIL P 52.211 KA ANG: -256.53

B-STFR-USB 3P Duty: 52.158 KA AT -76.18 DEG ( 21.68 MVA) X/R: 4.07
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0006 + J 0.0026 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 52.158 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 52.158 KA
TX-STFR-UTIL TX-STFR-UTIL P 52.158 KA ANG: -256.18

B-STHL L1-USB 3P Duty: 18.617 KA AT -68.61 DEG ( 7.74 MVA) X/R: 2.55
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0027 + J 0.0069 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 18.617 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 18.617 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 18.617 KA
C-STHL JUNC-STHL L1 B-STHL JUNC 18.617 KA ANG: -68.61

B-STHL L2-USB 3P Duty: 18.452 KA AT -68.18 DEG ( 7.67 MVA) X/R: 2.50
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0028 + J 0.0070 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 18.452 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 18.452 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 18.452 KA
C-STHL JUNC-STHL L2 B-STHL JUNC 18.452 KA ANG: -68.18

B-STHL L3-USB 3P Duty: 18.288 KA AT -67.76 DEG ( 7.60 MVA) X/R: 2.45
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0029 + J 0.0070 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 18.288 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 18.288 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 18.288 KA
C-STHL JUNC-STHL L3 B-STHL JUNC 18.288 KA ANG: -67.76

B-STHL L4-USB 3P Duty: 18.126 KA AT -67.35 DEG ( 7.53 MVA) X/R: 2.40
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0029 + J 0.0071 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 18.126 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 18.126 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 18.126 KA
C-STHL JUNC-STHL L4 B-STHL JUNC 18.126 KA ANG: -67.35

B-STHL L5-USB 3P Duty: 17.966 KA AT -66.94 DEG ( 7.47 MVA) X/R: 2.35
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0030 + J 0.0071 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 17.966 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 17.966 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 17.966 KA
C-STHL JUNC-STHL L5 B-STHL JUNC 17.966 KA ANG: -66.94
  
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THREE PHASE FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-STHL X-USB          3P Duty: 17.809 KA AT -66.54 DEG ( 7.40 MVA) X/R: 2.30
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0031 + J 0.0071 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 17.809 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 17.809 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 17.809 KA
C-STHL JUNC-STHL X      B-STHL JUNC          17.809 KA      ANG: -66.54

B-UCB-USB            3P Duty: 31.924 KA AT -77.85 DEG ( 11.50 MVA) X/R: 4.64
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0008 + J 0.0037 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 31.924 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 31.924 KA
TX-UCB-UTIL          TX-UCB-UTIL P          31.924 KA      ANG: -257.85

B-UHP-USB            3P Duty: 15.554 KA AT -75.44 DEG ( 6.47 MVA) X/R: 3.85
VOLTAGE: 240. EQUIV. IMPEDANCE= 0.0022 + J 0.0086 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 15.554 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 16.345 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 15.554 KA
TX-UHP-UTIL          TX-UHP-UTIL P          15.554 KA      ANG: -255.44

B-UP-A-USB           3P Duty: 37.078 KA AT -78.06 DEG ( 30.83 MVA) X/R: 4.73
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0015 + J 0.0073 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 37.078 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 37.078 KA
TX-UP-UTIL-A          TX-UP-UTIL-A P          37.078 KA      ANG: 101.94

B-UP-B-USB           3P Duty: 57.220 KA AT -76.47 DEG ( 20.61 MVA) X/R: 4.15
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0005 + J 0.0020 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 57.220 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 57.220 KA
TX-UP UTIL-B          TX-UP UTIL-B P          57.220 KA      ANG: -256.47

B-URBN FP DISC-USB   3P Duty: 40.741 KA AT -75.33 DEG ( 33.87 MVA) X/R: 3.82
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0017 + J 0.0066 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 40.741 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.741 KA
TX-URBN-UTIL-B          TX-URBN-UTIL-B P          40.741 KA      ANG: 104.67

B-URBN SWBD-USB      3P Duty: 40.741 KA AT -75.33 DEG ( 33.87 MVA) X/R: 3.82
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0017 + J 0.0066 OHMS
  
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Feb 21, 2013 17:45:50 THREE PHASE LOW VOLTAGE DUTY PAGE 12
PSU - Non-West Campus Loop
Portland, OR
ESE0008355 / TQSISE0008355.1

T H R E E P H A S E F A U L T R E P O R T
(FOR APPLICATION OF LOW VOLTAGE BREAKERS)
PRE FAULT VOLTAGE: 1.0000
MODEL TRANSFORMER TAPS: NO

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LOW VOLTAGE POWER CIRCUIT BREAKER 40.741 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.741 KA
TX-URBN-UTIL-A TX-URBN-UTIL-A P 40.741 KA ANG: 104.67

B-EB-FP DISC-USB 3P Duty: 1.896 KA AT -71.05 DEG ( 1.58 MVA) X/R: 2.92
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0475 + J 0.1383 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 1.896 KA
MOLDED CASE CIRCUIT BREAKER < 10KA 2.186 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 1.896 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 1.896 KA
C-EB-TX-FP-FP DISC TX-EB-FIRE PUMP S 1.896 KA ANG: -71.05
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UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-AB ANNEX DISC-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	27.199 26.736 23.555 27.116 (4. Z1= 4. Z2= Z0=	10.2052 10.2052 10.7367 26.287 GND RETURN KA)	32.108 31.376	29.706
B-AB DISC-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	42.535 41.429 36.836 42.319 (4. Z1= 4. Z2= Z0=	6.5258 6.5258 7.0497 40.377 GND RETURN KA)	50.950 49.180	46.841
B-AB PNLBRD-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	42.535 41.429 36.836 42.319 (4. Z1= 4. Z2= Z0=	6.5258 6.5258 7.0497 40.377 GND RETURN KA)	50.950 49.180	46.841
B-ARC-A-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	14.551 14.259 12.601 14.544 (5. Z1= 5. Z2= Z0=	8.2665 8.2665 8.7758 13.978 GND RETURN KA)	18.324 17.720	16.494
B-ARC-B-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	21.867 21.574 18.937 21.848 (4. Z1= 4. Z2= Z0=	12.6938 12.6938 13.2129 21.287 GND RETURN KA)	26.254 25.725	24.112
B-BHB MSB-A-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	18.195 17.744 15.757 18.152 (5. Z1= 5. Z2= Z0=	6.6107 6.6107 7.1172 17.313 GND RETURN KA)	23.160 22.264	20.756
B-BHB MSB-B-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	27.648 27.192 23.944 27.590 (5. Z1= 4. Z2= Z0=	10.0394 10.0394 10.5468 26.748 GND RETURN KA)	34.017 33.193	30.919
B-BHB MSB-C-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	27.648 27.192 23.944 27.590 (5. Z1= 4. Z2= Z0=	10.0394 10.0394 10.5468 26.748 GND RETURN KA)	34.017 33.193	30.919

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-BLKS K-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	31.323 0.000 27.127 27.127 (1. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	7.6800 7.6800 INFINITE	31.650 0.000	31.487
B-BLKS L1-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	37.681 0.000 32.633 32.633 (3. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	6.3841 6.3841 INFINITE	40.627 0.000	39.168
B-BLKS L2-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	37.681 0.000 32.633 32.633 (3. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	6.3841 6.3841 INFINITE	40.627 0.000	39.168
B-BLKS L3-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	37.681 0.000 32.633 32.633 (3. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	6.3841 6.3841 INFINITE	40.627 0.000	39.168
B-BLKS L4-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	37.681 0.000 32.633 32.633 (3. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	6.3841 6.3841 INFINITE	40.627 0.000	39.168
B-BLKS L5-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	37.681 0.000 32.633 32.633 (3. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	6.3841 6.3841 INFINITE	40.627 0.000	39.168
B-BLKS X-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	27.943 0.000 24.199 24.199 (1. Z1= 1. Z2= Z0= INFINITE 0.000 GND RETURN KA)	8.6091 8.6091 INFINITE	27.991 0.000	27.967
B-EB-52-U1	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	5.907 5.659 5.115 5.889 (5. Z1= 5. Z2= Z0= INFINITE 5.429 GND RETURN KA)	0.7838 0.7838 0.8878	7.445 7.116	6.699

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-EB-52-U2	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	5.920 5.682 5.127 5.909 (5. Z1= 5. Z2= Z0= 5.460 GND RETURN KA)	0.7821 0.7821 0.8814	7.459 7.142	6.713
B-EB-52-U3	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	5.914 5.676 5.122 5.902 (5. Z1= 5. Z2= Z0= 5.454 GND RETURN KA)	0.7828 0.7828 0.8824	7.454 7.138	6.708
B-EB-USB-1	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	26.415 26.006 22.876 26.549 (6. Z1= 6. Z2= Z0= 25.604 GND RETURN KA)	4.5535 4.5535 4.7715	34.652 33.599	30.682
B-EB-USB-2	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	26.440 26.233 22.898 26.471 (6. Z1= 6. Z2= Z0= 26.027 GND RETURN KA)	4.5491 4.5491 4.6577	34.742 34.378	30.742
B-EB-USB-3	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	36.465 36.180 31.580 36.543 (6. Z1= 5. Z2= Z0= 35.898 GND RETURN KA)	7.6119 7.6119 7.7930	46.742 46.099	41.772
B-EB-USB-5	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	25.794 25.579 22.338 25.823 (6. Z1= 6. Z2= Z0= 25.366 GND RETURN KA)	4.6632 4.6632 4.7813	33.781 33.394	29.930
B-EB-USB-6	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	26.407 25.995 22.869 26.541 (6. Z1= 6. Z2= Z0= 25.589 GND RETURN KA)	4.5549 4.5549 4.7747	34.618 33.560	30.660
B-EB-USB-7	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	26.432 26.221 22.891 26.463 (6. Z1= 6. Z2= Z0= 26.013 GND RETURN KA)	4.5505 4.5505 4.6609	34.708 34.336	30.720

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-EH A-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	22.718 0.000 19.674 19.674 (2. Z1= 1. Z2= Z0=	10.5892 10.5892 INFINITE 0.000 GND RETURN KA)	24.186 0.000	23.458
B-EH B-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	22.718 0.000 19.674 19.674 (2. Z1= 1. Z2= Z0=	10.5892 10.5892 INFINITE 0.000 GND RETURN KA)	24.186 0.000	23.458
B-EH C-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	22.718 0.000 19.674 19.674 (2. Z1= 1. Z2= Z0=	10.5892 10.5892 INFINITE 0.000 GND RETURN KA)	24.186 0.000	23.458
B-EH E DISC-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	22.718 0.000 19.674 19.674 (2. Z1= 1. Z2= Z0=	10.5892 10.5892 INFINITE 0.000 GND RETURN KA)	24.186 0.000	23.458
B-HGDC-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	44.761 44.481 38.765 45.141 (4. Z1= 4. Z2= Z0=	5.3743 5.3743 5.4788 44.197 GND RETURN KA)	54.119 53.035	49.556
B-HH 1-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	50.812 0.000 44.004 44.004 (4. Z1= 1. Z2= Z0=	4.7344 4.7344 INFINITE 0.000 GND RETURN KA)	59.319 0.000	55.150
B-HH 2-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	45.858 0.000 39.714 39.714 (2. Z1= 1. Z2= Z0=	5.2458 5.2458 INFINITE 0.000 GND RETURN KA)	48.492 0.000	47.185
B-HOFF-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	33.251 32.921 28.796 33.523 (4. Z1= 3. Z2= Z0=	8.3477 8.3477 8.6050 32.589 GND RETURN KA)	38.413 37.547	35.880

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-HSB-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	48.870 0.000 42.323 42.323 (4. Z1= 1. Z2= Z0=	4.9225 4.9225 INFINITE 0.000 GND RETURN KA)	56.423 0.000	52.717
B-JCB-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	33.473 33.235 28.988 33.730 (4. Z1= 4. Z2= Z0=	8.2924 8.2924 8.4748 32.995 GND RETURN KA)	40.861 40.005	37.264
B-KHSE-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	30.433 29.853 26.356 30.424 (4. Z1= 4. Z2= Z0=	9.1207 9.1207 9.6560 29.290 GND RETURN KA)	37.119 35.994	33.863
B-KNGA-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	48.870 0.000 42.323 42.323 (4. Z1= 1. Z2= Z0=	4.9225 4.9225 INFINITE 0.000 GND RETURN KA)	56.423 0.000	52.717
B-MCB BSMT-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	7.999 9.224 6.928 10.178 (4. Z1= 3. Z2= Z0=	15.0362 15.0362 10.9149 10.376 GND RETURN KA)	9.572 10.058	8.804
B-MCB PNTHS-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	32.032 28.222 27.740 33.004 (5. Z1= 3. Z2= Z0=	3.7551 3.7551 5.4400 24.903 GND RETURN KA)	39.632 31.061	35.938
B-MONT-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	41.312 0.000 35.777 35.777 (3. Z1= 1. Z2= Z0=	5.8230 5.8230 INFINITE 0.000 GND RETURN KA)	46.967 0.000	44.186
B-NASC-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	15.562 15.231 13.477 15.451 (3. Z1= 3. Z2= Z0=	17.8360 17.8360 19.0002 14.914 GND RETURN KA)	17.833 17.400	16.718

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-OND 15 FLR-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	21.349 0.000 18.488 18.488 (4.	Z1= 11.2683 Z2= 11.2683 Z0= INFINITE 0.000 GND RETURN KA)	24.966 0.000	23.194
B-OND ANNEX SWBD-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	38.166 39.756 33.053 38.987 (5.	Z1= 7.2727 Z2= 7.2727 Z0= 6.4000 41.485 GND RETURN KA)	46.958 48.967	42.682
B-OND MAIN SWBD-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	15.962 16.600 13.824 16.311 (4.	Z1= 7.5355 Z2= 7.5355 Z0= 6.6665 17.291 GND RETURN KA)	19.181 19.939	17.610
B-PRKW L1-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2.	Z1= 5.9318 Z2= 5.9318 Z0= INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629
B-PRKW L2-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2.	Z1= 5.9318 Z2= 5.9318 Z0= INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629
B-PRKW L3-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2.	Z1= 5.9318 Z2= 5.9318 Z0= INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629
B-PRKW L4-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2.	Z1= 5.9318 Z2= 5.9318 Z0= INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629
B-PRKW L5-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2.	Z1= 5.9318 Z2= 5.9318 Z0= INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-PRKW X-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.555 0.000 35.121 35.121 (2. Z1= 1. Z2= Z0=	5.9318 5.9318 INFINITE 0.000 GND RETURN KA)	42.689 0.000	41.629
B-PS3-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	16.289 16.255 14.106 16.329 (4. Z1= 3. Z2= Z0=	17.0409 17.0409 17.1464 16.222 GND RETURN KA)	18.836 18.733	17.586
B-SBA-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	30.433 29.853 26.356 30.424 (4. Z1= 4. Z2= Z0=	9.1207 9.1207 9.6560 29.290 GND RETURN KA)	37.119 35.994	33.863
B-SBH DISC A-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	9.363 0.000 8.109 8.109 (2. Z1= 1. Z2= Z0=	25.6916 25.6916 INFINITE 0.000 GND RETURN KA)	10.010 0.000	9.689
B-SBH DISC B-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	9.363 0.000 8.109 8.109 (2. Z1= 1. Z2= Z0=	25.6916 25.6916 INFINITE 0.000 GND RETURN KA)	10.010 0.000	9.689
B-SBH JUNC	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	9.626 0.000 8.337 8.337 (3. Z1= 1. Z2= Z0=	24.9904 24.9904 INFINITE 0.000 GND RETURN KA)	10.406 0.000	10.020
B-SEC NORTH ECB-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.607 0.000 35.167 35.167 (5. Z1= 1. Z2= Z0=	5.9241 5.9241 INFINITE 0.000 GND RETURN KA)	49.681 0.000	45.264
B-SEC NORTH PNL-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	40.607 0.000 35.167 35.167 (5. Z1= 1. Z2= Z0=	5.9241 5.9241 INFINITE 0.000 GND RETURN KA)	49.681 0.000	45.264

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION	FAULT	KA	X/R	EQUIVALENT (PU)	ASYM. KA AT 0.5 CYCLES	
VOLTAGE	DUTIES	(RMS)		FAULT IMPEDANCE	* MAX. RMS	AVG. RMS *
B-SEC SOUTH DISC 1A-USB	3P Duty:	36.472	3. Z1=	6.5959	41.369	38.960
	SLG DUTY:	0.000	1. Z2=	6.5959	0.000	
240. VOLTS	LN/LN:	31.585	Z0=	INFINITE		
	LN/LN/GND:	31.585 (0.000	GND RETURN KA)		
B-SEC SOUTH DISC 2A-USB	3P Duty:	36.064	3. Z1=	6.6704	40.213	38.167
	SLG DUTY:	0.000	1. Z2=	6.6704	0.000	
240. VOLTS	LN/LN:	31.232	Z0=	INFINITE		
	LN/LN/GND:	31.232 (0.000	GND RETURN KA)		
B-SEC SOUTH DISC 2B-USB	3P Duty:	36.064	3. Z1=	6.6704	40.213	38.167
	SLG DUTY:	0.000	1. Z2=	6.6704	0.000	
240. VOLTS	LN/LN:	31.232	Z0=	INFINITE		
	LN/LN/GND:	31.232 (0.000	GND RETURN KA)		
B-SEC SOUTH PNL 1B-USB	3P Duty:	36.064	3. Z1=	6.6704	40.213	38.167
	SLG DUTY:	0.000	1. Z2=	6.6704	0.000	
240. VOLTS	LN/LN:	31.232	Z0=	INFINITE		
	LN/LN/GND:	31.232 (0.000	GND RETURN KA)		
B-SEC SOUTH PNL 1C-USB	3P Duty:	36.064	3. Z1=	6.6704	40.213	38.167
	SLG DUTY:	0.000	1. Z2=	6.6704	0.000	
240. VOLTS	LN/LN:	31.232	Z0=	INFINITE		
	LN/LN/GND:	31.232 (0.000	GND RETURN KA)		
B-SEC SOUTH PNL 1D-USB	3P Duty:	36.064	3. Z1=	6.6704	40.213	38.167
	SLG DUTY:	0.000	1. Z2=	6.6704	0.000	
240. VOLTS	LN/LN:	31.232	Z0=	INFINITE		
	LN/LN/GND:	31.232 (0.000	GND RETURN KA)		
B-SEH-USB	3P Duty:	33.251	4. Z1=	8.3477	38.413	35.880
	SLG DUTY:	32.921	3. Z2=	8.3477	37.547	
208. VOLTS	LN/LN:	28.796	Z0=	8.6050		
	LN/LN/GND:	33.523 (32.589	GND RETURN KA)		
B-SH-USB	3P Duty:	52.211	4. Z1=	5.3164	62.741	57.602
	SLG DUTY:	50.413	4. Z2=	5.3164	59.577	
208. VOLTS	LN/LN:	45.216	Z0=	5.8893		
	LN/LN/GND:	52.059 (48.723	GND RETURN KA)		

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-STFR-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	52.158 0.000 45.170 45.170 (4.	Z1= 4.6122 Z2= 4.6122 Z0= INFINITE 0.000 GND RETURN KA)	62.298 0.000	57.345
B-STHL L1-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	18.617 0.000 16.123 16.123 (3.	Z1= 12.9216 Z2= 12.9216 Z0= INFINITE 0.000 GND RETURN KA)	20.144 0.000	19.388
B-STHL L2-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	18.452 0.000 15.980 15.980 (2.	Z1= 13.0375 Z2= 13.0375 Z0= INFINITE 0.000 GND RETURN KA)	19.887 0.000	19.176
B-STHL L3-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	18.288 0.000 15.838 15.838 (2.	Z1= 13.1542 Z2= 13.1542 Z0= INFINITE 0.000 GND RETURN KA)	19.639 0.000	18.970
B-STHL L4-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	18.126 0.000 15.698 15.698 (2.	Z1= 13.2715 Z2= 13.2715 Z0= INFINITE 0.000 GND RETURN KA)	19.398 0.000	18.768
B-STHL L5-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	17.966 0.000 15.559 15.559 (2.	Z1= 13.3896 Z2= 13.3896 Z0= INFINITE 0.000 GND RETURN KA)	19.165 0.000	18.571
B-STHL X-USB	3P Duty: SLG DUTY: 240. VOLTS LN/LN: LN/LN/GND:	17.809 0.000 15.423 15.423 (2.	Z1= 13.5083 Z2= 13.5083 Z0= INFINITE 0.000 GND RETURN KA)	18.938 0.000	18.378
B-UCB-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	31.924 31.306 27.647 31.900 (5. 4.	Z1= 8.6949 Z2= 8.6949 Z0= 9.2126 30.708 GND RETURN KA)	39.317 38.113	35.721

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION	FAULT	KA	X/R	EQUIVALENT (PU)	ASYM. KA AT 0.5 CYCLES	
VOLTAGE	DUTIES	(RMS)		FAULT IMPEDANCE	* MAX. RMS	AVG. RMS *
B-UHP-USB	3P Duty:	15.554	4.	Z1= 15.4667	18.344	16.979
	SLG DUTY:	0.000	1.	Z2= 15.4667	0.000	
240. VOLTS	LN/LN:	13.470		Z0= INFINITE		
	LN/LN/GND:	13.470 (0.000	GND RETURN KA)		
B-UP-A-USB	3P Duty:	37.078	5.	Z1= 3.2440	45.854	41.589
	SLG DUTY:	34.143	4.	Z2= 3.2440	41.044	
480. VOLTS	LN/LN:	32.111		Z0= 4.0864		
	LN/LN/GND:	36.476 (31.621	GND RETURN KA)		
B-UP-B-USB	3P Duty:	57.220	4.	Z1= 4.8510	68.683	63.088
	SLG DUTY:	54.081	4.	Z2= 4.8510	63.856	
208. VOLTS	LN/LN:	49.554		Z0= 5.6994		
	LN/LN/GND:	56.506 (51.256	GND RETURN KA)		
B-URBN FP DISC-USB	3P Duty:	40.741	4.	Z1= 2.9523	47.967	44.431
	SLG DUTY:	38.206	3.	Z2= 2.9523	43.595	
480. VOLTS	LN/LN:	35.283		Z0= 3.5504		
	LN/LN/GND:	40.669 (35.929	GND RETURN KA)		
B-URBN SWBD-USB	3P Duty:	40.741	4.	Z1= 2.9523	47.967	44.431
	SLG DUTY:	38.206	3.	Z2= 2.9523	43.595	
480. VOLTS	LN/LN:	35.283		Z0= 3.5504		
	LN/LN/GND:	40.669 (35.929	GND RETURN KA)		
B-EB-FP DISC-USB	3P Duty:	1.896	3.	Z1= 63.4516	2.105	2.002
	SLG DUTY:	1.894	3.	Z2= 63.4516	2.097	
480. VOLTS	LN/LN:	1.642		Z0= 63.6019		
	LN/LN/GND:	1.902 (1.893	GND RETURN KA)		

FAULT STUDY SUMMARY
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

BUS RECORD NO NAME	VOLTAGE AVAILABLE			FAULT DUTIES (KA)	
	L-L	3 PHASE	X/R	LINE/GRND	X/R
B-AB ANNEX DISC-USB	208.	27.199	3.86	26.736	3.77
B-AB DISC-USB	208.	42.535	4.12	41.429	3.96
B-AB PNLBRD-USB	208.	42.535	4.12	41.429	3.96
B-ARC-A-USB	480.	14.551	5.12	14.259	4.83
B-ARC-B-USB	208.	21.867	4.16	21.574	4.04
B-BHB MSB-A-USB	480.	18.195	5.37	17.744	5.04
B-BHB MSB-B-USB	208.	27.648	4.62	27.192	4.47
B-BHB MSB-C-USB	208.	27.648	4.62	27.192	4.47
B-BLKS K-USB	240.	31.323	1.38	0.000	1.00
B-BLKS L1-USB	240.	37.681	2.50	0.000	1.00
B-BLKS L2-USB	240.	37.681	2.50	0.000	1.00
B-BLKS L3-USB	240.	37.681	2.50	0.000	1.00
B-BLKS L4-USB	240.	37.681	2.50	0.000	1.00
B-BLKS L5-USB	240.	37.681	2.50	0.000	1.00
B-BLKS X-USB	240.	27.943	0.99	0.000	1.00
B-EB-52-U1	12470.	5.907	5.14	5.659	5.09
B-EB-52-U2	12470.	5.920	5.13	5.682	5.07
B-EB-52-U3	12470.	5.914	5.14	5.676	5.09
B-EB-USB-1	480.	26.415	6.16	26.006	5.74
B-EB-USB-2	480.	26.440	6.20	26.233	6.13
B-EB-USB-3	208.	36.465	5.54	36.180	5.39
B-EB-USB-5	480.	25.794	6.11	25.579	6.02
B-EB-USB-6	480.	26.407	6.14	25.995	5.72
B-EB-USB-7	480.	26.432	6.19	26.221	6.11
B-EH A-USB	240.	22.718	2.32	0.000	1.00
B-EH B-USB	240.	22.718	2.32	0.000	1.00
B-EH C-USB	240.	22.718	2.32	0.000	1.00
B-EH E DISC-USB	240.	22.718	2.32	0.000	1.00
B-HGDC-USB	240.	44.761	4.29	44.481	4.04
B-HH 1-USB	240.	50.812	3.68	0.000	1.00
B-HH 2-USB	240.	45.858	2.22	0.000	1.00
B-HOFF-USB	208.	33.251	3.51	32.921	3.32
B-HSB-USB	240.	48.870	3.50	0.000	1.00
B-JCB-USB	208.	33.473	4.47	33.235	4.21
B-KHSE-USB	208.	30.433	4.45	29.853	4.24
B-KNGA-USB	240.	48.870	3.50	0.000	1.00
B-MCB BSMT-USB	480.	7.999	4.10	9.224	2.66
B-MCB PNTHS-USB	480.	32.032	4.74	28.222	2.80
B-MONT-USB	240.	41.312	3.27	0.000	1.00
B-NASC-USB	208.	15.562	3.39	15.231	3.34
B-OND 15 FLR-USB	240.	21.349	3.71	0.000	1.00
B-OND ANNEX SWBD-USB	208.	38.166	4.62	39.756	4.64
B-OND MAIN SWBD-USB	480.	15.962	4.17	16.600	4.17
B-PRKW L1-USB	240.	40.555	2.15	0.000	1.00

Feb 21, 2013 17:45:50
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UNBALANCED LOW VOLTAGE DUTY PAGE 12

FAULT STUDY SUMMARY
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

BUS RECORD NO NAME	VOLTAGE L-L	A V A I L A B L E 3 PHASE	F A U L T X/R	D U T I E S (KA) LINE/GRND	X/R
B-PRKW L2-USB	240.	40.555	2.15	0.000	1.00
B-PRKW L3-USB	240.	40.555	2.15	0.000	1.00
B-PRKW L4-USB	240.	40.555	2.15	0.000	1.00
B-PRKW L5-USB	240.	40.555	2.15	0.000	1.00
B-PRKW X-USB	240.	40.555	2.15	0.000	1.00
B-PS3-USB	208.	16.289	3.53	16.255	3.48
B-SBA-USB	208.	30.433	4.45	29.853	4.24
B-SBH DISC A-USB	240.	9.363	2.38	0.000	1.00
B-SBH DISC B-USB	240.	9.363	2.38	0.000	1.00
B-SBH JUNC	240.	9.626	2.54	0.000	1.00
B-SEC NORTH ECB-USB	240.	40.607	4.51	0.000	1.00
B-SEC NORTH PNL-USB	240.	40.607	4.51	0.000	1.00
B-SEC SOUTH DISC 1A-USB	240.	36.472	3.23	0.000	1.00
B-SEC SOUTH DISC 2A-USB	240.	36.064	2.98	0.000	1.00
B-SEC SOUTH DISC 2B-USB	240.	36.064	2.98	0.000	1.00
B-SEC SOUTH PNL 1B-USB	240.	36.064	2.98	0.000	1.00
B-SEC SOUTH PNL 1C-USB	240.	36.064	2.98	0.000	1.00
B-SEC SOUTH PNL 1D-USB	240.	36.064	2.98	0.000	1.00
B-SEH-USB	208.	33.251	3.51	32.921	3.32
B-SH-USB	208.	52.211	4.18	50.413	3.88
B-STFR-USB	240.	52.158	4.07	0.000	1.00
B-STHL L1-USB	240.	18.617	2.55	0.000	1.00
B-STHL L2-USB	240.	18.452	2.50	0.000	1.00
B-STHL L3-USB	240.	18.288	2.45	0.000	1.00
B-STHL L4-USB	240.	18.126	2.40	0.000	1.00
B-STHL L5-USB	240.	17.966	2.35	0.000	1.00
B-STHL X-USB	240.	17.809	2.30	0.000	1.00
B-UCB-USB	208.	31.924	4.64	31.306	4.42
B-UHP-USB	240.	15.554	3.85	0.000	1.00
B-UP-A-USB	480.	37.078	4.73	34.143	4.18
B-UP-B-USB	208.	57.220	4.15	54.081	3.87
B-URBN FP DISC-USB	480.	40.741	3.82	38.206	3.32
B-URBN SWBD-USB	480.	40.741	3.82	38.206	3.32
B-EB-FP DISC-USB	480.	1.896	2.92	1.894	2.88

148 FAULTED BUSES, 150 BRANCHES, 44 CONTRIBUTIONS
 UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

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THREE PHASE MOMENTARY DUTY PAGE 1

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-AB ANNEX DISC-USB      VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-AB DISC-USB           VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-AB PNLBRD-USB         VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-ARC-A-USB             VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-ARC-B-USB            VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-A-USB         VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-B-USB         VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-C-USB         VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BLKS K-USB           VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L1-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L2-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L3-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L4-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L5-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS X-USB           VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )

B-EB-52-U1              E/Z:      5.907 KA AT -75.14 DEG ( 127.58 MVA) X/R:      5.14
                      SYM*1.6:    9.451 KA      MOMENTARY BASED ON X/R:    7.445 KA
                      SYM*2.7:   15.948 KA      CREST BASED ON X/R:   12.885 KA
                      VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3126 + J 1.1781 OHMS

B-EB-52-U2              E/Z:      5.920 KA AT -75.13 DEG ( 127.86 MVA) X/R:      5.13
                      SYM*1.6:    9.471 KA      MOMENTARY BASED ON X/R:    7.459 KA
                      SYM*2.7:   15.983 KA      CREST BASED ON X/R:   12.910 KA
                      VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3122 + J 1.1755 OHMS
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Feb 21, 2013 17:45:50
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THREE PHASE MOMENTARY DUTY PAGE 2

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

=====

CONTRIBUTIONS TO B-EB-52-U2

(CONTINUED)

B-EB-52-U3	E/Z:	5.914 KA AT -75.13 DEG (127.74 MVA)	X/R:	5.14
	SYM*1.6:	9.463 KA	MOMENTARY BASED ON X/R:	7.454 KA
	SYM*2.7:	15.969 KA	CREST BASED ON X/R:	12.901 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE=	0.3123 + J 1.1765 OHMS
B-EB-USB-1	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)	
B-EB-USB-2	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)	
B-EB-USB-3	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)	
B-EB-USB-5	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)	
B-EB-USB-6	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)	
B-EB-USB-7	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)	
B-EH A-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-EH B-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-EH C-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-EH E DISC-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-HGDC-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-HH 1-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-HH 2-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-HOFF-USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)	
B-HSB-USB	VOLTAGE:	240.	(SEE LOW VOLTAGE REPORT)	
B-JCB-USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)	

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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=====
B-KHSE-USB          VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-KNGA-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-MCB BSMT-USB      VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-MCB PNTHS-USB     VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-MONT-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-NASC-USB          VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-OND 15 FLR-USB    VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-OND ANNEX SWBD-USB VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-OND MAIN SWBD-USB VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-PRKW L1-USB       VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L2-USB       VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L3-USB       VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L4-USB       VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L5-USB       VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PRKW X-USB        VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-PS3-USB           VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-SBA-USB           VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-SBH DISC A-USB    VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SBH DISC B-USB    VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SBH JUNC          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SEC NORTH ECB-USB VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SEC NORTH PNL-USB VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
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Feb 21, 2013 17:45:50
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THREE PHASE MOMENTARY DUTY PAGE 4

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

```
=====
B-SEC SOUTH DISC 1A-USB      VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH DISC 2A-USB      VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH DISC 2B-USB      VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH PNL 1B-USB       VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH PNL 1C-USB       VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH PNL 1D-USB       VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEH-USB                     VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-SH-USB                       VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-STFR-USB                     VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL L1-USB                 VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL L2-USB                 VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL L3-USB                 VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL L4-USB                 VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL L5-USB                 VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-STHL X-USB                  VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-UCB-USB                     VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-UHP-USB                     VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-UP-A-USB                    VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
B-UP-B-USB                    VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-URBN FP DISC-USB           VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
B-URBN SWBD-USB              VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
B-EB-FP DISC-USB             VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
=====
```

Feb 21, 2013 17:45:50
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UNBALANCED MOMENTARY DUTY PAGE 1

UNBALANCED MOMENTARY DUTY REPORT

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

LOCATION	VOLTAGE	FAULT TYPE	E/Z KA	X/R	EQUIVALENT IMPEDANCE (PU)	MOMENTARY E/Z * 1.6 @ 0.5 CYCLE	FAULT DUTIES
B-EB-52-U1	12470.	3P Duty:	5.91	5.1	Z1= 0.7838	9.45	7.44
		SLG DUTY:	5.66	5.1	Z2= 0.7838	9.05	7.12
		VOLTS LN/LN:	5.12		Z0= 0.8878		
		LN/LN/GND:	5.89 (5.43	GND RETURN KA)		
B-EB-52-U2	12470.	3P Duty:	5.92	5.1	Z1= 0.7821	9.47	7.46
		SLG DUTY:	5.68	5.1	Z2= 0.7821	9.09	7.14
		VOLTS LN/LN:	5.13		Z0= 0.8814		
		LN/LN/GND:	5.91 (5.46	GND RETURN KA)		
B-EB-52-U3	12470.	3P Duty:	5.91	5.1	Z1= 0.7828	9.46	7.45
		SLG DUTY:	5.68	5.1	Z2= 0.7828	9.08	7.14
		VOLTS LN/LN:	5.12		Z0= 0.8824		
		LN/LN/GND:	5.90 (5.45	GND RETURN KA)		

Feb 21, 2013 17:45:50
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UNBALANCED MOMENTARY DUTY PAGE 2

M O M E N T A R Y D U T Y S U M M A R Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
MODEL TRANSFORMER TAPS: NO
SOLUTION METHOD : E/Z

```
=====
BUS RECORD          VOLTAGE    * 3 P H A S E *    * * * SLG * * *
NO NAME            L-L          KA      X/R          KA      X/R
=====
```

BUS RECORD	VOLTAGE	* 3	P H A S E *	* * *	SLG	* * *
NO NAME	L-L	KA	X/R	KA	X/R	
B-EB-52-U1	12470.	7.445	5.14	7.116	5.09	
B-EB-52-U2	12470.	7.459	5.13	7.142	5.07	
B-EB-52-U3	12470.	7.454	5.14	7.138	5.09	

54 FAULTED BUSES, 150 BRANCHES, 44 CONTRIBUTIONS
UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

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THREE PHASE INTERRUPTING DUTY PAGE 1

THREE PHASE INTERRUPTING DUTY REPORT

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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=====
B-AB ANNEX DISC-USB      VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-AB DISC-USB           VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-AB PNLBRD-USB        VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-ARC-A-USB            VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-ARC-B-USB            VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-A-USB        VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-B-USB        VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BHB MSB-C-USB        VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-BLKS K-USB           VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L1-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L2-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L3-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L4-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS L5-USB          VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-BLKS X-USB           VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-EB-52-U1              E/Z: 5.907 KA AT -75.14 DEG ( 127.58 MVA) X/R: 5.14
                        VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3126 + J 1.1781 OHMS
                        CONTRIBUTIONS: B-EB-52-U3 5.907 KA ANG: -75.14
  
```

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GENERATOR NAME -- AT BUS --          KA  VOLTS PU  LOCAL/REMOTE
EB-UTIL-B              4.976  0.00      R
G-EB GEN                0.952  0.45      L
TOTAL REMOTE:          4.976 KA  NACD RATIO: 0.8424

      SYM2  SYM3  SYM5  SYM8
MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 5.907 5.907 5.907 5.907

      TOT2  TOT3  TOT5  TOT8
MULT. FACT: 1.049 1.000 1.000 1.000
DUTY (KA) : 6.198 5.907 5.907 5.907
  
```

THREE PHASE INTERRUPTING DUTY REPORT

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

=====

B-EB-52-U2 E/Z: 5.920 KA AT -75.13 DEG (127.86 MVA) X/R: 5.13
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3122 + J 1.1755 OHMS
 C-UTIL-BK-EB-5 EB-UTIL-B BUS 4.988 KA ANG: -253.01
 C-EB-52-U3-52- B-EB-52-U3 0.953 KA ANG: -86.25

GENERATOR NAME	-- AT BUS --	KA	VOLTS PU	LOCAL/REMOTE
EB-UTIL-B		4.988	0.00	R
G-EB GEN		0.953	0.45	L
TOTAL REMOTE: 4.988 KA NACD RATIO: 0.8426				

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	5.920	5.920	5.920	5.920

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.049	1.000	1.000	1.000
DUTY (KA) :	6.210	5.920	5.920	5.920

B-EB-52-U3 E/Z: 5.914 KA AT -75.13 DEG (127.74 MVA) X/R: 5.14
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3123 + J 1.1765 OHMS
 C-EB-USB-8-52- USB-8 S 0.953 KA ANG: 93.74
 C-EB-52-U3-52- B-EB-52-U2 4.982 KA ANG: -253.02

GENERATOR NAME	-- AT BUS --	KA	VOLTS PU	LOCAL/REMOTE
EB-UTIL-B		4.982	0.00	R
G-EB GEN		0.953	0.45	L
TOTAL REMOTE: 4.982 KA NACD RATIO: 0.8424				

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	5.914	5.914	5.914	5.914

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.049	1.000	1.000	1.000
DUTY (KA) :	6.206	5.914	5.914	5.914

Feb 21, 2013 17:45:50
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THREE PHASE INTERRUPTING DUTY PAGE 3

THREE PHASE INTERRUPTING DUTY REPORT
PRE FAULT VOLTAGE: 1.0000
MODEL TRANSFORMER TAPS: NO
NACD OPTION: INTERPOLATED

B-EB-USB-1 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
B-EB-USB-2 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
B-EB-USB-3 VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
B-EB-USB-5 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
B-EB-USB-6 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
B-EB-USB-7 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
B-EH A-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-EH B-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-EH C-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-EH E DISC-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-HGDC-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-HH 1-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-HH 2-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-HOFF-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
B-HSB-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-JCB-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
B-KHSE-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
B-KNGA-USB VOLTAGE: 240. (SEE LOW VOLTAGE REPORT)
B-MCB BSMT-USB VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)

Feb 21, 2013 17:45:50
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THREE PHASE INTERRUPTING DUTY PAGE 4

THREE PHASE INTERRUPTING DUTY REPORT
PRE FAULT VOLTAGE: 1.0000
MODEL TRANSFORMER TAPS: NO

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=====
B-MCB PNTHS-USB      VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
B-MONT-USB           VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-NASC-USB           VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-OND 15 FLR-USB     VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-OND ANNEX SWBD-USB VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-OND MAIN SWBD-USB  VOLTAGE:  480. ( SEE LOW VOLTAGE REPORT )
B-PRKW L1-USB        VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L2-USB        VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L3-USB        VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L4-USB        VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PRKW L5-USB        VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PRKW X-USB         VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-PS3-USB            VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-SBA-USB            VOLTAGE:  208. ( SEE LOW VOLTAGE REPORT )
B-SBH DISC A-USB     VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SBH DISC B-USB     VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SBH JUNC           VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC NORTH ECB-USB  VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC NORTH PNL-USB  VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH DISC 1A-USB VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH DISC 2A-USB VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH DISC 2B-USB VOLTAGE:  240. ( SEE LOW VOLTAGE REPORT )
=====
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Feb 21, 2013 17:45:50
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THREE PHASE INTERRUPTING DUTY PAGE 5

THREE PHASE INTERRUPTING DUTY REPORT
PRE FAULT VOLTAGE: 1.0000
MODEL TRANSFORMER TAPS: NO

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=====
B-SEC SOUTH PNL 1B-USB      VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH PNL 1C-USB      VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SEC SOUTH PNL 1D-USB      VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-SEH-USB                   VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-SH-USB                     VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-STFR-USB                   VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL L1-USB                VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL L2-USB                VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL L3-USB                VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL L4-USB                VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL L5-USB                VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-STHL X-USB                 VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-UCB-USB                    VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-UHP-USB                    VOLTAGE: 240. ( SEE LOW VOLTAGE REPORT )
B-UP-A-USB                   VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-UP-B-USB                   VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )
B-URBN FP DISC-USB          VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-URBN SWBD-USB             VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
B-EB-FP DISC-USB            VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )
=====
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UNBALANCED INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	AC/DC FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-EB-52-U1	3P Duty:	5.91	5.1	SYM2:	1.00	1.00	5.91 5.66
	VOLTS: 12470.0	SLG: 5.66	5.1	SYM3:	1.00	1.00	5.91 5.66
	NACD: 0.842	LN/LN: 5.12		SYM5:	1.00	1.00	5.91 5.66
		LN/LN/GND: 5.89		SYM8:	1.00	1.00	5.91 5.66
		GND RETURN: 5.43		TOT2:	1.05	1.05	6.20 5.93
		Z1 (PU):	0.78383	TOT3:	1.00	1.00	5.91 5.66
		Z2 (PU):	0.78383	TOT5:	1.00	1.00	5.91 5.66
		Z0 (PU):	0.88779	TOT8:	1.00	1.00	5.91 5.66
B-EB-52-U2	3P Duty:	5.92	5.1	SYM2:	1.00	1.00	5.92 5.68
	VOLTS: 12470.0	SLG: 5.68	5.1	SYM3:	1.00	1.00	5.92 5.68
	NACD: 0.843	LN/LN: 5.13		SYM5:	1.00	1.00	5.92 5.68
		LN/LN/GND: 5.91		SYM8:	1.00	1.00	5.92 5.68
		GND RETURN: 5.46		TOT2:	1.05	1.05	6.21 5.95
		Z1 (PU):	0.78213	TOT3:	1.00	1.00	5.92 5.68
		Z2 (PU):	0.78213	TOT5:	1.00	1.00	5.92 5.68
		Z0 (PU):	0.88141	TOT8:	1.00	1.00	5.92 5.68
B-EB-52-U3	3P Duty:	5.91	5.1	SYM2:	1.00	1.00	5.91 5.68
	VOLTS: 12470.0	SLG: 5.68	5.1	SYM3:	1.00	1.00	5.91 5.68
	NACD: 0.842	LN/LN: 5.12		SYM5:	1.00	1.00	5.91 5.68
		LN/LN/GND: 5.90		SYM8:	1.00	1.00	5.91 5.68
		GND RETURN: 5.45		TOT2:	1.05	1.05	6.21 5.95
		Z1 (PU):	0.78282	TOT3:	1.00	1.00	5.91 5.68
		Z2 (PU):	0.78282	TOT5:	1.00	1.00	5.91 5.68
		Z0 (PU):	0.88237	TOT8:	1.00	1.00	5.91 5.68

Feb 21, 2013 17:45:50
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I N T E R R U P T I N G D U T Y S U M M A R Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

```

=====
BUS RECORD          VOLTAGE NACD   * 3 P H A S E *   * * * S L G * * *
NO NAME            L-L    RATIO  E/Z KA    X/R    E/Z KA    X/R
=====
B-EB-52-U1         12470. 0.842   5.907    5.14   5.659    5.09
B-EB-52-U2         12470. 0.843   5.920    5.13   5.682    5.07
B-EB-52-U3         12470. 0.842   5.914    5.14   5.676    5.09
  
```

54 FAULTED BUSES, 150 BRANCHES, 44 CONTRIBUTIONS
 UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

C. APPENDIX C – UTILITY FAULT CURRENT INFORMATION

See attached spreadsheet with a summary of utility fault current and transformer information.

Building	Abbrev	Voltage		XFMR Winding		Transformer		Source Imp. (p.u., 100 MVA, 12.47 kVA base)				Three-Phase		Single-Line to Ground			
		Prim. (kV)	Sec. (V)	Prim.	Sec.	kVA	%Z	Positive		Zero		Calc. Fault Current (A)	X/R	Calc. Fault Current (A)	X/R		
Helen Gordon Child Development Center	HGDC	12.47/7.2	240/120	Wye-Gnd	Wye-Gnd	167	3.2	0.179163	+/	0.343599	0.418583	+/	0.390416	11948	1.918	10455.4	1.387
						167	2.5										
						167	2.5										
Parking Structure #3	PS3	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	150	2.5	0.167202	+/	0.341799	0.39704	+/	0.38495	12167.9	2.044	10726.4	1.461
University Honors Program	UHP	12.47/7.2	240/120	Open Wye	Open Delta	15	1.6	0.13151	+/	0.333374	0.338712	+/	0.376847	12919.2	2.535	11530.1	1.734
						75	3.4										
Blumel Hall	JCB	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	750	5.9	0.336332	+/	0.365078	0.699803	+/	0.46392	9327.2	1.085	7635.1	0.87
St. Helens Building	STHL	12.47/7.2	240/120	1 Phase	1 Phase	50	1.8	0.327908	+/	0.378712	0.636073	+/	0.456782	9242.3	1.155	7834.4	0.94
Stephen Erpler Hall	SEH	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	300	2.36	0.441798	+/	0.381284	0.88977	+/	0.511894	7933.7	0.863	6360.3	0.719
Hoffman Hall	HOFF	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	300	2.36	0.441798	+/	0.381284	0.88977	+/	0.511894	7933.7	0.863	6360.3	0.719
King Albert Building	KNGA	12.47/7.2	240/120	Open Wye	Open Delta	15	1.7	0.296333	+/	0.358905	0.634659	+/	0.452666	9947.6	1.211	8189.8	0.954
						100	1.35										
Strafford Building	STFR	12.47/7.2	240/120	Open Wye	Open Delta	167	2.1	0.226365	+/	0.37093	0.567392	+/	0.442698	10654.6	1.639	8885	1.161
						167	2.1										
Harder House	HH	12.47/7.2	240/120	Open Wye	Open Delta	167	2.1	0.226365	+/	0.37093	0.567392	+/	0.442698	10654.6	1.639	8885	1.161
						167	2.1										
Parkway Building	PRKW	12.47/7.2	240/120	Open Wye	Open Delta	167	2.1	0.226365	+/	0.37093	0.567392	+/	0.442698	10654.6	1.639	8885	1.161
						167	2.1										
Harrison Street Building	HSB	12.47/7.2	240/120	Open Wye	Open Delta	15	1.7	0.296333	+/	0.358905	0.634659	+/	0.452666	9947.6	1.211	8189.8	0.954
						100	1.35										
Montgomery Court	MONT	12.47/7.2	240/120	Open Wye	Open Delta	15	1.9	0.454403	+/	0.383213	0.912278	+/	0.516846	7789	0.843	6234.7	0.705
						100	1.6										
Simon Benson House	SBH	12.47/7.2	240/120	1 Phase	1 Phase	25	1.83	0.545849	+/	0.42212	0.9962	+/	0.55363	6709.8	0.773	5527.9	0.67
Blackstone	BLKS	12.47/7.2	240/120	Open Wye	Open Delta	15	1.9	0.454403	+/	0.383213	0.912278	+/	0.516846	7789	0.843	6234.7	0.705
						100	1.6										
Shattuck Hall	SH	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	2.2	0.321542	+/	0.866747	0.725719	+/	1.352211	5008.2	2.696	4114.7	2.254
East Hall	EH	12.47/7.2	240/120	Open Wye	Open Delta	100	2.4	0.321542	+/	0.866747	0.725719	+/	1.352211	5008.2	2.696	4114.7	2.254
						50	1.8										
University Center	UCB	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	3.9	0.205658	+/	0.871185	0.587199	+/	1.314205	5172.3	4.236	4319.6	3.061
Ondine Residence	OND	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	300	2	0.193825	+/	0.847133	0.495688	+/	1.29414	5327.7	4.371	4457.2	3.383
			240/120	1 Phase	167	5.2											
Ondine Annex	OND ANNEX	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	3.2	0.204179	+/	0.848741	0.514274	+/	1.298835	5303.7	4.157	4430.3	3.248
The Broadway	BHB-A	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	1000	5.73	0.222893	+/	0.854722	0.550222	+/	1.30488	5241.6	3.835	4375.3	3.026
	BHB-B	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	4.58	0.214275	+/	0.853436	0.534724	+/	1.300957	5261.7	3.983	4397.8	3.123
	BHB-C	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	4.58	0.214275	+/	0.853436	0.534724	+/	1.300957	5261.7	3.983	4397.8	3.123
Native American Student Community Center	NASC	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	150	2.5	0.571251	+/	1.052598	1.100444	+/	2.108991	3865.9	1.843	2909.5	1.879
Art Building	AB-A	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	100	2.3	0.21241	+/	0.832471	0.513695	+/	1.296005	5389	3.919	4471.7	3.155
						100	1.7										
	AB-B	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	100	2.3	0.21241	+/	0.832471	0.513695	+/	1.296005	5389	3.919	4471.7	3.155
						100	1.7										
AB-ANNEX	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	225	2.1	0.235497	+/	0.839867	0.558132	+/	1.303529	5308	3.566	4401.4	2.899	
Fourth Avenue Building	EB	12.47/7.2	N/A	N/A	N/A	N/A	N/A	0.271188	+/	0.887648	0.657231	+/	1.297292	4988.3	3.273	4211	2.561
Science & Education Center	SEC SOUTH-A	12.47/7.2	240/120	Open Wye	Open Delta	167	2.53	0.227716	+/	0.834786	0.541283	+/	1.303015	5350.7	3.666	4430.2	2.982
						100	2.37										
	SEC SOUTH-B	12.47/7.2	240/120	Open Wye	Open Delta	167	2.53	0.227716	+/	0.834786	0.541283	+/	1.303015	5350.7	3.666	4430.2	2.982
						100	2.37										
SEC NORTH-A	12.47/7.2	240/120	Open Wye	Open Delta	167	2.53	0.227716	+/	0.834786	0.541283	+/	1.303015	5350.7	3.666	4430.2	2.982	
					100	2.37											
SEC NORTH-B	12.47/7.2	240/120	Open Wye	Open Delta	167	2.53	0.227716	+/	0.834786	0.541283	+/	1.303015	5350.7	3.666	4430.2	2.982	
					100	2.37											
University Place	UP-A	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	1500	3.3	0.33884	+/	0.99903	0.782889	+/	1.756517	4388.8	2.948	3447.7	2.571
	UP-B	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	1.9	0.343406	+/	0.999673	0.791121	+/	1.758575	4380.2	2.911	3439.7	2.543
Koinonia House	KHSE	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	4.1	0.290416	+/	0.878966	0.70289	+/	1.330089	5001.5	3.027	4153.4	2.406
Graduate School of Education	SBA	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	500	4.1	0.290416	+/	0.878966	0.70289	+/	1.330089	5001.5	3.027	4153.4	2.406
School of Business Administration																	
Academic and Student Rec Center	ARC-A	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	750	5.53	0.203279	+/	0.870349	0.579547	+/	1.311054	5180.2	4.282	4330.9	3.095
	ARC-B	12.47/7.2	208/120	Wye-Gnd	Wye-Gnd	300	3.54	0.203279	+/	0.870349	0.579547	+/	1.311054	5180.2	4.282	4330.9	3.095
Urban Center	URBN-A	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	750	1.5	0.372667	+/	0.89157	0.851056	+/	1.367452	4791.3	2.392	3932.6	1.974
	URBN-B	12.47/7.2	480/277	Wye-Gnd	Wye-Gnd	750	1.5	0.372667	+/	0.89157	0.851056	+/	1.367452	4791.3	2.392	3932.6	1.974

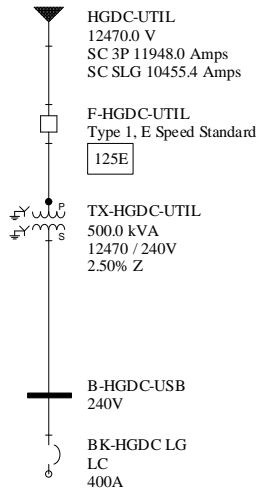
D. APPENDIX D – ONE-LINE DIAGRAMS

See power system study one-line diagrams on the attached sheets.

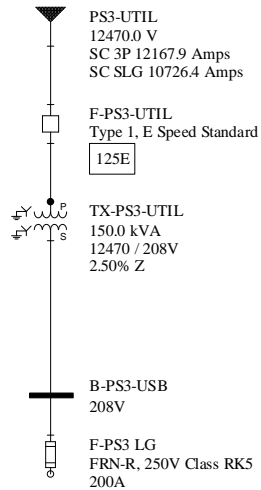
Table D.1 – One-Line Diagram Index

Campus Area	Page Number	Buildings
Northwest Campus	1 of 9	HGDC, PS3, UHP, JCB
	2 of 9	STHL, SEH, HOFF, KNGA
North-Central Campus	3 of 9	STFR, HH, PRKW
	4 of 9	HSB, MONT, SBH, BLKS
South-Central Campus	5 of 9	SH, EH, UCB
	6 of 9	OND, BHB, NASC
Southeast Campus	7 of 9	AB, EB
	8 of 9	SEC, UP
Northeast Campus	9 of 9	MCB, SBA, ARC, URBN, KHSE

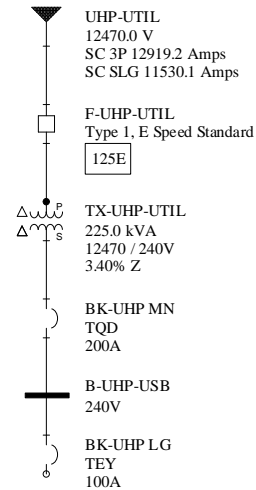
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DEVELOPMENT CENTER**



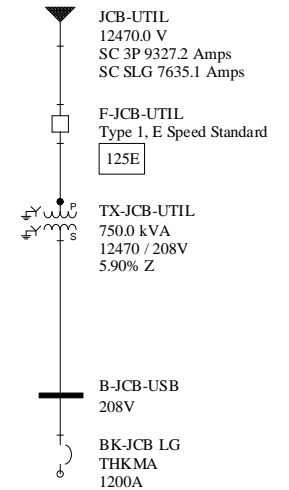
**PARKING
STRUCTURE #3**



**UNIVERSITY
HONORS PROGRAM**



**JOSEPH C.
BLUMEL HALL**



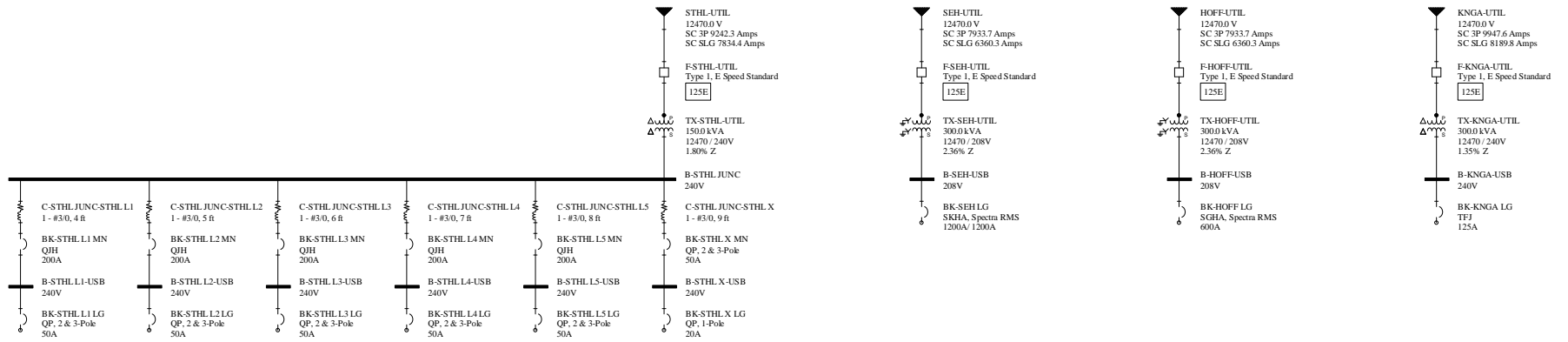
Eaton Electrical Services & Systems
 PSU - Non-West Campus Loop
 One-Line Diagram
 February 22, 2013
 Engineer: M. Moore

ST. HELEN'S HALL

STEPHEN EPLER HALL

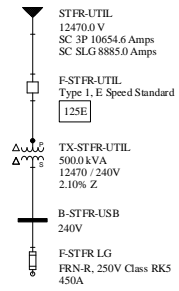
GEORGE C. HOFFMAN HALL

KING ALBERT BUILDING

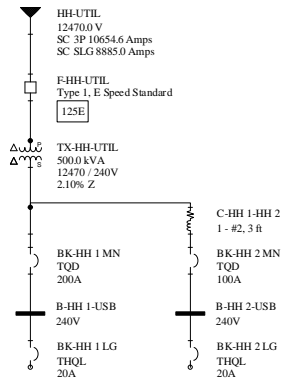


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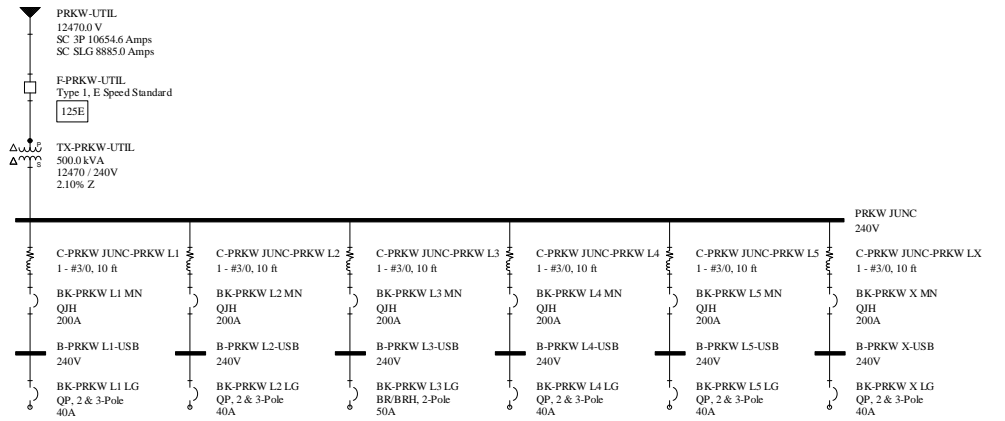
STRATFORD BUILDING



HARDER HOUSE

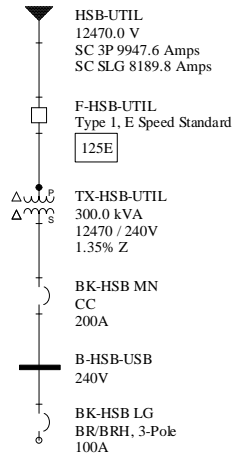


PARKWAY BUILDING

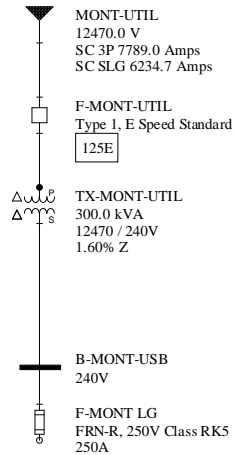


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 One-Line Diagram
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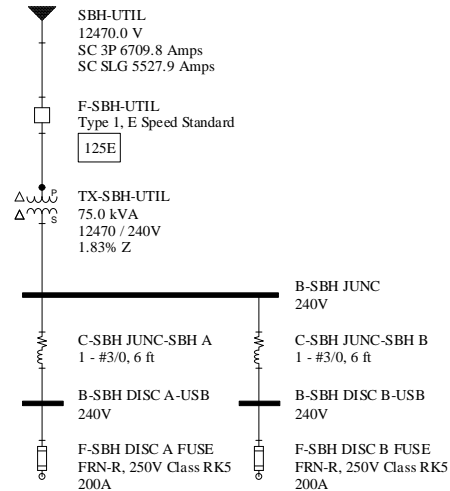
HARRISON STREET BUILDING



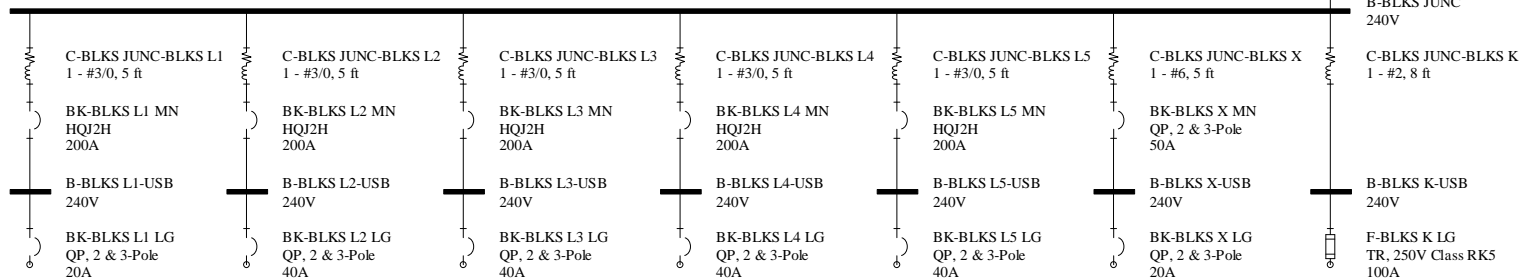
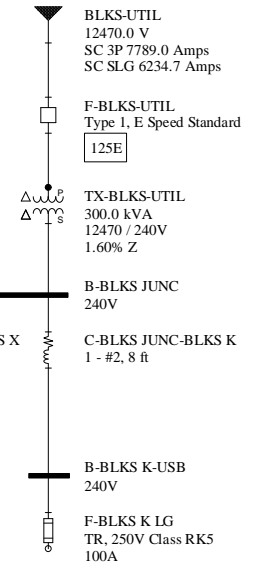
MONTGOMERY COURT



SIMON BENSON HOUSE

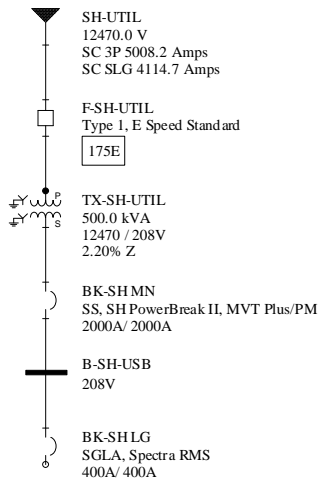


BLACKSTONE

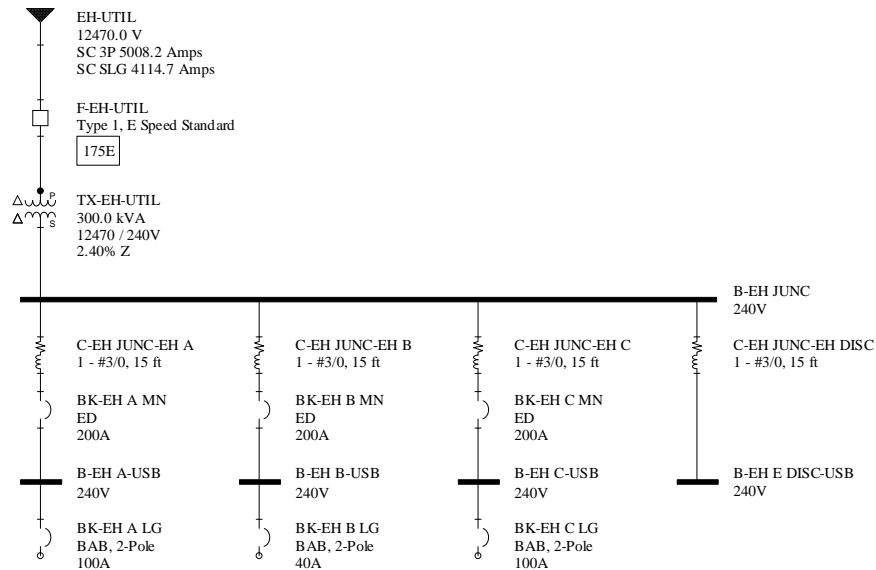


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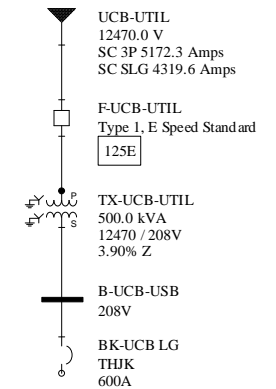
**SHATTUCK
HALL**



**EAST
HALL**



**UNIVERSITY
CENTER BUILDING**



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 PSU - Non-West Campus Loop
 One-Line Diagram
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ONDINE

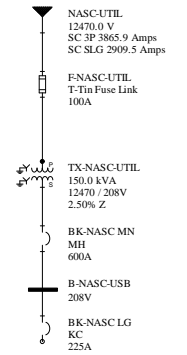
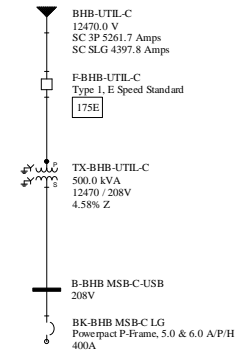
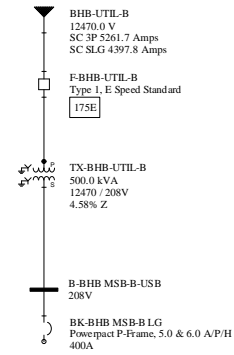
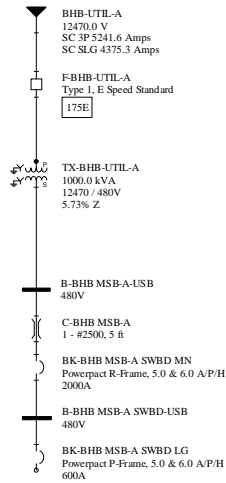
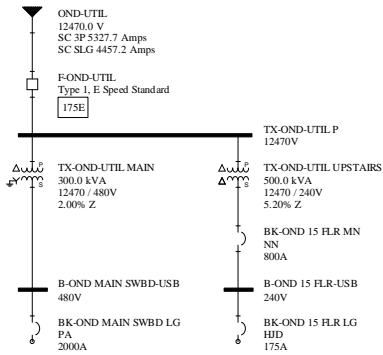
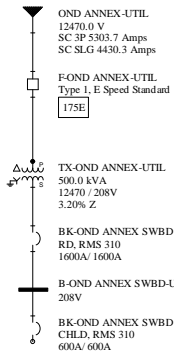
BROADWAY HOUSING BUILDING

NATIVE AMERICAN STUDENT CENTER

ANNEX

MAIN

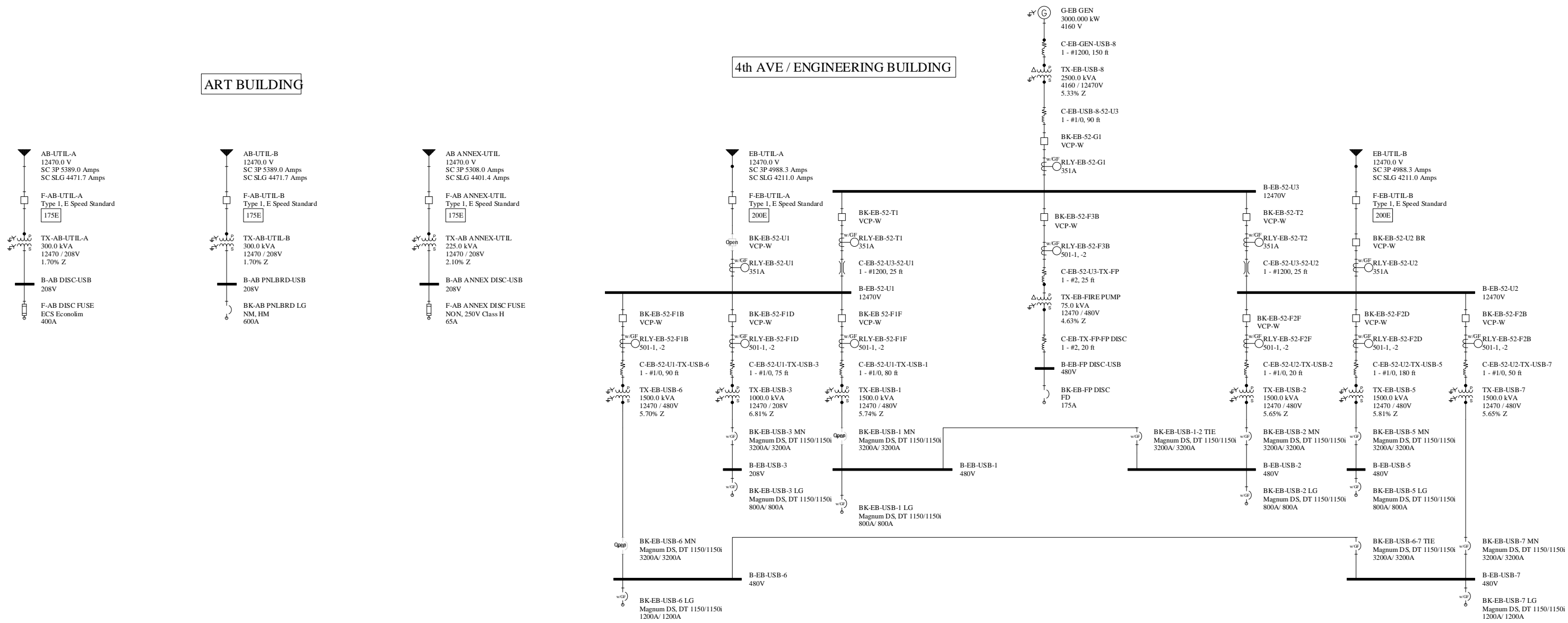
UPSTAIRS



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 One-Line Diagram
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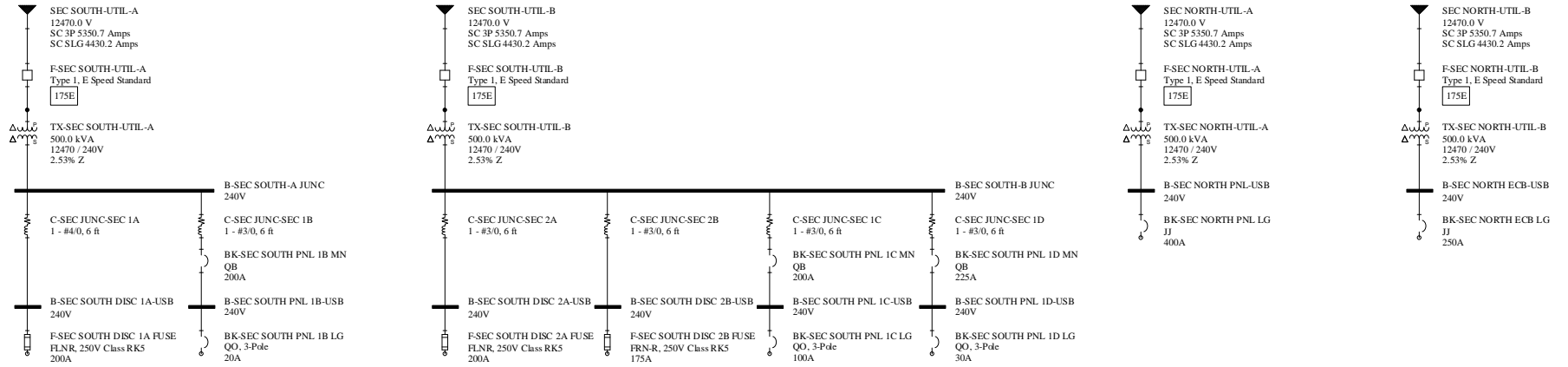
ART BUILDING

4th AVE / ENGINEERING BUILDING

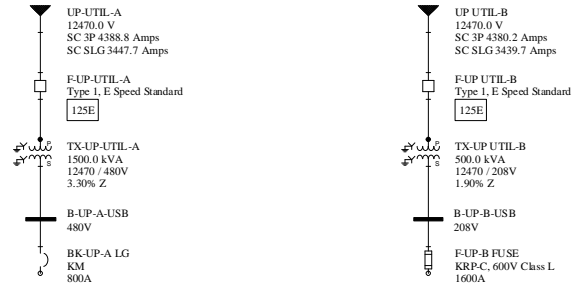


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SCIENCE EDUCATION CENTER

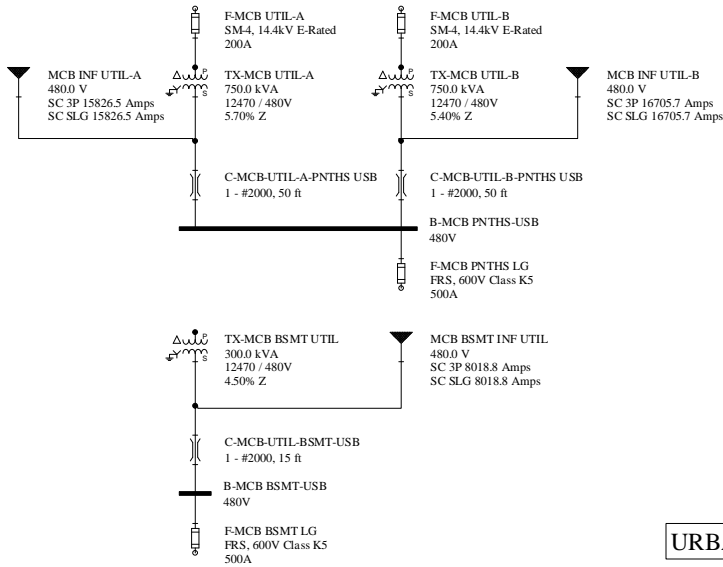


UNIVERSITY PLACE

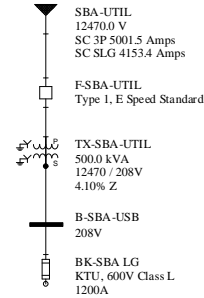


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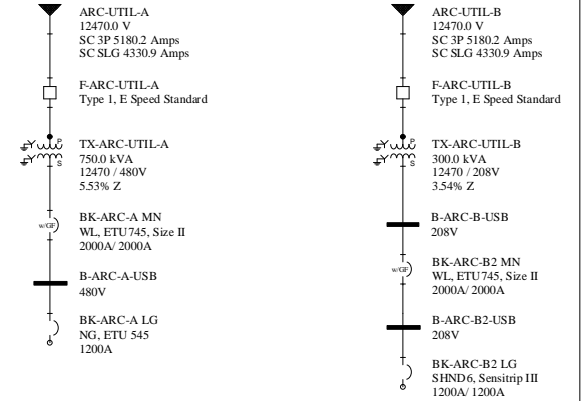
MARKET CENTER BUILDING



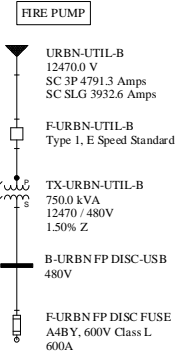
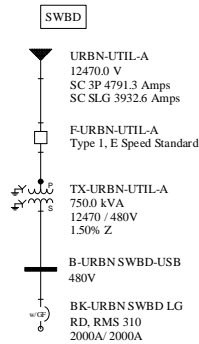
SCHOOL OF ED / BUSINESS ADMIN



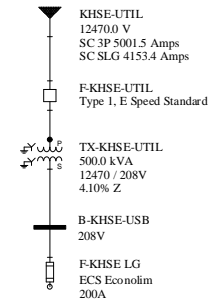
ACADEMIC & STUDENT REC CENTER



URBAN CENTER



KOINONIA HOUSE



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 PSU - Non-West Campus Loop
 One-Line Diagram
 February 22, 2013
 Engineer: M. Moore



Powering Business Worldwide

**Electrical Services & Systems
26850 SW Kinsman Road
Wilsonville, OR 97070
(503) 582-2729**

GENERAL ORDER NUMBER: ESE0008353

REPORT NUMBER: TQSISE0008353.1

SUBMITTED BY: M. MOORE

**SHORT CIRCUIT STUDY
PROTECTIVE DEVICE COORDINATION STUDY
ARC FLASH HAZARD ANALYSIS
FOR
PORTLAND STATE UNIVERSITY
WEST CAMPUS LOOP
PORTLAND, OREGON**

FEBRUARY 2013

1.0	EXECUTIVE SUMMARY	1-1
1.1	Objectives.....	1-1
1.2	Results	1-2
1.3	Recommendations.....	1-4
2.0	SHORT-CIRCUIT ANALYSIS.....	2-1
2.1	Short-Circuit Objectives.....	2-4
2.2	System Modeling.....	2-4
2.3	Short-Circuit Results.....	2-6
2.4	Equipment Evaluation.....	2-6
3.0	PROTECTIVE DEVICE COORDINATION STUDY	3-1
3.1	General Description and Protection Philosophy	3-1
3.2	Codes and Standards.....	3-2
3.3	Coordination Objectives	3-3
3.4	Coordination Results	3-3
3.5	Coordination Recommendations	3-4
3.6	Time-Current Characteristic Plots.....	3-4
4.0	RECOMMENDED PROTECTIVE DEVICE SETTINGS	4-1
5.0	ARC FLASH HAZARD ANALYSIS	5-1
5.1	Introduction.....	5-1
5.2	Study Procedure.....	5-2
5.3	Arc Flash Hazard Analysis Results.....	5-4
5.4	Arc Flash Summary Table Heading Descriptions	5-6
5.5	Arc Flash Hazard Analysis Recommendations.....	5-7
A.	APPENDIX A – SHORT-CIRCUIT INPUT REPORT	A-1
B.	APPENDIX B – SHORT-CIRCUIT RESULTS	B-1
C.	APPENDIX C – UTILITY CORRESPONDENCE	C-1
D.	APPENDIX D – ONE-LINE DIAGRAM	D-1

1.0 EXECUTIVE SUMMARY

This report contains the results of analysis performed on the electrical distribution system for the Portland State University – West Campus Loop, Portland, Oregon. The purpose of this study is to evaluate the existing electrical system, as detailed below.

The executive summary contains the description and guide to the rest of the report. In addition, it also contains the recommendations of the entire study.

1.1 Objectives

1. Short-Circuit Study

Perform a short-circuit study on the existing electrical distribution system shown in order to determine the available fault current at pertinent locations throughout the distribution system. The scope of the study includes:

- Analysis begins at the main 12.47 kV SRTC switchgear, continues through each medium voltage switchgear lineup on the West Campus Loop, and ends at the 480 V or 208 V service entrance disconnect in each West Campus Loop building shown in the contract drawing designated “12.47 kV Single Line Diagram” dated 6-20-88.

The available fault currents determined by the short-circuit study will be used in the coordination and device evaluation analysis.

2. Equipment Evaluation

Evaluate the short-circuit ratings of protective devices and other distribution equipment found at the locations shown in the drawing designated “12.47 kV Single Line Diagram” dated 6-20-88.

3. Coordination Study

Review the existing system overcurrent protection and coordination. Where applicable, provide suggestions for improvement.

4. Arc Flash Analysis

Perform an arc flash hazard analysis per NFPA 70E on the electrical distribution system described in item #1 above.

5. Recommendations

Provide specific recommendations for improving the electrical distribution system performance and correcting any deficiencies found by the studies.

1.2 Results

1. Short-Circuit Study

Short-circuit currents were calculated for each bus shown on the one-line diagram in Appendix D.

The following source impedance information was provided by Portland General Electric at the Preferred and Alternate feeds for the Science II Building:

Preferred Feed (Switch 1815):

- Voltage: 12.47 kV
- Positive Sequence Source Impedance: $0.1117 + j0.5581 \Omega$
- Zero-Sequence Source Impedance: $0.6837 + j0.7567 \Omega$

Alternate Feed (Switch 1998):

- Voltage: 12.47 kV
- Positive Sequence Source Impedance: $0.1175 + j0.5439 \Omega$
- Zero-Sequence Source Impedance: $0.3328 + j0.4914 \Omega$

A copy of the email provided by Mr. Tom Riddle with Portland General Electric can be found for review in Appendix C.

Short-circuit currents were calculated for a three-phase bolted fault and single-line-to-ground fault at each bus shown on the one-line diagram found in Appendix D. The system was modeled for worst-case fault currents.

The following short-circuit study cases were evaluated:

- Study Case No. 1 – System supplied from PGE Preferred Feed via 12.47 kV Switch 1815. Switchboard B-SRTC-SWBD1 supplied from the normal source.
- Study Case No. 2 – System supplied from PGE Preferred Feed via 12.47 kV Switch 1815. Switchboard B-SRTC-SWBD1 supplied from the emergency source.
- Study Case No. 3 – System supplied from PGE Alternate Feed via 12.47 kV Switch 1998. Switchboard B-SRTC-SWBD1 supplied from the normal source.
- Study Case No. 4 – System supplied from PGE Alternate Feed via 12.47 kV Switch 1998. Switchboard B-SRTC-SWBD1 supplied from the emergency source. **This is the worst case scenario and the scenario illustrated in the one-line diagram found in Appendix D.**

See Section 2, Appendix A and Appendix B for more information.

2. Equipment Evaluation

The Equipment Evaluation is based on the power system worst-case short-circuit current configuration.

The short-circuit ratings of protective devices and other distribution equipment are evaluated in Section 2, Table 2.1.

In summary of Table 2.1, the following equipment failed the equipment evaluation:

- LV Switchboard B-CH-SUB 4A
- LV Switchboard B-NH-USB EAST

Equipment evaluation status is listed as "UNKNOWN" and a "MINIMUM REQUIRED" short-circuit rating is suggested at locations for which distribution equipment information and/or short-circuit rating information is not available. Four locations were shown this way in this study. Each of the locations was missing a nameplate with short-circuit rating information and not enough information could be collected while on site to make a conservative assumption regarding the short-circuit rating of the equipment.

The short-circuit withstand ratings of low voltage disconnect switches are not evaluated in this study. Care should be taken in order to ensure that these devices are applied within their UL listed short-circuit withstand ratings. The typical withstand ratings for Eaton disconnect switches (safety switches) range from 10,000 A to 200,000 A for certain fused types.

3. Coordination Study

The time-current coordination plots of the protective overcurrent devices are shown in Section 3. In developing the device settings, consideration was given to both isolation of faults, protection of cables, and protection of transformers.

Efforts were made to provide the best coordination possible with the existing protective devices. It should be understood that selective coordination between two instantaneous trip units cannot be achieved for fault levels above the instantaneous pickup of the upstream device. There is some overlapping of curves that cannot be avoided.

The system coordination began at the main 12.47 kV SRTC switchgear and continued downstream through the West Campus Loop to the largest feeder breaker at each 480 V or 208 V service entrance disconnect within each West Campus Loop building. These buildings include the Science Research and Teaching Center, Science Building 1, West Heating Plant, Peter Stott Center, Millar Library, Cramer Hall, Smith Memorial Center, Library East, University Services Building, Neuberger Hall, Parking Structure 1, Lincoln Hall, and the Extended Studies Building.

See Section 3 for more information and Section 4 for device settings.

4. Suggested Protective Device Settings

Settings for the adjustable protective devices within the scope of work are shown in Section 4.

Each entry references a coordination plot number found in Section 3. The referenced plot illustrates the coordination of the listed device with the relevant “upstream” and “downstream” protective devices. The protective devices listed in Section 4 should be set per the suggested settings.

5. Arc Flash Analysis

Details of the arc flash analysis are shown in Section 5. This arc flash hazard analysis of the Portland State University – West Campus Loop in Portland, Oregon required energy and boundary calculations for approximately forty-eight (48) locations. In summary of Section 5, there are several locations that have incident energy levels that are above 40 cal/cm². According to NFPA 70E-2012, Article 130.7(A), Informational Note 3, greater emphasis must be placed on establishing an electrically safe work condition when working within the limited approach boundary at locations where the incident energy exceeds 40 cal/cm². The greater emphasis is due to additional hazards created from blast pressure associated with a possible arc. See NFPA 70E-2012, Article 120 for details on establishing an electrically safe work condition.

At the request of Portland State University, arc-flash incident energy calculations were performed at an 8’ working distance. This distance is greater than the standard working distances prescribed by IEEE 1584-2002 and are applicable for energized work, including non-contact voltage testing, being performed by a qualified person using a hot-stick. A distance of 8’ was chosen as it is the approximate distance the face and torso of a qualified person would be when using a 6’ hot-stick. To minimize confusion, these values will not be shown on the arc-flash labels.

Please note for this study, the arc flash hazard has been calculated but not the risk. The risk associated with performing energized electrical work will vary based on the work being performed as well as the condition of the equipment and other factors that can be best determined by a qualified person.

See Table 5.1, Table 5.2, and Table 5.3 for a complete arc flash summary. **Note that the incident energy values listed in Table 5.1, Table 5.2, and Table 5.3 are only valid after the recommended protective device settings shown in Section 4 have been implemented.**

1.3 Recommendations

1. Overdutied Equipment

It is recommended that the overdutied panelboards listed below be reviewed for switchboard/breaker replacement to comply with the short-circuit current

ratings required. The short-circuit rating of each of these locations is based on the lowest interrupting rating of any device in the switchboard. It is possible that replacing only the circuit breakers that are overdutied, as opposed to the entire switchboard, will sufficiently increase the rating of the switchboards below. See Section 2 for detailed short-circuit analysis.

- LV Switchboard B-CH-SUB 4A
- LV Switchboard B-NH-USB EAST

2. Additional Power Systems Studies

The scope of the analysis ended at each 480 V or 208 V main switchboard within each West Campus Loop building. These buildings include the Science Research and Teaching Center, Science Building 1, West Heating Plant, Peter Stott Center, Millar Library, Cramer Hall, Smith Memorial Center, Library East, University Services Building, Neuberger Hall, Parking Structure 1, Lincoln Hall, and the Extended Studies Building. It is recommended that the studies be expanded to include all of the low voltage distribution equipment in each of these buildings.

There are many locations that would benefit from a full short-circuit and coordination study. For example, there is a lack of selectivity between the main circuit breaker and the largest feeder breaker in the Switchboard 2 located in Science Building 2. Under the scope of this project, insufficient information was collected to recommend adjustment the settings of the largest feeder breaker. This lack of selectivity may result in an unnecessary loss of load for a fault downstream of the largest feeder breaker. Expansion of scope to include coordination of the entire low voltage system may allow for adjustment of these settings and improve the selectivity at Switchboard 2. Another location which may benefit from a full coordination study is Panelboard PNL-B in Cramer Hall. It appears the minimum settings are currently being employed on the largest feeder breaker in this panelboard. As a result, there may be a lack of selectivity with downstream loads.

Expansion of scope to include an arc flash hazard analysis for all locations supplied by the West Campus Loop will ensure that all equipment at Portland State University is properly labeled per NFPA 70E-2012 and meets all OSHA requirements that result from the general duty clause.

3. Medium Voltage Equipment Recommendations

During the testing of the Medium Voltage Cables performed by Emerson Network Power, it was found that many of the Medium Voltage Switches had not been properly maintained and did not operate properly. In the report issued by Glumac, based on the results of the Emerson Network Power testing, there are a series of recommendations regarding cleaning and maintenance of these switches. Similarly, based on the results of the Emerson Network Power testing, Glumac issued a series of

recommendations regarding replacement of medium voltage cables. Eaton agrees with all recommendations of this nature by Glumac.

Proper maintenance of the Medium Voltage Switches is vital to safe operation of this equipment. Failure to properly maintain these switches may result in a dangerous situation when they are operated. Cables which were found to need replacement in the Glumac study showed signs of insulation breakdown. This is a potentially dangerous situation which could result in an arc-flash in the event of insulation failure.

4. Low Voltage Equipment Recommendations

The majority of the low voltage equipment on the West Campus loop at Portland State University is very old and appears to have not been tested and maintained over the life of the equipment. It is critical that Portland State University create a plan to inspect and test the low voltage equipment supplied by this loop, similar to the testing that has occurred in Science Building, to determine if the electrical distribution equipment is still operable. Because testing has recently occurred at both Science Building 2 and Lincoln Hall, the remainder of the buildings should be given priority. If any equipment is found to not be performing as originally intended, a plan to replace the equipment should occur. The following discussion highlights specific recommendations and is broken out by building.

- Science Building 1

The low voltage equipment in Science Building 1 (208 V) has been verified in its entirety. The 208 V switchboard contains many older fused switches that supply the loads in Science Building 1. Based on the age of the equipment it is recommended that this equipment be replaced or tested and maintained according to manufacturer recommendations.

- Extended Studies Building

The protective devices contained in the low voltage main switchboard in the XSB Building have been verified. However, the transformer manufactured by Sorgel Electrical that steps the voltage down from 12.47 kV to 208 V does not have a nameplate installed. As a result, the transformer information including the kVA rating, voltage ratings, winding connections, and impedance could not be field verified at the time of the study. Additionally, it was determined that some fuses were mounted in an aftermarket enclosure which acts as secondary protection for the transformer supplying power to XSB. The fuses are not mounted in a switch, but rather bolted in place. It is recommended that this fuse assembly be replaced with a new, fused safety switch or main breaker.

- Science Research and Teaching Center, Switchboard #1, Section 1

The low voltage equipment in Science Building 2, Switchboard 1, Section 1 (208 V) has been verified. The main breaker in Section 1 has been retro-fit with an AC-Pro electronic trip unit. During data collection, the as found

settings could not be determined. As a result, it is recommended that this trip unit be tested and the settings in Section 4 be implemented.

- Heating Plant

The low voltage equipment in the Heating Plant (480 V) has been verified in its entirety. Due to the age of this equipment it is highly recommended that the molded case circuit breakers and panelboard be tested to ensure proper operation. If the testing shows that these circuit breakers do not operate as intended, it is recommended that this panelboard be replaced.

- Physical Education (Peter Scott Center)

Several of the sub main breakers in the low voltage switchboard in the Peter Scott Center could not be field verified. The equipment covers and deadfronts for the 1600A sub main breakers manufactured by Mears Controls could not be removed while energized without tripping the breaker. As a result, the next time the Peter Scott Center 480 V switchboard is de-energized for maintenance, the fuses contained in these fused breakers should be verified.

- Library Building West (Millar)

The low voltage equipment in the Library West (Millar) building (480 V) has been verified in its entirety. The 480 V switchboard contains many older fused switches that supply the loads in Science Building 1. Based on the age of the equipment it is recommended that this equipment be tested and maintained according to manufacturer recommendations.

- Cramer Hall SE

The low voltage equipment in Cramer Hall – SE main distribution switchboard (208 V) has been verified. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable.

- Cramer Hall Emergency

The low voltage equipment in Cramer Hall – Emergency switchboard (208 V) has been verified. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable.

- Cramer Hall Panel B

The low voltage equipment in Cramer Hall – Panel B (480 V) has been verified. Panel B is a newer style, Square D, Type QED switchboard that appears to be in better condition compared to other equipment in Cramer Hall. However, it is still recommended that this equipment is tested and maintained according to manufacturer recommendations.

- Cramer Hall Sub 4A

The low voltage equipment in Cramer Hall – Substation 4A has been verified. However, it was not possible to verify the existing settings on the 1600 A and 1000 A feeder breakers as the trip unit batteries appeared to be dead. The trip units utilized in these circuit breakers are General Electric, MicroVersaTrip electronic trip units that are self-powered and require a certain amount of load current on the breaker. Without enough load current, the trip unit must be powered via the battery backup. It is recommended that the batteries be replaced and the settings verified.

- Cramer Hall Northwest

The protective devices contained in the low voltage main switchboard in Lincoln Hall (208 V) have been verified. However, these protective devices were made by ITE and appear to have been neglected and not tested over the years. It is highly recommended that these devices be tested and replaced as necessary. Additionally, the transformer that steps the voltage down from 12.47 kV to 208 V is housed in a separate electrical room near the low voltage equipment. However, due to the lack of enclosures, the transformer could not be safely accessed during data collection. As a result, the transformer nameplate information as well as the secondary conductor information could not be obtained for use in this analysis.

It is recommended that PSU consider replacing this bank of 3, single phase transformers with a new, three-phase transformer in a suitable enclosure. It is also recommended that all conductors be moved to conduits. This would ensure that if an unqualified person entered the room, the shock and arc flash hazard would be reduced significantly. Presently, it is critical only qualified people have access to the lock on the door.

- College Center Building (Smith Memorial Center)

The main low voltage equipment in Smith Memorial Center has been verified. However, four of the sub main breakers could not be accessed safely during data collection. These four breakers were manufactured by Federal Pacific and are rated at 50 kAIC at 208 V. If the covers of these sub-main breakers are removed it is possible that the circuit breaker could trip. As a result, the next time this low voltage equipment is taken down for maintenance, the circuit breaker settings should be verified. Additionally, based on the condition and appearance of the switchboard, it is highly recommended that the switchboard and all of the circuit breakers be tested and replaced as necessary.

Additionally, a 750 kVA transformer is used to supply this low voltage equipment. The low voltage conductors run from the transformer to the low voltage switchboard in the Smith Memorial Center. The conductor terminations on the secondary side of the transformer are not in a guarded enclosure. Electrical tape, which is used to provide insulation from energized equipment, is prone to breaking down. It is highly recommended that these

conductors be re-run in an appropriately sized conduit to prevent personnel in the room from coming into contact with these energized conductors.

- College Center Building (2nd Addition)

The low voltage equipment in Smith Memorial Center – 2nd Addition (208 V) has been verified. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable.

- Library Building East

The main breaker in the low voltage switchboard in the Library Building East could not be field verified. The equipment covers and deadfronts for the main breaker manufactured by Mears Controls could not be removed while energized without tripping the breaker. As a result, the next time this switchboard is de-energized for maintenance, the fuses contained in these fused breakers should be verified. Additionally, due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable.

- University Services / Parking #2

The low voltage equipment in University Services Building / Parking Structure #1 (208 V) has been verified. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable.

- Neuberger Hall – West and East

The low voltage equipment in Neuberger Hall – Both the East and West main switchboards (208 V) have been verified. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable. Also, during the data collection it was observed that a meter located in the East Switchboard had been broken. A wooden cover had been constructed as an attempt to isolate this meter. This is a highly dangerous situation and needs to be corrected as soon as possible. The meter should be replaced and the wooden cover should be removed.



Figure 1-1 - Meter

- Parking #1

The low voltage equipment in Parking Structure #1 was very old ITE equipment. There are no published interrupting ratings for the equipment. As a result, a minimum required rating will be assigned to this switchboard that can be used if / when the interrupting rating of this equipment can be determined. Due to the age and existing state of this equipment it is highly recommended that the switchboard and breakers be tested to ensure that the equipment is still operable. Additionally, during the on-site data collection only one set of 500 kcmil copper conductors was noted. The one-line diagram illustrated two sets of conductors per phase at the time of construction. With only set of 500 kcmil copper conductors per phase, the upstream fusing cannot provide proper protection per NEC 240.4(F).

5. Recommended Settings

Adjustable protective device settings should be set according to the settings tables provided in Section 4.

6. Inaccessible data

In addition to individual breaker data that was unavailable due to operating mechanisms covering some breaker types and settings, the following equipment could not be verified during the data collection effort. As a result, some data such as fuse types, relay time dial curve selection, breaker types, equipment interrupting ratings, and equipment manufacturers could not be verified. It is recommended that the following list be reviewed to determine if any of the data can be accessed by the proper personnel during a maintenance shutdown or outage.

- Science Research and Teaching Center (SRTC)

The nameplates on the Science Building 2 switchgear (B-SRTC-SB2) did not show the speed rating of the S&C, Type SM-5 fuses installed in the switchgear. It was assumed that “standard speed” fuses were utilized in this switchgear.

The existing settings on the AC-Pro trip unit used on the main circuit breaker in switchboard 1 (B-SRTC-SWBD1) could not be verified during the data collection as the trip unit was non-responsive.

- Science Building 1

In the main 12.47 kV Science Building 1 Switchgear the nameplate for the fused switch that supplies Lincoln Hall indicated that fuses used in the switch were S&C, Type SM-5, 60E fuses. A time current curve for the 60E fuse could not be obtained and it was assumed that 80E fuses are used in this switch according to previous study documentation.

- Lincoln Hall

The main transformer for Lincoln Hall is contained in a utility vault that could not be accessed during data collection. As a result, it was assumed that this transformer was a 1000 kVA, delta-wye, 12.47 kV - 208 / 120 V transformer, as indicated on the contract one-line diagram, with an impedance of 5.32%. Furthermore, the secondary conductors were assumed to be eight (8) sets of 500 kcmil copper conductors per phase.

- Extended Studies Building

The main transformer for the Extended Studies Building was manufactured by Sorgel Electric and does not have a nameplate. As a result, it was assumed that this transformer was a 200 kVA, delta-wye, 12.47 kV - 208 / 120 V transformer, as indicated on the contract one-line diagram, with an impedance of 2.15%.

The nameplate on the 12.47 kV disconnect switch did not show the speed rating of the S&C, Type SM-4 fuses installed in the switch. It was assumed that “standard speed” fuses were utilized in this switchgear.

- Peter Stott Center

The feeder breakers in the 480 V main switchboard are manufactured by Mears Controls. The fuses contained in these fused breakers could not be determined during the data collection as the breaker needs to be de-energized to verify the fuse information.

- Cramer Hall

The main Cramer Hall medium voltage switchgear (B-CH) did not have fuse information for each feeder. As a result, the fuses used to supply transformer CH-003 were assumed to be S&C, Type SM-5, 25E. The fuses used to supply the Smith Memorial Student Union were assumed to be S&C, Type SM-5, 100E. The fuses used to supply the University Services Building were

assumed to be S&C, Type SM-5, 50E. This information agrees with a previous study performed for Portland State University.

The Cramer Hall – NW distribution medium voltage switchgear (B-CH-NW SWBD DS) did not have a nameplate that listed the equipment rating or fuse type. As a result, it was assumed that S&C, Type SM-5, 40E fuses were used to supply the NW transformer (as indicated on the Cramer Hall one-line diagram provided by PSU).

The main transformer that supplies Cramer Hall – NW distribution could not be accessed safely during data collection. As a result, it was assumed that this transformer was a 500 kVA, delta-wye, 12.47 kV - 208 / 120 V transformer, with an impedance of 1.85% (as indicated on the Cramer Hall one-line diagram provided by PSU). Furthermore, the secondary conductors were assumed to be four (4) sets of 600 kcmil copper conductors per phase.

The main 12.47 kV disconnect at Sub 4A did not have any fuse information noted. A one-line diagram provided by PSU indicated that the fuses used in the switch were S&C, Type SM-5, Standard Speed 60E fuses. A time current curve for the 60E fuse could not be obtained and it was assumed that 65E fuses are used in this switch.

The fuses contained in the bolted pressure switch located in Cramer Hall that is used as a main disconnect for PNL B (B-CH-PNL B) could not be determined during the data collection. As a result, it was assumed that Bussmann, Type KRP-C, Class L, 1200 A fuses were used. These fuses are used in similar switches on the PSU campus.

- Library East:

The main breaker in the 208 V main switchboard was manufactured by Mears Controls. The fuses contained in this fused breaker could not be determined during the data collection as the breaker needs to be de-energized to verify the fuse information.

- Medium Voltage Distribution System:

The cable information for portions of the medium voltage distribution system could not be verified. If the cable was not tested during the December 2012 testing, the cable size and insulation type could not be verified. As a result, Table 1.1 illustrates the cable assumptions that were used in the analysis. If these cables or associated medium voltage switchgear is tested in the future, these assumptions should be verified and the study should be revised if necessary.

Table 1.1 – Conductor Assumptions			
From	To	Conductor Size, # sets / phase	Distance
Science Building 2 (B-SRTC-SB2)	Transformer TX-SRTC-SWBD1-1	1-#1/0 / ϕ	30'
Science Building 2 (B-SRTC-SB2)	Transformer TX-SRTC-SWBD1-2	1-#1/0 / ϕ	60'
Science Building 2 (B-SRTC-SB2)	Transformer TX-SRTC-SWBD2	1-#1/0 / ϕ	20'
Science Building 2 (B-SRTC-SB2)	Transformer TX-SRTC-SWBD3	1-#1/0 / ϕ	20'
Science Building 2 (B-SRTC-SB2)	B-SRTC-SWBD4 DS	1-#4/0 / ϕ	75'
B-SRTC-SWBD4 DS	Transformer TX-SRTC-SWBD4	1-#4/0 / ϕ	5'
West Heat Plant (B-WHP)	Transformer TX-WHP-USB	1-#1 / ϕ	5'
Peter Stott Center (B-PSC)	Transformer TX-PSC-USB	1-#1/0 / ϕ	5'
Millar Library (B-ML)	Transformer TX-ML-USB	1-#1/0 / ϕ	5'
Science Building 1 (B-SB1)	Transformer TX-SB1-USB	1-#1/0 / ϕ	10'
Extended Studies (B-XSB-TX DS)	Transformer TX-XSB-USB	1-#2 / ϕ	5'
Lincoln Hall (B-LH-TX DS)	Transformer TX-LH-USB	1-#2 / ϕ	175'
Cramer NW (B-CH-NW USB DS)	Transformer TX-CH-NW USB	1-#1/0 / ϕ	15'
Cramer Hall (B-CH CHLR)	Transformer TX-CH-002	1-#1/0 / ϕ	5'
Cramer Hall (B-CH CHLR)	B-CH-SUB 4A DS	1-#4/0 / ϕ	300'
Sub 4A (B-CH-SUB 4A DS)	Transformer TX-CH-006	1-#4/0 / ϕ	5'
Parking 2 (B-PS2-TX DS)	Transformer 1 TX-PS2-USB	1-#1/0 / ϕ	10'
Smith Memorial (B-SMC)	Transformer TX-SMC-USB	1-#1/0 / ϕ	30'
Smith Memorial (B-SMC 2ND USB DS)	Transformer TX-SMC 2ND USB	1-#1/0 / ϕ	5'
Library East (B-LE USB DS)	Transformer TX-LE USB	1-#1/0 / ϕ	5'
Neuberger Hall (B-NH EAST)	Transformer TX-NH-USB EAST	1-#1/0 / ϕ	5'
Neuberger Hall (B-NH WEST)	Transformer TX-NH-USB WEST	1-#1/0 / ϕ	5'
Parking 1 (B-PS1-TX DS)	Transformer TX-PS1-USB	1-#1 / ϕ	5'

7. Reducing Incident Energy Levels

The calculated incident energy at a particular location is dependent on three main factors: short-circuit current, distance, and time. These three factors directly affect the incident energy in the following manner:

Short-circuit current: The short-circuit current for a given power system is dependent on the system impedance and source fault current, and cannot be easily reduced.

Distance: IEEE Std 1584™-2002 provides a table with typical working distances. Increasing the working distance reduces the amount of incident energy that reaches the worker; however it becomes difficult to perform many work tasks with an increased working distance, therefore, this is not an optimal solution for most cases.

Time: The incident energy decreases when reducing the exposure time of the arc. This exposure time is directly related to the clearing time of the protective device(s) which feed the fault location.

Based on the preceding summary, arc flash mitigation techniques are most effective and feasible when they involve reducing the arc exposure time. In many locations, the setting of the protective device can be adjusted in order to decrease the interrupting time, resulting in a decreased incident energy. However, in this study, settings for protective devices have not been adjusted to reduce incident energy if the chance of nuisance trips within critical circuits is introduced.

The other option involving reducing the arc exposure time is to consider equipment modifications and upgrades. Several solutions include upgrading trip units, installing “maintenance switches”, and using relays with multiple settings groups. Each specific location needs to be analyzed to determine which reduction method is best employed.

8. Testing and Preventative Maintenance

It is recommended that regularly scheduled testing and preventative maintenance be performed to ensure that the electrical distribution equipment continues to perform at an optimum level. Testing should entail primary injection testing of all power circuit breakers to verify proper tripping ranges, contact resistance testing, insulation resistance testing and complete switchgear and transformer cleaning and inspection.

9. Periodic Arc Flash Analysis Review

The 2012 edition of NFPA 70E includes several new requirements regarding arc flash hazard analysis. One new requirement found in Article 130 is that an arc flash hazard analysis must be updated:

- Every five years (at minimum)
- When the electrical system is modified or renovated in any way, including renovations, additions, or subtractions to the system

It is recommended that a plan is implemented to schedule a review of the arc flash hazard analysis for the Portland State University - West Campus Loop in a period not to exceed five years, and that a review is performed whenever substantial modifications or renovations take place.

10. Predictive Diagnostics Using Continuous Partial Discharge Measurements

Eaton recommends conducting Continuous Partial Discharge measurements on most medium voltage power transformers, bus ducts, switchgear, motors, generators, terminations, and splices of transmission and distribution cables. Partial Discharge (PD) analysis is a non-invasive, online method of collecting, filtering, and evaluating PD occurring in electrical apparatus. The goals are:

- To detect partial discharges as a result of failing or compromised insulation
- To analyze the partial discharge activity, and if an insulation defect is detected:
 - a. Make conclusions as to the severity of the defect.
 - b. Advise as to possible defect locations and possible cause(s) of the defect.
 - c. Advise as to urgency of inspection.
 - d. Suggest preventive measures both immediate and long term.

Electrical insulation is very important to monitor as it defines a major item in the reliability of electrical machines. Continuous Partial Discharge on-line monitoring using the Eaton InsulGard™ is the most sensitive and reliable method for detecting failing insulation. PD monitoring when used in conjunction with Eaton's RM™ system offers customers the added benefit of prompt expert analysis and recommendation.

2.0 SHORT-CIRCUIT ANALYSIS

The short-circuit study determines the fault currents that flow in the system during various fault conditions. The calculated fault currents are used in the device evaluation and coordination studies. See Appendix A and Appendix B for the computer generated input data and output data. NEC-2011, Article 110.24(A) requires that service entrance equipment is labeled with the following pieces of information:

- Maximum available fault current
- Date on which the fault current was calculated

Article 110.24(B) adds that if there is a modification that may change this fault current value, it must be recalculated. The field marking must be updated to reflect the new value of maximum fault current.

The short-circuit calculations were done using A_FAULT, a computer software package by SKM Systems Analysis. The short-circuit analysis performed by A_FAULT is based on IEEE Std C37.010™-1999, IEEE Std C37.5™-1979, and IEEE Std C37.13™-2008.

Separate “Z” (complex), “X” (reactive), and “R” (resistive) networks are used by A_FAULT for the short-circuit analysis. A_FAULT uses complex network reduction and the relationship E/Z to calculate the fault current magnitude and angle at each faulted bus. The complex equivalent circuit impedance, Z , is calculated by the reduction of the “Z” (complex) network, and is reported as the “EQUIV. IMPEDANCE” in the A_FAULT reports. The X/R ratios calculated for each fault condition are based on the separate reduction of the X and R networks. These X/R ratios are used for the calculation of fault duty multipliers, to evaluate the short-circuit ratings of system components.

A_FAULT is capable of generating three types of short-circuit reports for both balanced (three-phase bolted) and unbalanced (line-to-ground) faults. The reports that are generated depend on the system that is being evaluated.

The three types of short-circuit reports are:

- Fault Report (for low voltage)
- Momentary Duty Report (for medium voltage)
- Interrupting Duty Report (for medium voltage)

1. Fault Report

The fault currents reported in the “Fault Report” are applicable to low voltage devices and components. The fault currents calculated in this report are based on the contribution data derived from IEEE Std C37.13-2008. The fault currents are calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the first cycle duty multipliers described in IEEE Std 141™-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The momentary symmetrical current = E/Z .
- The X/R ratio is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.

Multiplying factors are determined, and used to adjust the calculated symmetrical fault current. The adjusted current is used to evaluate low voltage protective devices. Low voltage output algorithms and output reports reflect NEMA AB-1 molded case breaker de-rating multipliers. Breakers are de-rated for circuits where the power factor is lower than the NEMA test circuit (higher X/R ratio). The multipliers adjust the symmetrical fault current to the value associated with the systems fault point X/R ratio. The adjusted value listed on the report may then be compared directly with the manufacturer's published interrupting rating.

2. Momentary Duty Report

The “Momentary Duty Report” contains the calculated fault currents that occur during the first half-cycle of the fault. The momentary fault currents are used to evaluate medium and high voltage fuses, and the “closing and latching” capability (momentary rating) of medium and high voltage breakers. The fault currents reported in the “Momentary Duty Report” are calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the first cycle duty multipliers described in IEEE Std 141-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The momentary symmetrical current = E/Z .
- The X/R ratio reported is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.
- A_FAULT calculates and reports the momentary asymmetrical current in two different ways, once as “sym*1.6” and again as “momentary based on X/R ”. The “sym*1.6” value is the momentary symmetrical current multiplied by 1.6. The “momentary based on X/R ” value is the momentary symmetrical current multiplied by

$$\sqrt{1+2e^{(-2\pi/(X/R))}}$$

3. Interrupting Duty Report

The fault currents reported in the “Interrupting Duty Report” are used to evaluate the interrupting rating of medium- and high-voltage breakers. The interrupting symmetrical current is calculated as follows:

- Motor and generator subtransient reactance values (X_d'') are adjusted per the interrupting duty multipliers described in IEEE Std 141-1993 (Red Book).
- The complex equivalent circuit impedance, Z , is calculated by network reduction of the “ Z ” (complex) network.
- The interrupting symmetrical current = E/Z .
- The X/R ratio reported is equal to the equivalent circuit reactance, X , divided by the equivalent circuit resistance, R . As discussed above, X is calculated by the reduction of the “ X ” (reactive) network and R is calculated by the reduction of the “ R ” (resistive) network.
- A_FAULT uses the calculated X/R ratio to determine the minimum contact parting time multiplying factors for 2, 3, 5, and 8 cycle breakers. The multiplying factors are based on IEEE Std C37.5-1979 and IEEE Std C37.010-1999 standards. The multiplying factors are applied to the interrupting symmetrical current in order to calculate the RMS short-circuit current interrupting duty for 2, 3, 5, and 8 cycle breakers. This duty is compared to the symmetrical current interrupting rating of the circuit breaker. NACD (No AC Decrement) ratios are calculated with consideration of generator "Local" and "Remote" contributions as outlined in IEEE Std C37.010-1999.
- Motor and generator impedance multipliers for the short-circuit calculations are summarized in the following table. This is based on the recommended combination network for comprehensive multi-voltage system calculations (from IEEE Std 141-1993; Red Book):

<u>Machine Type</u>	<u>Impedance (First Cycle Duty)</u>	<u>Impedance (Interrupting Duty)</u>
Turbine generators, Condensers, Hydrogenerators with amortisseur windings	1.0 Xd"	1.0 Xd"
Synchronous motors	1.0 Xd"	1.5 Xd"
Induction motors > 1000 hp at speed ≤ 1800 RPM, or > 250 hp at 3600 RPM.	1.0 Xd"	1.5 Xd"
Induction motors ≥ 50 hp not covered above.	1.2 Xd"	3.0 Xd"
Induction motors < 50 hp	1.67 Xd"	Neglect

Note: Xd" is the subtransient reactance of the rotating machine.

2.1 Short-Circuit Objectives

The objective of the short-circuit analysis is to calculate the maximum short-circuit currents produced by balanced three-phase and unbalanced faults at each bus shown on the one-line diagram in Appendix D.

2.2 System Modeling

Short-circuit currents were calculated for a three-phase bolted fault and single-line-to-ground fault at each bus shown on the one-line diagram found in Appendix D. The system was modeled for worst-case fault currents.

1. Cases:

The following short-circuit study cases were evaluated:

- Study Case No. 1 – System supplied from PGE Preferred Feed via 12.47 kV Switch 1815. Switchboard B-SRTC-SWBD1 supplied from the normal source.
- Study Case No. 2 – System supplied from PGE Preferred Feed via 12.47 kV Switch 1815. Switchboard B-SRTC-SWBD1 supplied from the emergency source.
- Study Case No. 3 – System supplied from PGE Alternate Feed via 12.47 kV Switch 1998. Switchboard B-SRTC-SWBD1 supplied from the normal source.
- Study Case No. 4 – System supplied from PGE Alternate Feed via 12.47 kV Switch 1998. Switchboard B-SRTC-SWBD1 supplied from the

emergency source. **This is the worst case scenario and the scenario illustrated in the one-line diagram found in Appendix D.**

2. Utility Information:

The following source impedance information was obtained from Mr. Tom Riddle with Portland General Electric on 1/16/13 via email.

Preferred Feed (Switch 1815):

- Voltage: 12.47 kV
- Positive Sequence Source Impedance: $0.1117 + j0.5581 \Omega$
- Zero-Sequence Source Impedance: $0.6837 + j0.7567 \Omega$

Alternate Feed (Switch 1998):

- Voltage: 12.47 kV
- Positive Sequence Source Impedance: $0.1175 + j0.5439 \Omega$
- Zero-Sequence Source Impedance: $0.3328 + j0.4914 \Omega$

A copy of the email provided by Portland General Electric can be found for review in Appendix C.

3. System Information:

Input data used in this study was obtained from the following sources:

- Contract drawing – “12.47 kV Single Line Diagram” dated 6-20-88.
- Eaton on-site data collection performed in August of 2012.
- Medium Voltage testing report issued by Glumac in February of 2013.

4. Assumptions:

The following assumptions were used in modeling the power system, and ensure conservative, worst-case results:

- It was assumed motor contributions to system fault currents would be negligible.
- System voltage is modeled at 100% nominal.
- All medium voltage cable was modeled in non-magnetic conduit.
- Unless otherwise provided, transformer X/R ratios are obtained from IEEE Std C37.010-1999.

Complete information regarding the system model used for the computer simulation is included in Appendix A.

2.3 Short-Circuit Results

The results of the short-circuit analysis, including calculated branch contributions, are provided in Appendix B. The one-line diagram with referenced bus identification is included in Appendix D.

2.4 Equipment Evaluation

The purpose of the equipment evaluation is to compare the **maximum** calculated short-circuit currents to the short-circuit ratings of protective devices. The comparison is made in order to determine if the device can interrupt or withstand the available fault currents of the electrical system to which the device is applied, as required by NEC-2011, Article 110.9 and NEC-2011, Article 110.10. The device evaluation follows the evaluation procedures outlined in IEEE Std C37.13-2008, IEEE Std C37.010-1999, IEEE Std C37.5-1979, IEEE Std C37.41™-2008, IEEE Std 1015™-2006 (Blue Book), and applicable ANSI, NEMA, and UL standards.

The results of the short-circuit equipment evaluation are summarized in Table 2.1. The table indicates “Bus I.D.” (corresponds to bus designations used in the one-line diagram of Appendix D), “Manufacturer”, “Status” (Pass, fail, unknown, or marginal), “Type” (equipment category), “Equip Volts”, calculated short-circuit duty, the equipment short-circuit rating, the series rating (if applicable), and the maximum duty rating.

The maximum duty rating is calculated by:

$$\frac{S.C.duty}{DeviceS.C.Rating} \times 100$$

If the short-circuit rating of a device is not known, a MINIMUM REQUIRED short-circuit rating is listed. The MINIMUM REQUIRED rating at each location below is the lowest common rating for each type of equipment which will pass the equipment evaluation. For equipment with series ratings, the maximum duty rating is calculated using the series rating instead of the individual device short-circuit rating. All short-circuit current values are reported in units of kA.

1. For low voltage devices:

The calculated short-circuit duty is reported under “Calc Isc (kA)” and the device short-circuit rating is reported under “Equip Isc (kA)”. The calculated duty has been adjusted accordingly per the system X/R and device test X/R.

2. For medium/high voltage fuses, switches, and motor starters:

The calculated *momentary symmetrical* short-circuit duty is reported under “Calc Isc (kA)” and the device’s momentary symmetrical short-circuit rating is reported under “Equip Isc (kA)”. The calculated *momentary asymmetrical* duty

is reported under "Calc Mom (kA)". The device's momentary asymmetrical short-circuit rating is reported under "Equip Mom (kA)".

Table 2.1 - Equipment Evaluation

Bus I.D.	Manufacturer	Status	Type	Bus Voltage (V)	Calc Isc (kA)	Equip Isc (kA)	Rating %	Calc Mom (kA)	Equip Mom (kA)	Rating %
B-CH-PNL B DS	Square D	Pass	LV Disconnect	480	19.74 (*N1)	200.00	9.87			
B-XSB USB DS	Bussmann	Pass	LV Disconnect	208	20.60	200.00	10.30			
B-PS1-USB	Coast Electric	Pass	LV Panelboard	208	8.56	40.00	21.39			
B-CH-EMER USB	GE	Pass	LV Switchboard	208	14.59	42.00	34.74			
B-CH-NW USB	ITE	Unknown	LV Switchboard	208	62.59	MIN REQUIRED = 65 KAIC				
B-CH-PNL B	Square D	Pass	LV Switchboard	480	18.29	30.00	60.97			
B-CH-SE USB	GE	Pass	LV Switchboard	208	47.16 (*N1)	65.00	72.55			
B-CH-SUB 4A	GE	Fail	LV Switchboard	480	*46.56 (*N1)	30.00	*155.21			
B-LE USB	Mears Controls, Inc.	Pass	LV Switchboard	208	25.76	42.00	61.34			
B-LH-USB	Siemens	Pass	LV Switchboard	208	43.96	65.00	67.64			
B-ML-USB	Square D	Pass	LV Switchboard	480	15.81	65.00	24.32			
B-NH-USB EAST	Square D	Fail	LV Switchboard	208	*46.14	42.00	*109.87			
B-NH-USB WEST	Square D	Pass	LV Switchboard	208	43.03	65.00	66.21			
B-PS2-USB	Zinsco	Pass	LV Switchboard	208	32.39	42.00	77.12			
B-PSC-USB	Mears Controls	Pass	LV Switchboard	480	15.02	20.00	75.10			
B-SB1-USB	GE	Pass	LV Switchboard	208	41.56	200.00	20.78			
B-SMC 2ND USB	GE	Pass	LV Switchboard	208	26.66	42.00	63.47			
B-SMC USB	Fouch Electric	Pass	LV Switchboard	208	34.05	50.00	68.09			
B-SRTC-SWBD1	Westinghouse	Pass	LV Switchboard	208	45.29 (*N1)	65.00	69.67			
B-SRTC-SWBD2	Westinghouse	Pass	LV Switchboard	480	15.46	22.00	70.27			
B-SRTC-SWBD3	Westinghouse	Pass	LV Switchboard	480	15.46	22.00	70.27			
B-SRTC-SWBD5	Eaton	Pass	LV Switchboard	480	40.26 (*N1)	65.00	61.94			
B-WHP-USB	Westinghouse	Pass	LV Switchboard	480	3.24	25.00	12.95			
B-XSB USB	Square D	Pass	LV Switchboard	208	20.48	25.00	81.93			
B-SRTC-SWBD4	Westinghouse	Pass	MV Disconnect	4160	3.66	40.00	9.14	4.82	61.00	7.90
B-SRTC-SWBD4 DS	Westinghouse	Pass	MV Disconnect	12470	12.63	27.50	45.94	15.06	40.00	37.66
B-CH CHLR DS	GE	Pass	MV Switch	12470	10.97	25.00	43.87	12.16	40.00	30.39

Bus I.D.	Manufacturer	Status	Type	Bus Voltage (V)	Calc Isc (kA)	Equip Isc (kA)	Rating %	Calc Mom (kA)	Equip Mom (kA)	Rating %
B-LH-TX DS	Eaton	Pass	MV Switch	12470	8.94	38.00	23.53	8.99	61.00	14.74
B-CH	S&C	Pass	MV Switchgear	12470	11.03	25.00	44.12	12.28	40.00	30.70
B-CH ATS	S&C	Pass	MV Switchgear	12470	11.04	25.00	44.15	12.29	40.00	30.72
B-CH CHLR	GE	Unknown	MV Switchgear	12470	10.91	MIN REQUIRED = 16.6 KAIC		12.04	MIN REQUIRED = 25 KAIC	
B-CH-NW USB DS	Unknown	Unknown	MV Switchgear	12470	10.35	MIN REQUIRED = 16.6 KAIC		10.95	MIN REQUIRED = 25 KAIC	
B-CH-SUB 4A DS	S&C	Pass	MV Switchgear	12470	10.59	25.00	42.37	11.56	40.00	28.89
B-LE USB DS	S&C	Pass	MV Switchgear	12470	10.36	25.00	41.45	10.99	40.00	27.47
B-ML	Square D	Pass	MV Switchgear	12470	11.17	25.00	44.69	12.12	40.00	30.30
B-NH EAST	S&C	Pass	MV Switchgear	12470	9.69	25.00	38.75	9.99	40.00	24.96
B-NH WEST	S&C	Pass	MV Switchgear	12470	9.90	25.00	39.60	10.27	40.00	25.68
B-PS1-TX DS	S&C	Pass	MV Switchgear	12470	9.49	25.00	37.95	9.76	40.00	24.39
B-PS2-TX DS	Zinsco	Pass	MV Switchgear	12470	10.47	25.00	41.86	11.14	40.00	27.86
B-PSC	S&C	Pass	MV Switchgear	12470	11.57	25.00	46.30	13.03	40.00	32.57
B-SB1	S&C	Pass	MV Switchgear	12470	12.07	25.00	48.28	13.61	40.00	34.03
B-SMC	S&C	Pass	MV Switchgear	12470	10.47	25.00	41.86	11.14	40.00	27.86
B-SMC 2ND USB DS	Unknown	Unknown	MV Switchgear	12470	10.41	MIN REQUIRED = 16.6 KAIC		11.05	MIN REQUIRED = 25 KAIC	
B-SRTC-SB2	S&C	Pass	MV Switchgear	12470	12.73	25.00	50.94	15.29	40.00	38.22
B-SRTC-USB1 PUF	S&C	Pass	MV Switchgear	12470	12.65	25.00	50.60	15.84	40.00	39.61
B-SRTC-USB2 ALT	S&C	Pass	MV Switchgear	12470	12.94	25.00	51.75	15.92	40.00	39.81
B-WHP	S&C	Pass	MV Switchgear	12470	11.65	25.00	46.62	13.24	40.00	33.09
B-XSB-TX DS	S&C	Pass	MV Switchgear	12470	6.66	25.00	26.62	6.66	40.00	16.64

(*N1) System X/R higher than Test X/R, Calc Isc kA modified based on low voltage factor.

3.0 PROTECTIVE DEVICE COORDINATION STUDY

The protective device coordination study determines overcurrent protective relay and circuit breaker settings in order to provide an optimal compromise between protection and selectivity.

The coordination plots were developed using SKM System Analysis' CAPTOR software. Protective device coordination was performed in accordance with IEEE Std 242™-2001 (Buff Book). Minimum guidelines for equipment protection, as outlined in the National Electrical Code (NEC) and applicable standards of the American National Standards Institute (ANSI), were followed.

3.1 General Description and Protection Philosophy

Using the appropriate maximum fault currents, the time-current coordination curves were plotted as operating time versus current magnitudes to show protective device tripping and/or clearing characteristics and coordination among these devices.

Consideration was given to provide both selective isolation of faults and maximum protection of equipment such as cables, transformers, motors, etc.

To achieve the optimum protection and selectivity, the following guidelines were followed throughout the study:

1. Ideally, the settings of any overcurrent device should be high enough to permit the continuous full-load operating capacity of the cables and the equipment they supply, and to ride through system temporary disturbances such as in-rush current. On the other hand, the settings should be low enough to provide overload and short-circuit protection under minimum fault conditions.
2. Considering any two protective devices in series:
 - The maximum available fault current at the downstream device determines the upper limit of the coordination range between these two devices.
 - The minimum available fault current at the downstream device or the pick-up setting of the upstream device determines the lower limit of the coordination range.
 - Series instantaneous devices do not coordinate unless there is sufficient impedance between the two devices.
 - When plotting coordination curves, certain time intervals must be maintained between the curves in order to ensure correct selectivity. These time intervals vary, depending on the device types. In general, however, the following must be taken into consideration when determining the appropriate time separation interval: Breaker clearing

time, relay tolerances, induction disk over-travel, and a reasonable safety margin for error.

3.2 Codes and Standards

The minimum protection requirements as outlined in the National Electric Code (NEC), ANSI, and IEEE Standards were used as guidelines for protective device settings.

Applicable requirements are summarized below.

1. Cables

Power cables require overload and short-circuit protection in order to meet the requirements stated in NEC-2011, Article 240, and IEEE Std 242-2001 (Buff Book). NEC further requires that the ampacity of low voltage cable (0-2000 Volts) be determined by NEC-2011, Article 310.15. Cable de-rating based upon ambient temperature and the number of current carrying conductors in a raceway must also be applied. Medium voltage cable (2001-35,000 Volts) ampacity is defined by NEC-2011, Article 240.100(A) and NEC-2011, Article 310.60.

2. Transformers

A transformer is recommended to have protective devices on both primary and secondary side in order to meet the basic protection requirements for overloads and short-circuit withstand values. However, a transformer is permitted to be protected by only a primary side device if it meets the exceptions listed in NEC-2011, Article 240.4(F). In addition, the transformer protective devices must be able to withstand magnetizing inrush currents without tripping.

NEC protection requirements for transformers: Overcurrent devices are selected, and settings are recommended to provide overcurrent protection in accordance with NEC-2011, Article 450.3. Paragraph (A) specifies that transformers over 600 V comply with Table 450.3(A). Paragraph (B) specifies that transformers less than 600 V comply with Table 450.3(B). These tables provide guidance for sizing of primary and secondary overcurrent protective devices based on transformer full load ampere ratings, transformer impedance, and transformer location.

Short-circuit thermal limits for transformers: The primary devices should be set on the basis that the transformers have short-circuit withstand capabilities as defined by IEEE Std C57.109TM-1993.

3. Motors

The motors should have appropriate protective devices to meet the basic protection requirements for overloads and fault current withstand values. In addition, the motor short-circuit and ground fault protective devices should be set to ride through motor starting current.

3.3 Coordination Objectives

Review the existing system overcurrent protection and coordination. Provide suggestions for improvement.

3.4 Coordination Results

The system coordination began at the main 12.47 kV SRTC switchgear and continued downstream through the West Campus Loop to the largest feeder breaker at each 480 V or 208 V service entrance disconnect within each West Campus Loop building. These buildings include the Science Research and Teaching Center, Science Building 1, West Heating Plant, Peter Stott Center, Millar Library, Cramer Hall, Smith Memorial Center, Library East, University Services Building, Neuberger Hall, Parking Structure 1, Lincoln Hall, and the Extended Studies Building.

As shown on the time-current plots, each device curve is tagged with an arrow and label referencing its location on the plot's individual representative one-line diagram. This label also references the device to its' specific manufacturer information, including ratings and settings, as indicated in the text box on each plot. The device time-current characteristics are truncated at maximum through-fault current for a downstream fault.

Efforts were made to provide the best coordination possible with the protective devices supplied under this contract. Areas where breaker trip curves overlap indicate areas of possible non-selective breaker operation. Where possible, efforts were made to reduce non-selective breaker operation while maintaining adequate system protection. In some cases, because of device limitations, little can be done to improve device selectivity. Such device limitations include the fixed operating characteristic of a fuse, the built-in instantaneous or instantaneous "over-ride" elements of molded case circuit breakers, and the limited instantaneous trip range of trip units with an instantaneous trip function.

In cases involving redundant protective devices, non-selective breaker operation is of little or no concern. Protective devices are redundant if, regardless of which device opens, the same system outage occurs. Often, in order to improve overall system protection and coordination, redundant devices are intentionally set to overlap (i.e. non-selectively coordinate with) one another.

Adequate coordination is achieved using the recommended protective devices, with settings and ratings as listed in Section 4. The recommended adjustments would maximize coordination in an attempt to allow the various downstream devices to isolate faults without operation of the upstream devices. Although instantaneous trip devices provide the highest degree of protection, when applied in series they compromise selectivity at high-magnitude fault currents.

3.5 Coordination Recommendations

All of the adjustable low voltage electronic trip and thermal magnetic circuit breakers and medium voltage equipment should be tested and adjusted according to the recommended settings given in Section 4.

If the largest feeder breaker in a service entrance disconnect was adjustable, the as-found settings were used to plot the coordination curve. It is not possible to ensure these breakers are properly set without expanding the scope of this study to downstream locations. Therefore, no settings are recommended for these locations.

3.6 Time-Current Characteristic Plots

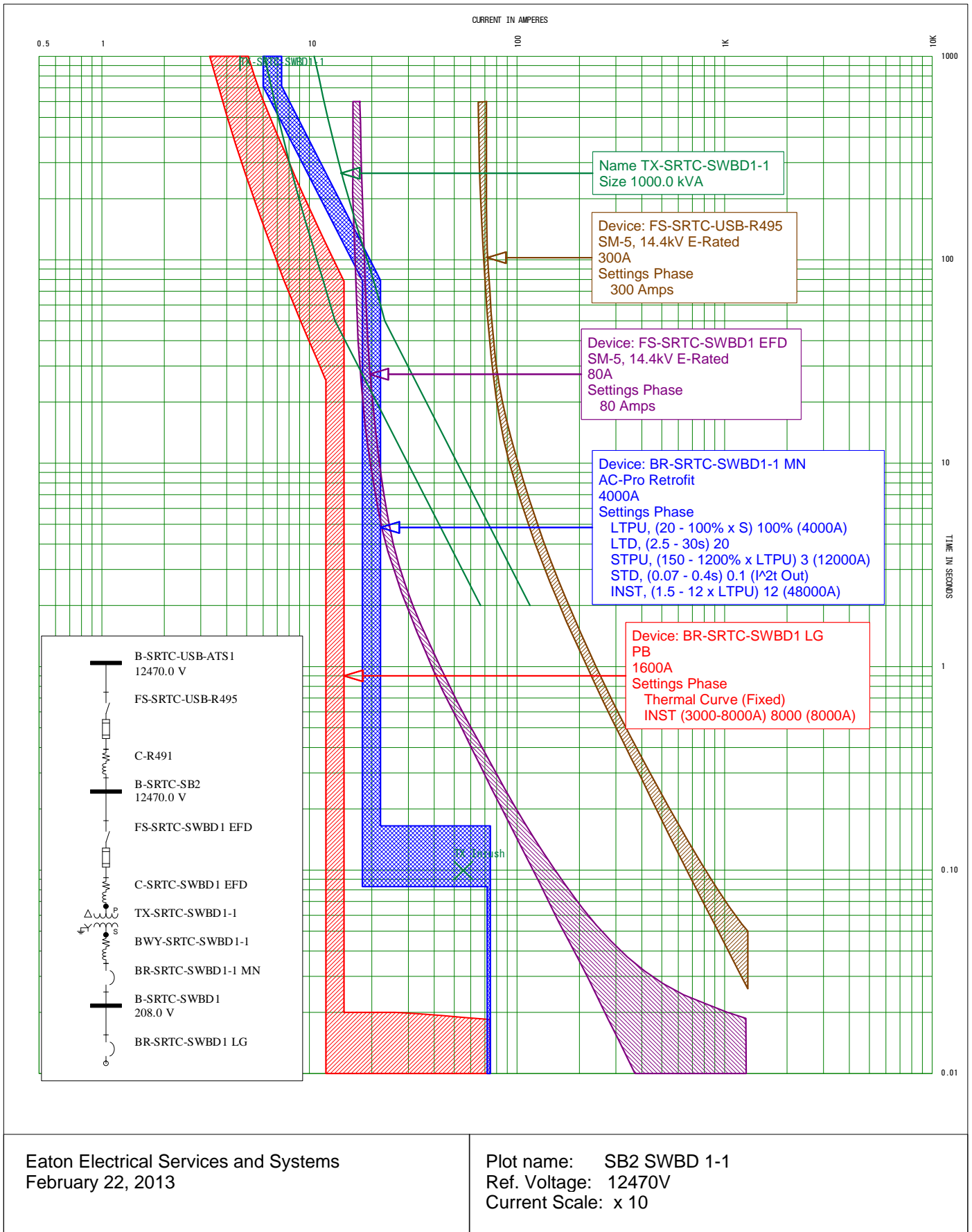
Refer to the following pages for the plotted coordination curves, which graphically indicate the degree of selectivity and protection obtained.

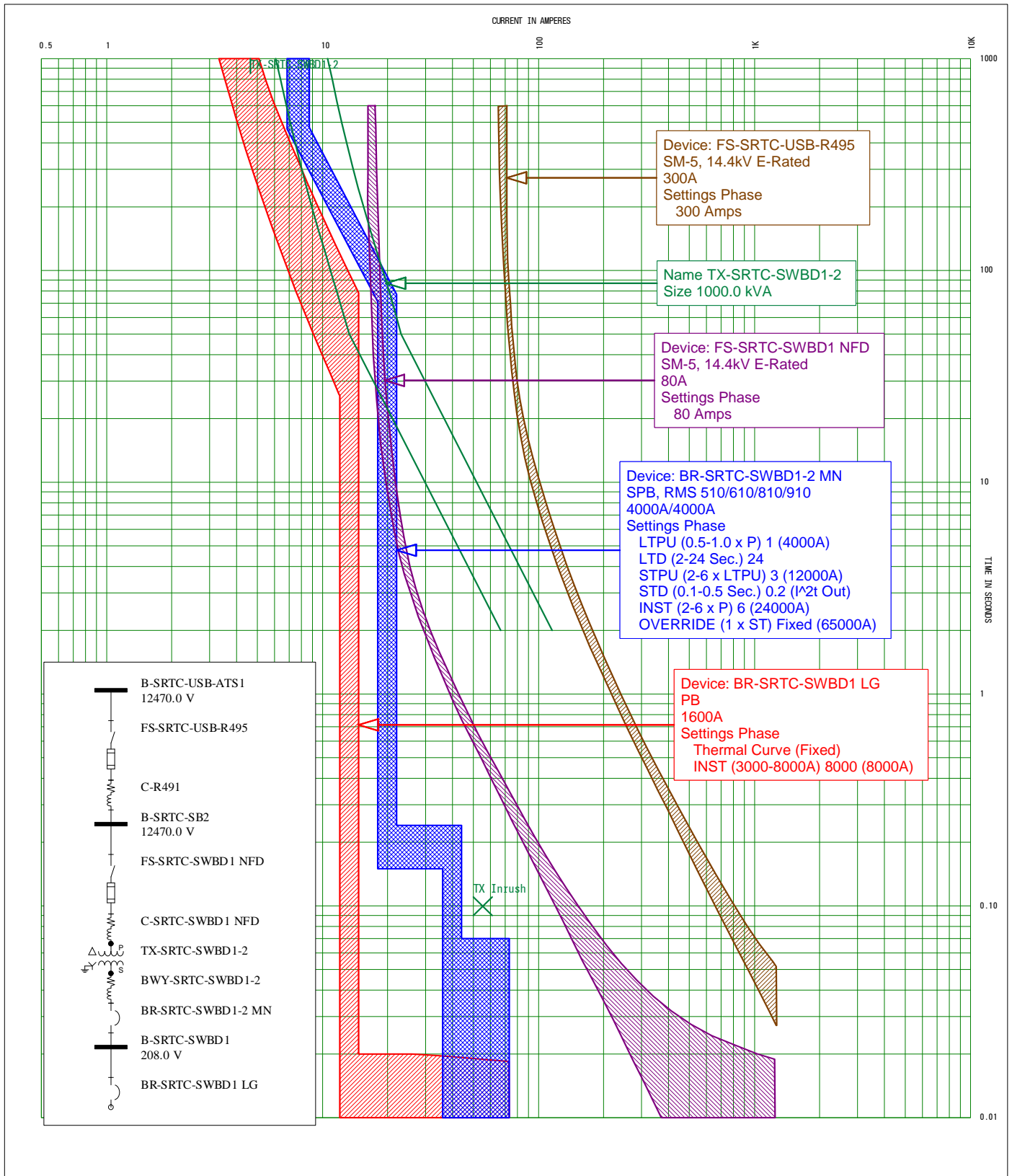
In some cases, a single time-current curve may be applicable to several locations in the system, where each location utilizes substantially similar devices, and serves similar loads.

The following list references the attached time-current curves for this report.

Table 3.1 – TCC Plots Index

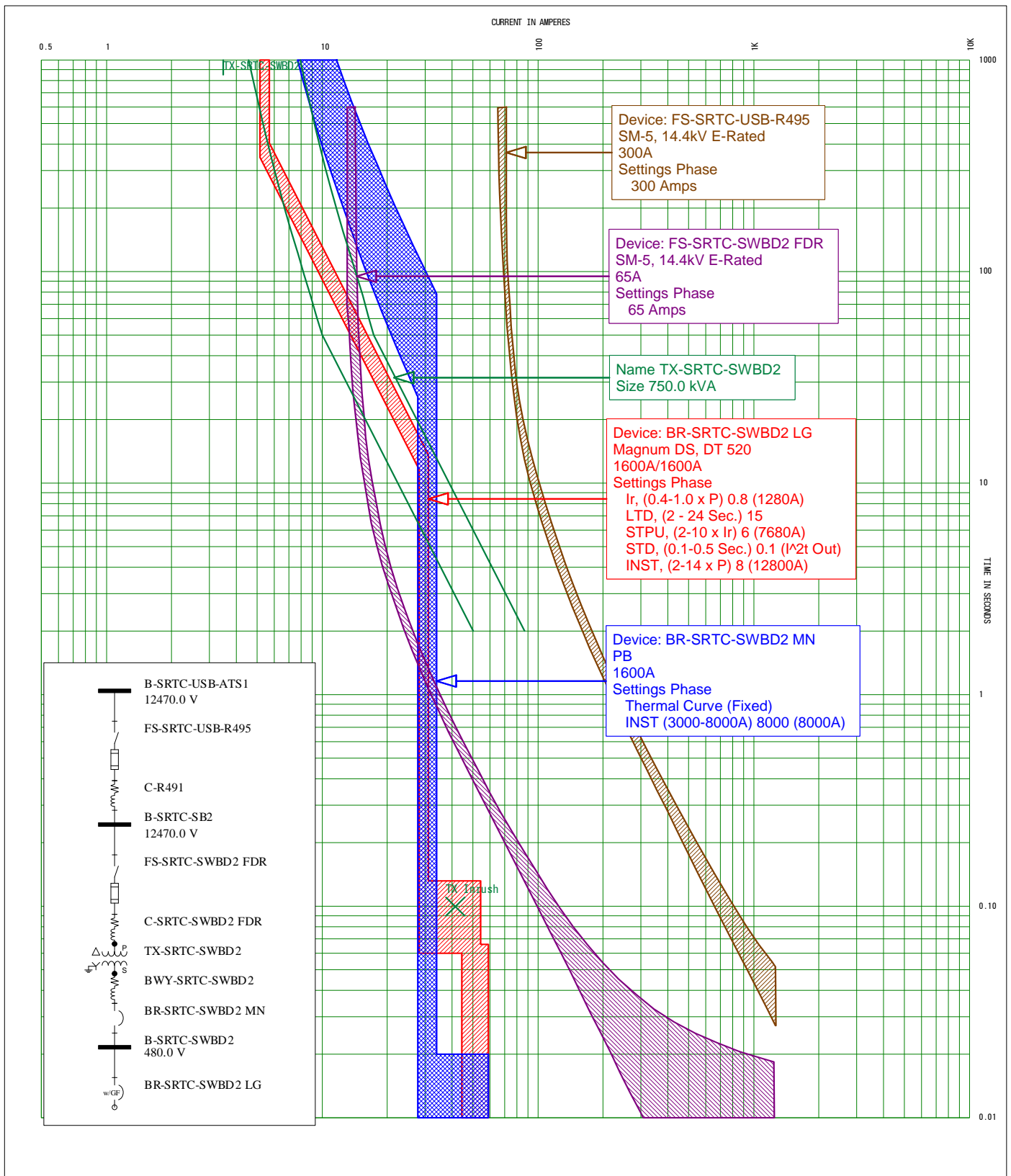
SB2 SWBD 1-1	Page 3-5
SB2 SWBD 1-2	Page 3-6
SB2 SWBD2	Page 3-7
SB2 SWBD3	Page 3-8
LH USB	Page 3-9
CH SE USB	Page 3-10
CH EMER USB	Page 3-11
LIB EAST	Page 3-12
SMC 2ND ADD	Page 3-13
NH E USB	Page 3-14
NH W USB	Page 3-15
PARK#1	Page 3-16
CH PNL B	Page 3-17
SB1 SWBD	Page 3-18
XSB USB	Page 3-19
WHP USB	Page 3-20
ML USB	Page 3-21





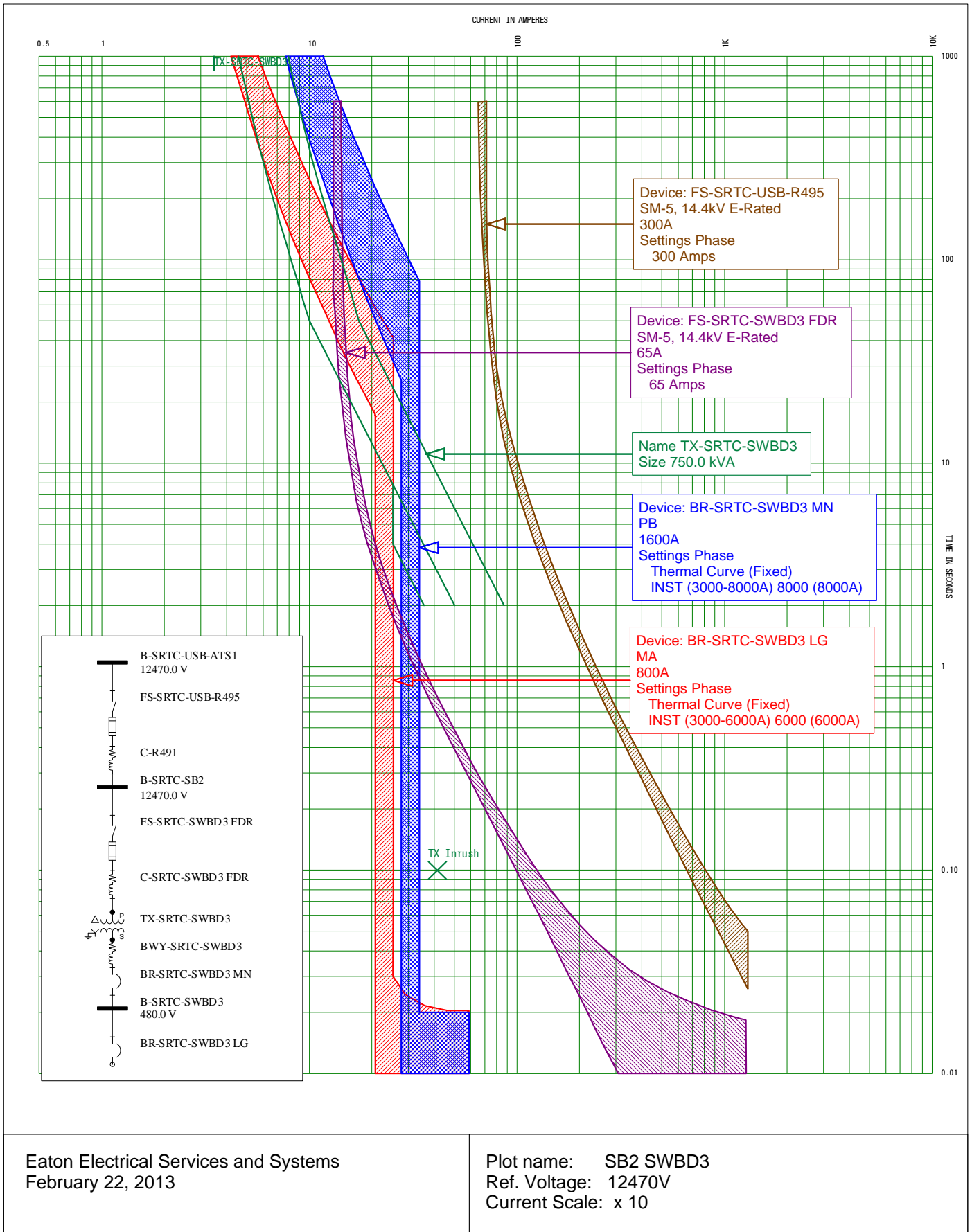
Eaton Electrical Services and Systems
February 22, 2013

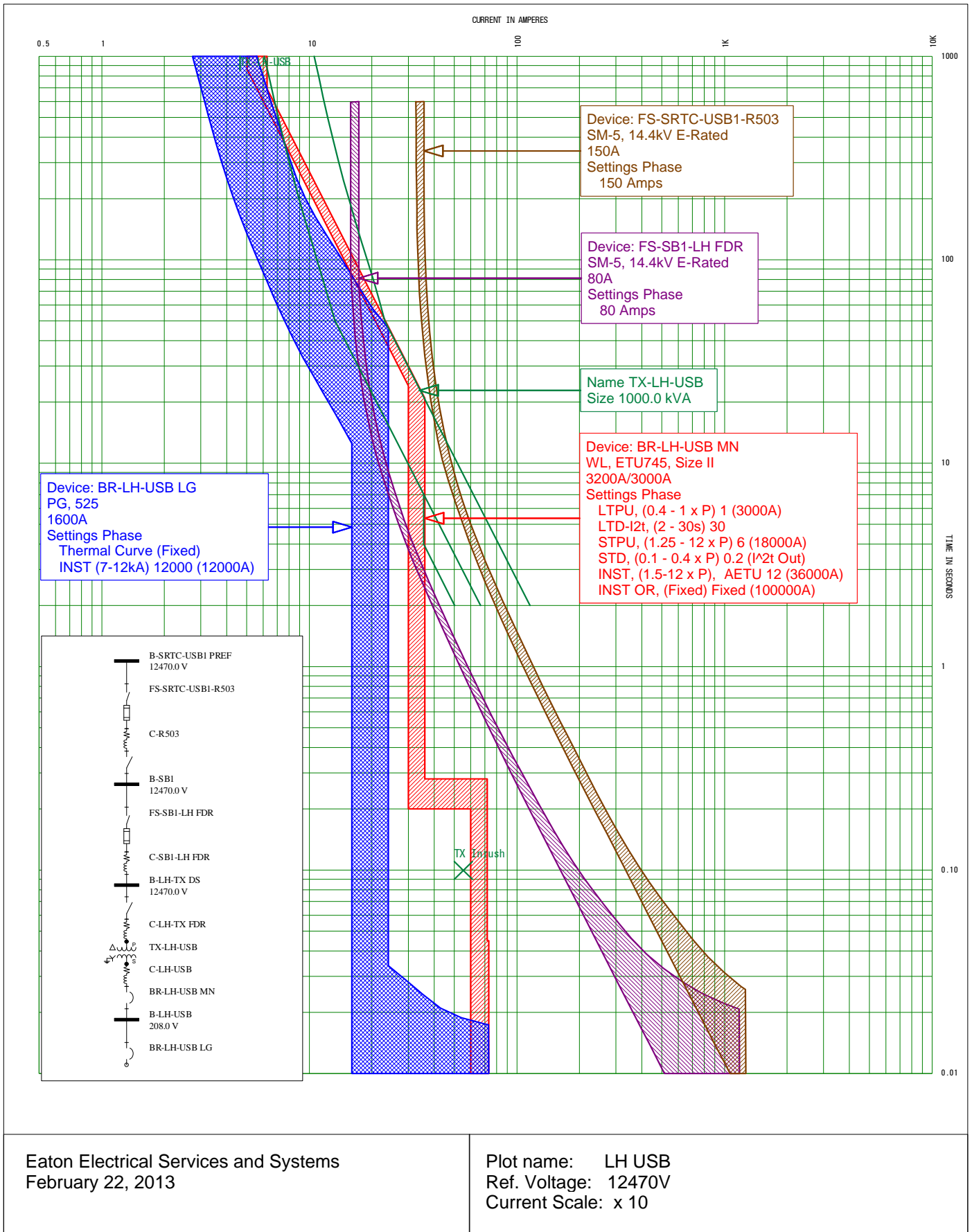
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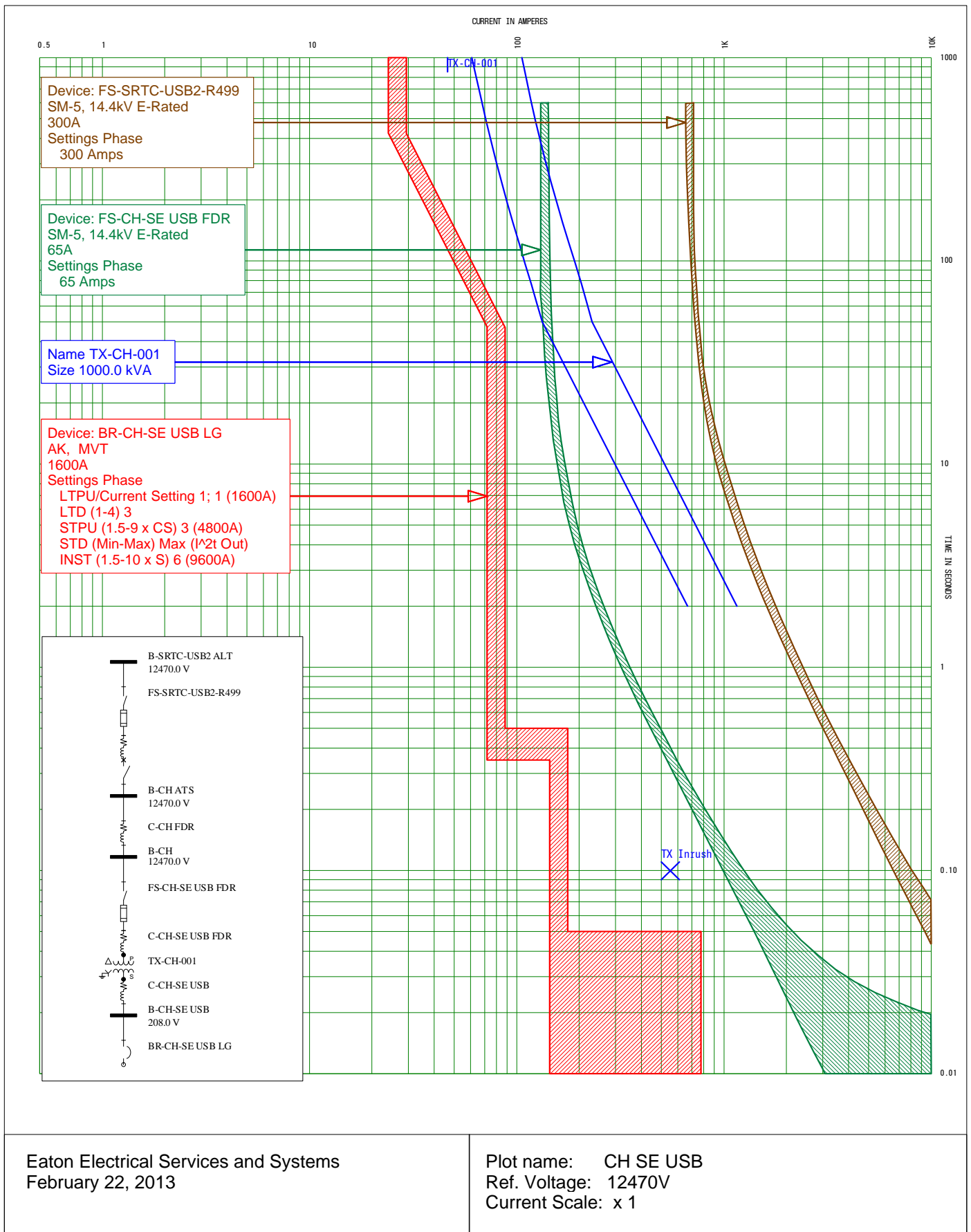


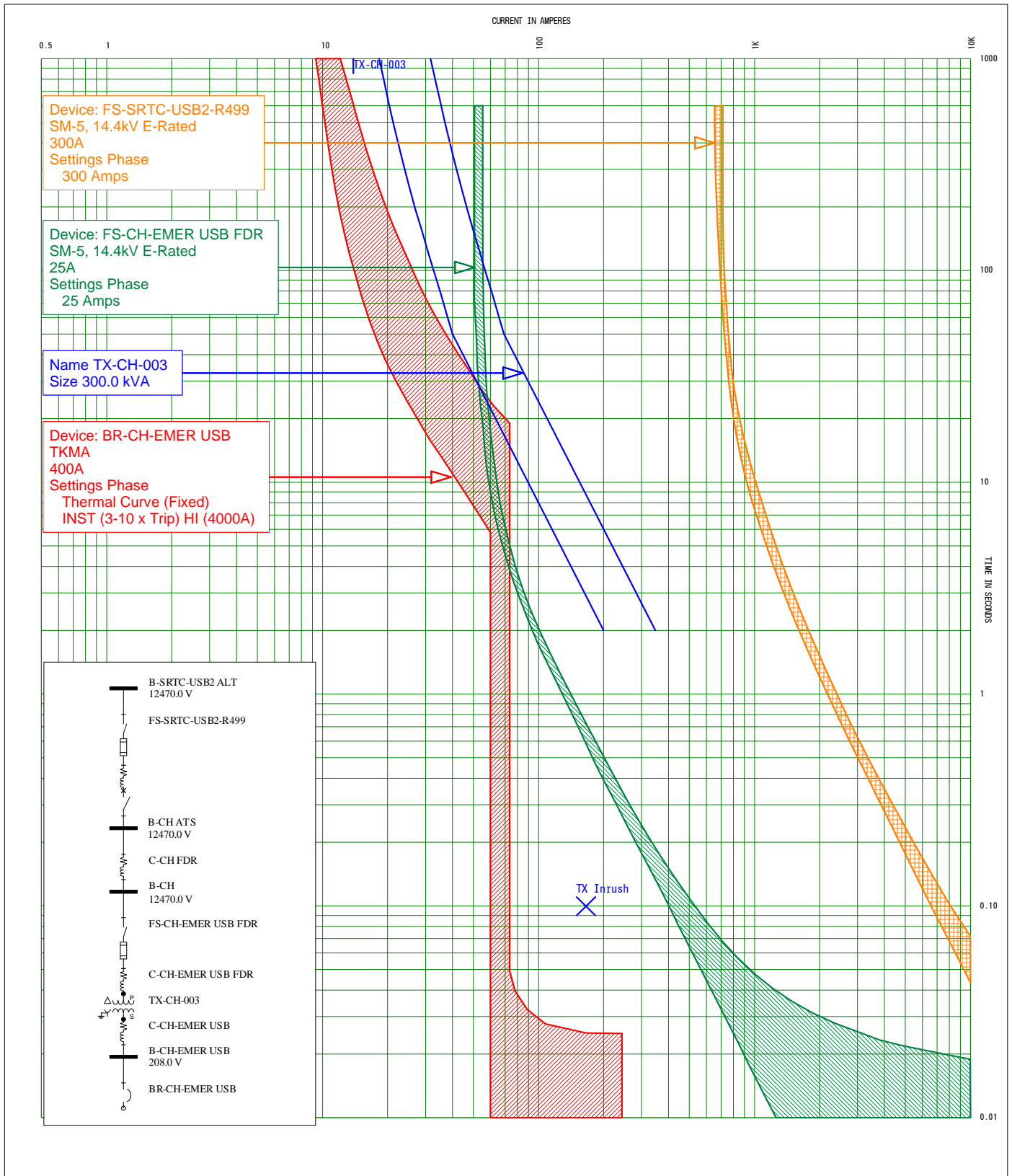
Eaton Electrical Services and Systems
February 22, 2013

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Current Scale: x 10



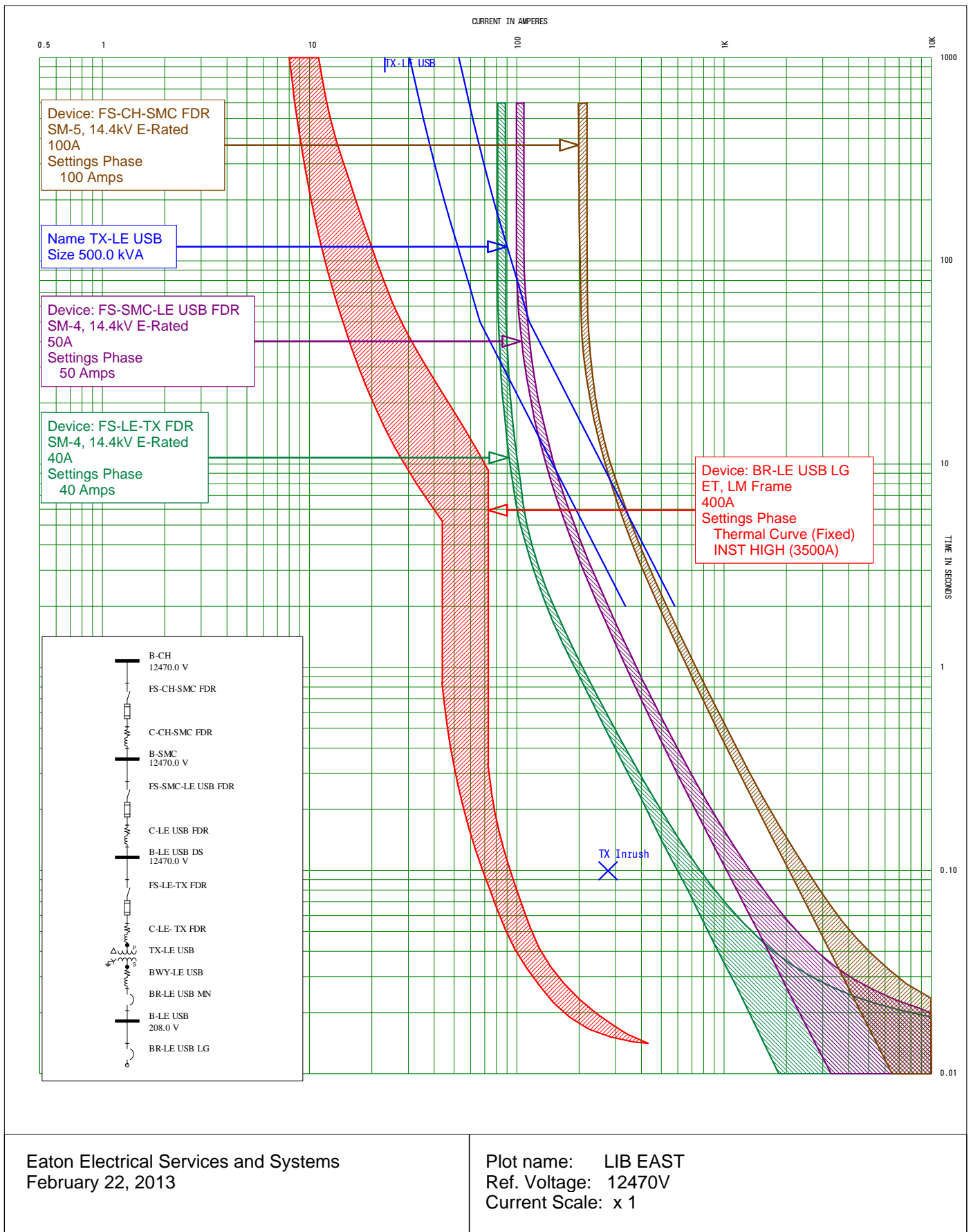


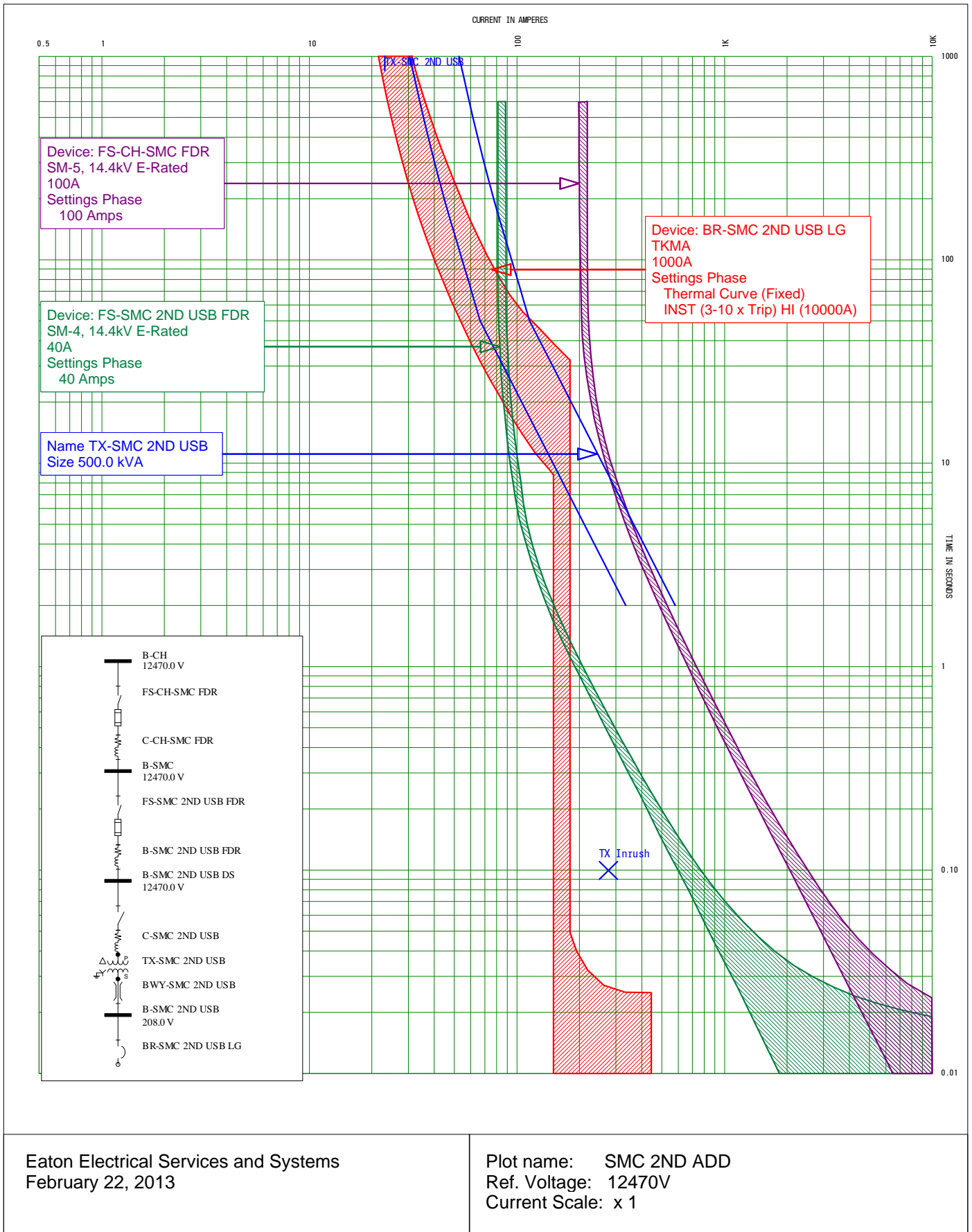


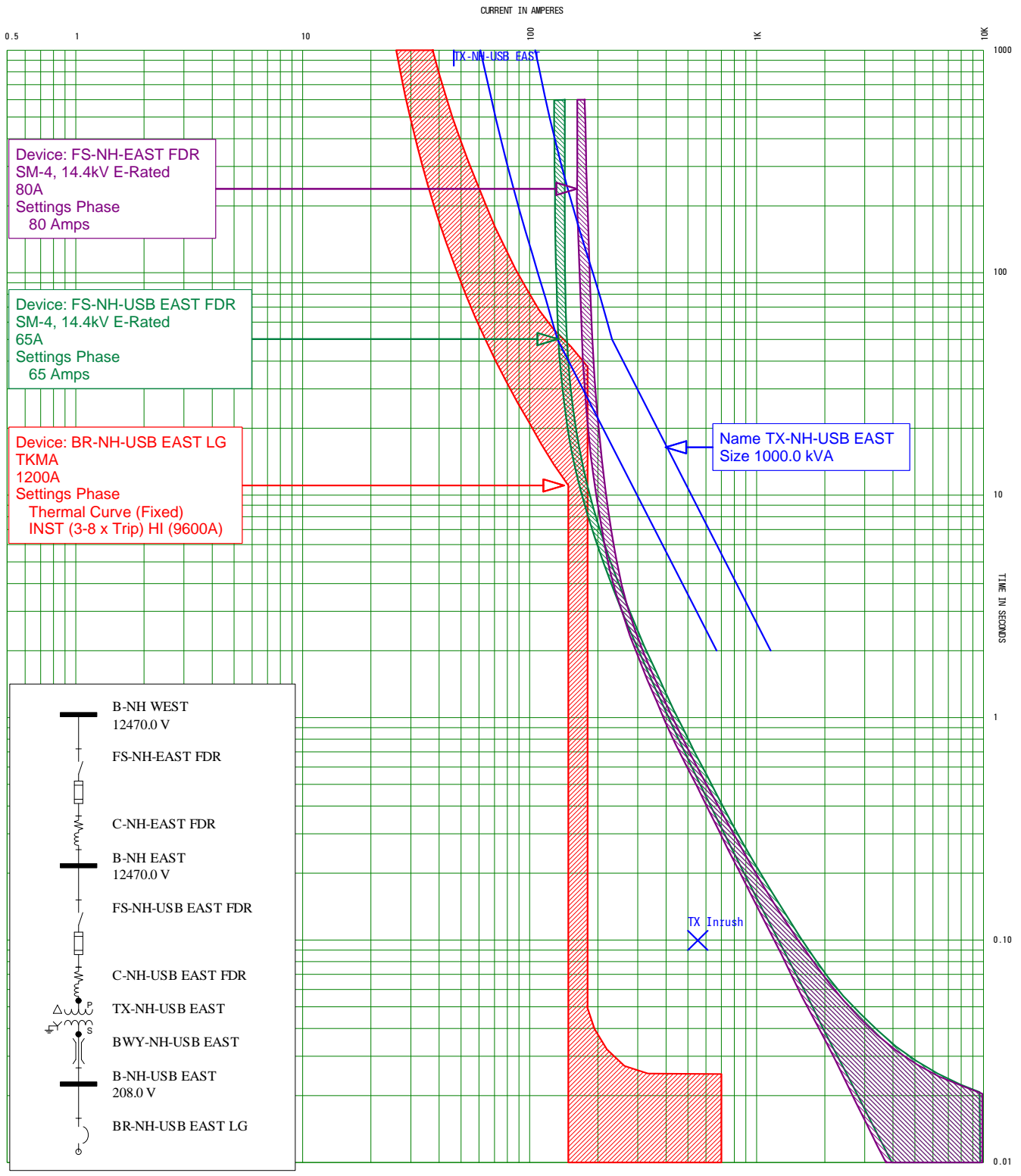


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February 22, 2013

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Current Scale: x 1

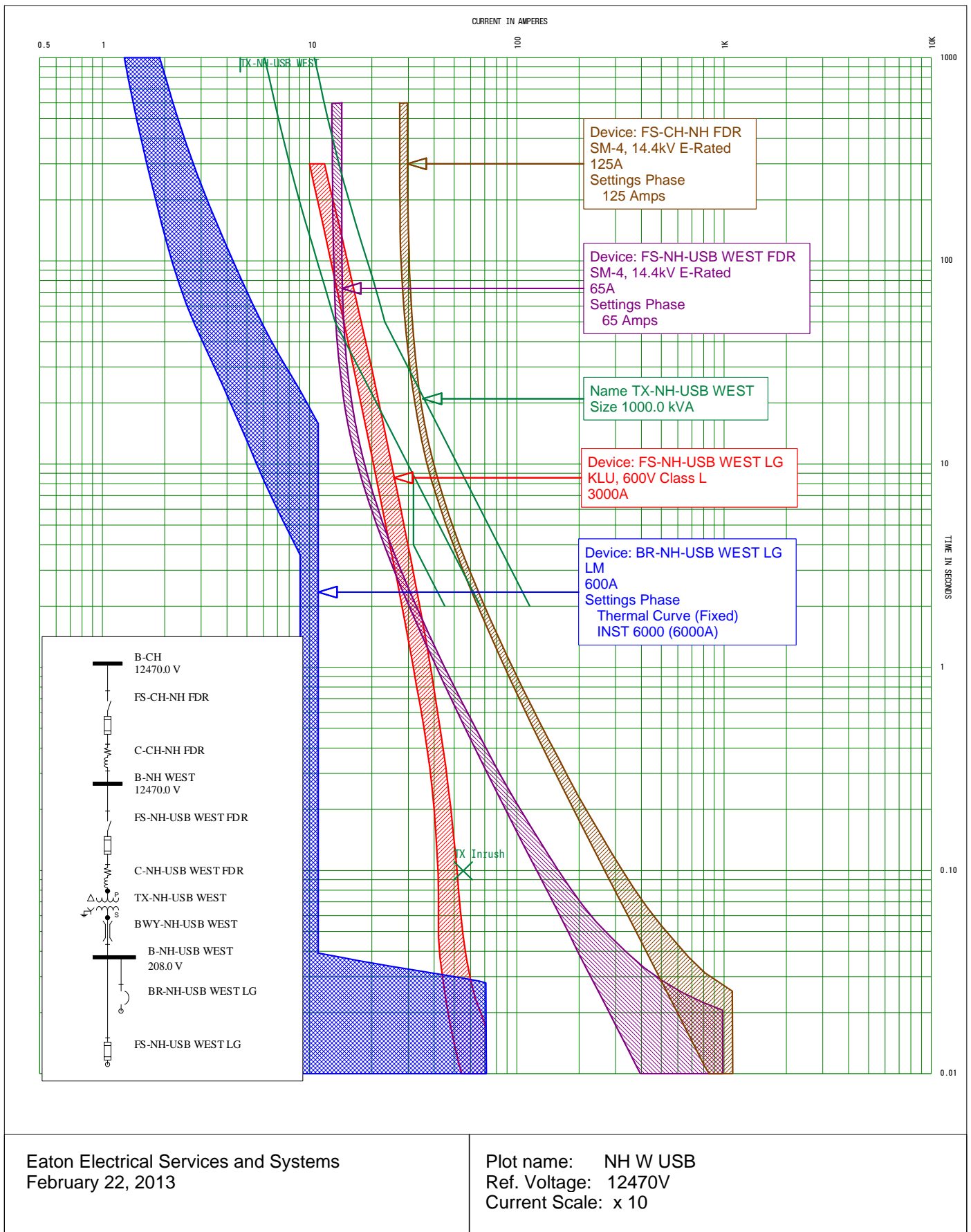


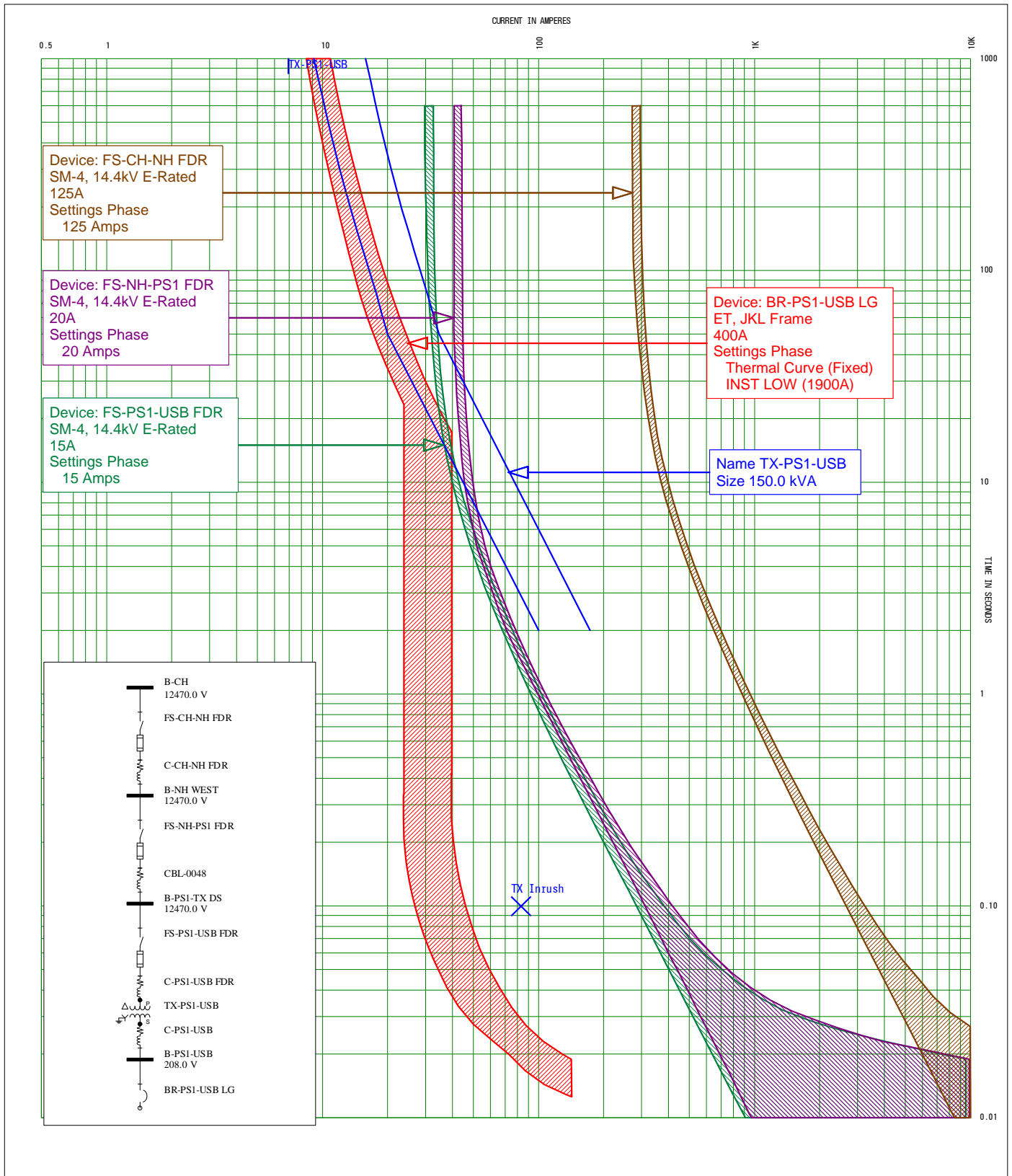




Eaton Electrical Services and Systems
February 22, 2013

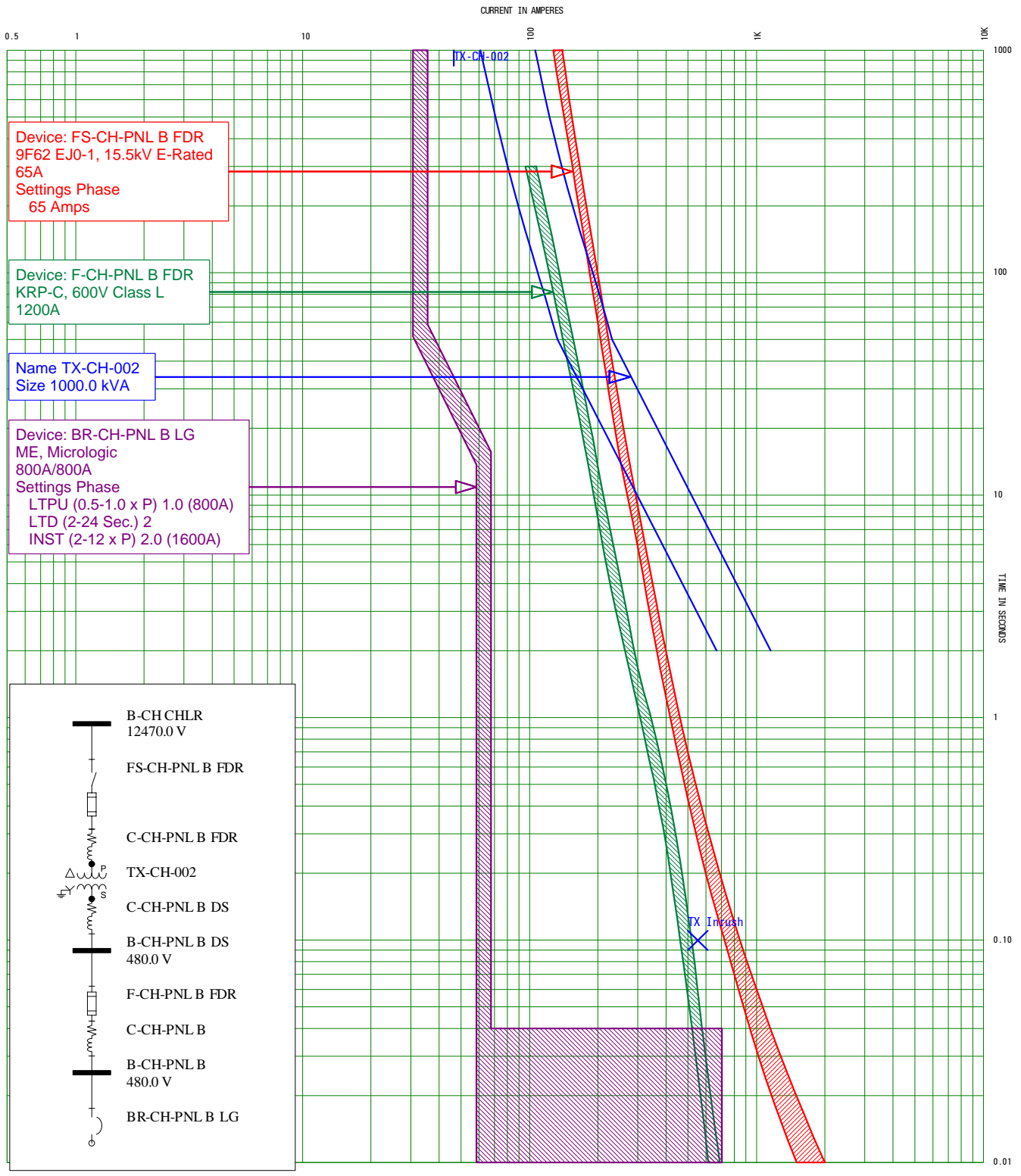
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Current Scale: x 1





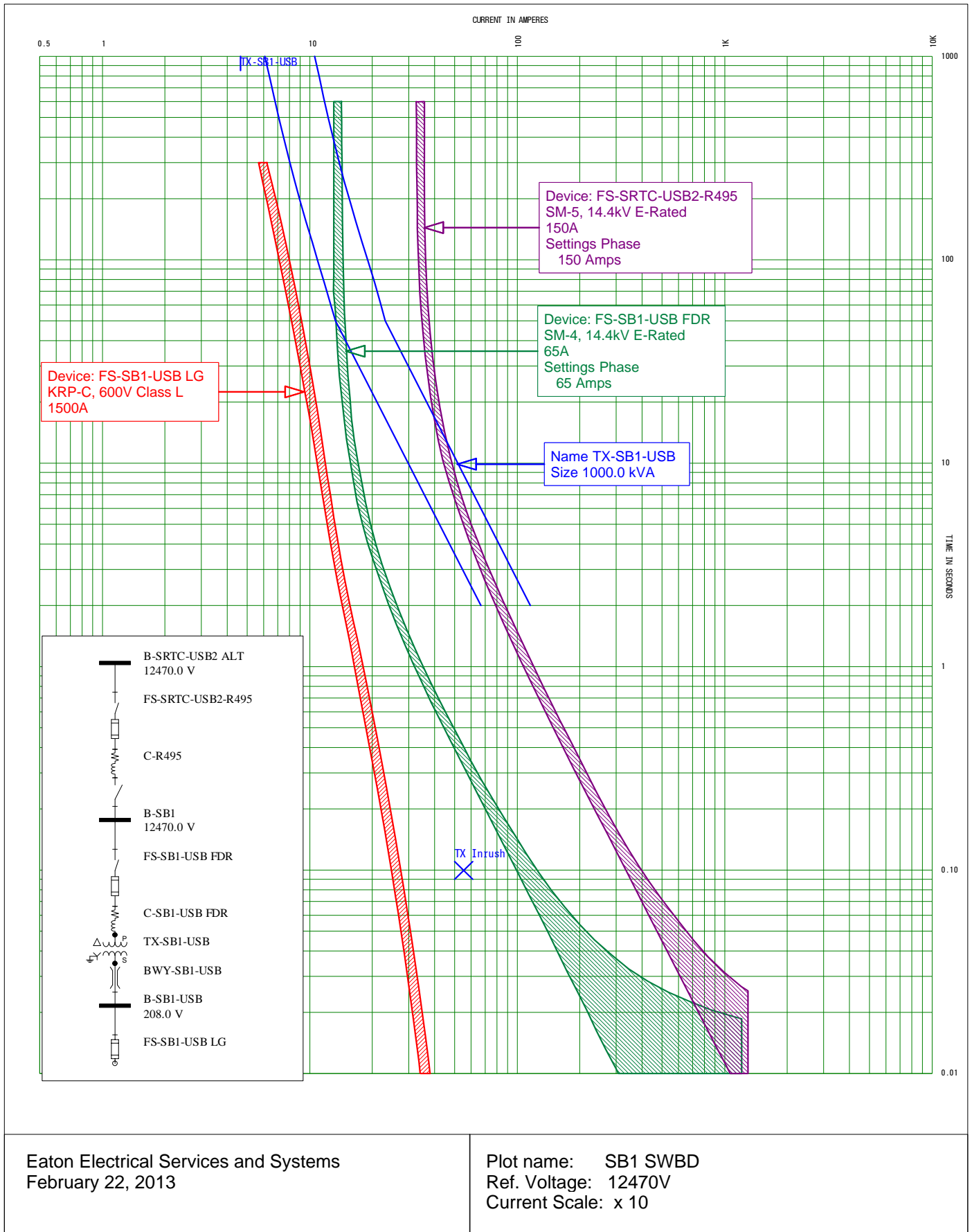
Eaton Electrical Services and Systems
February 22, 2013

Plot name: PARK#1
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Current Scale: x 1



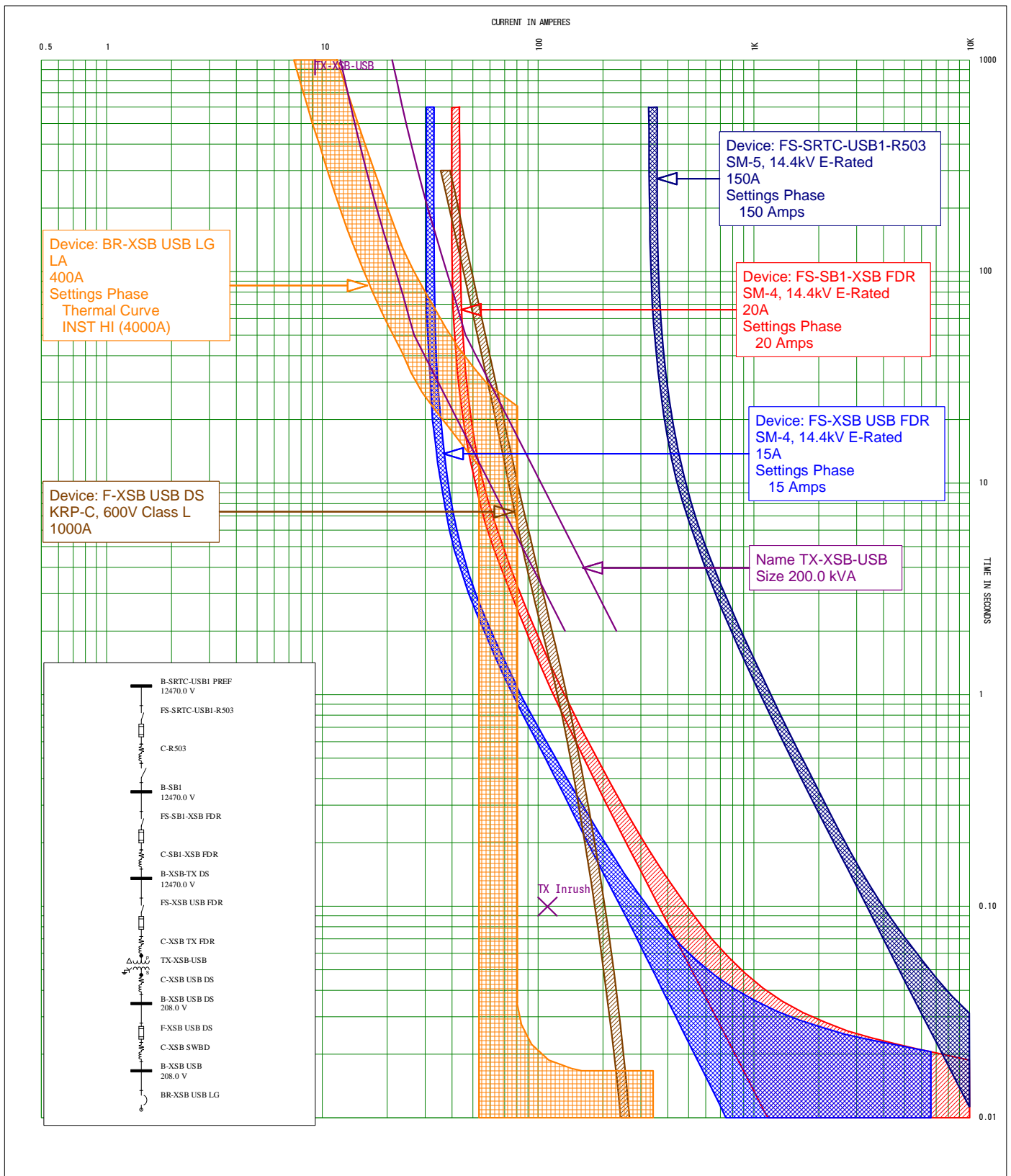
Eaton Electrical Services and Systems
February 22, 2013

Plot name: CH PNL B
Ref. Voltage: 12470V
Current Scale: x 1



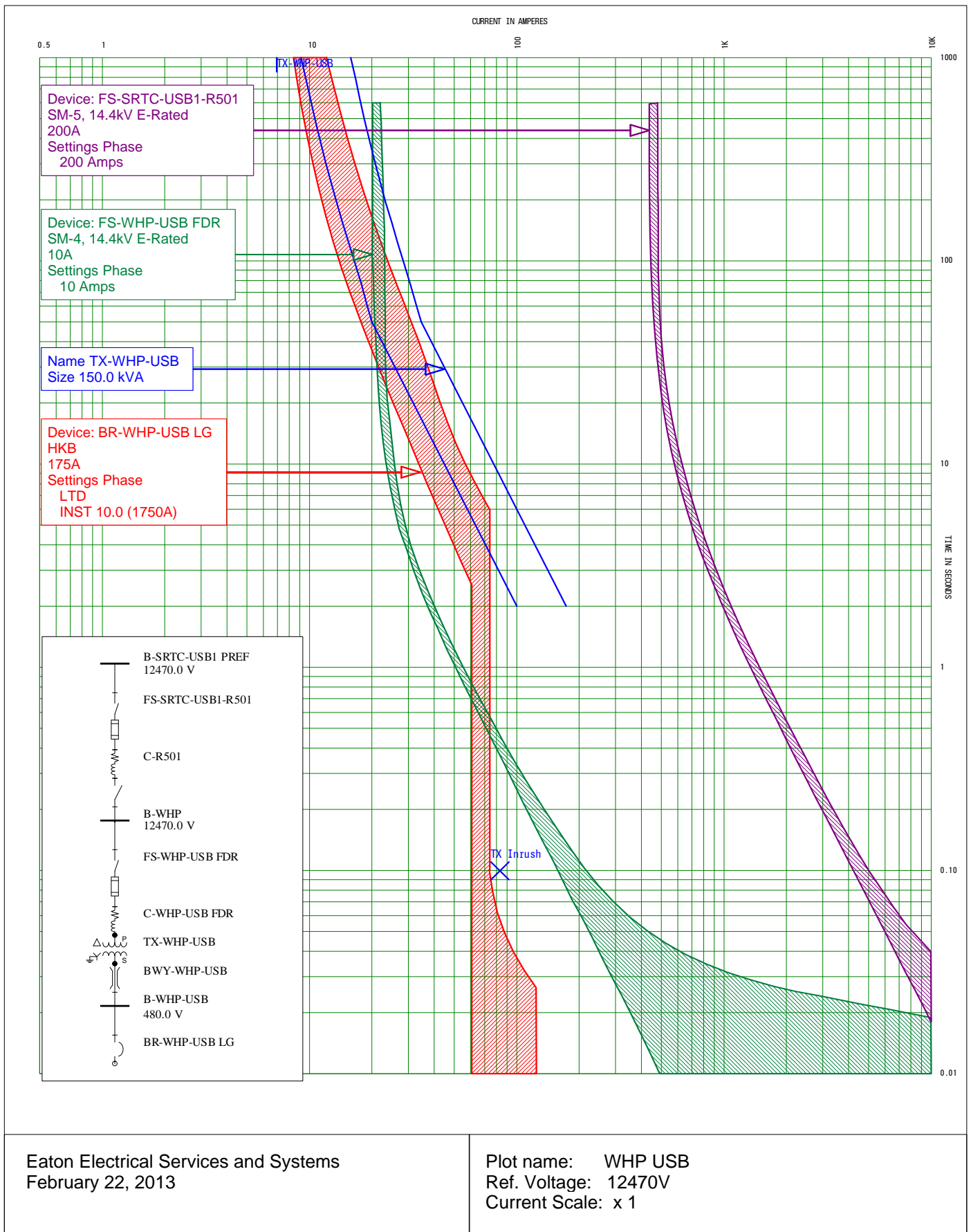
Eaton Electrical Services and Systems
February 22, 2013

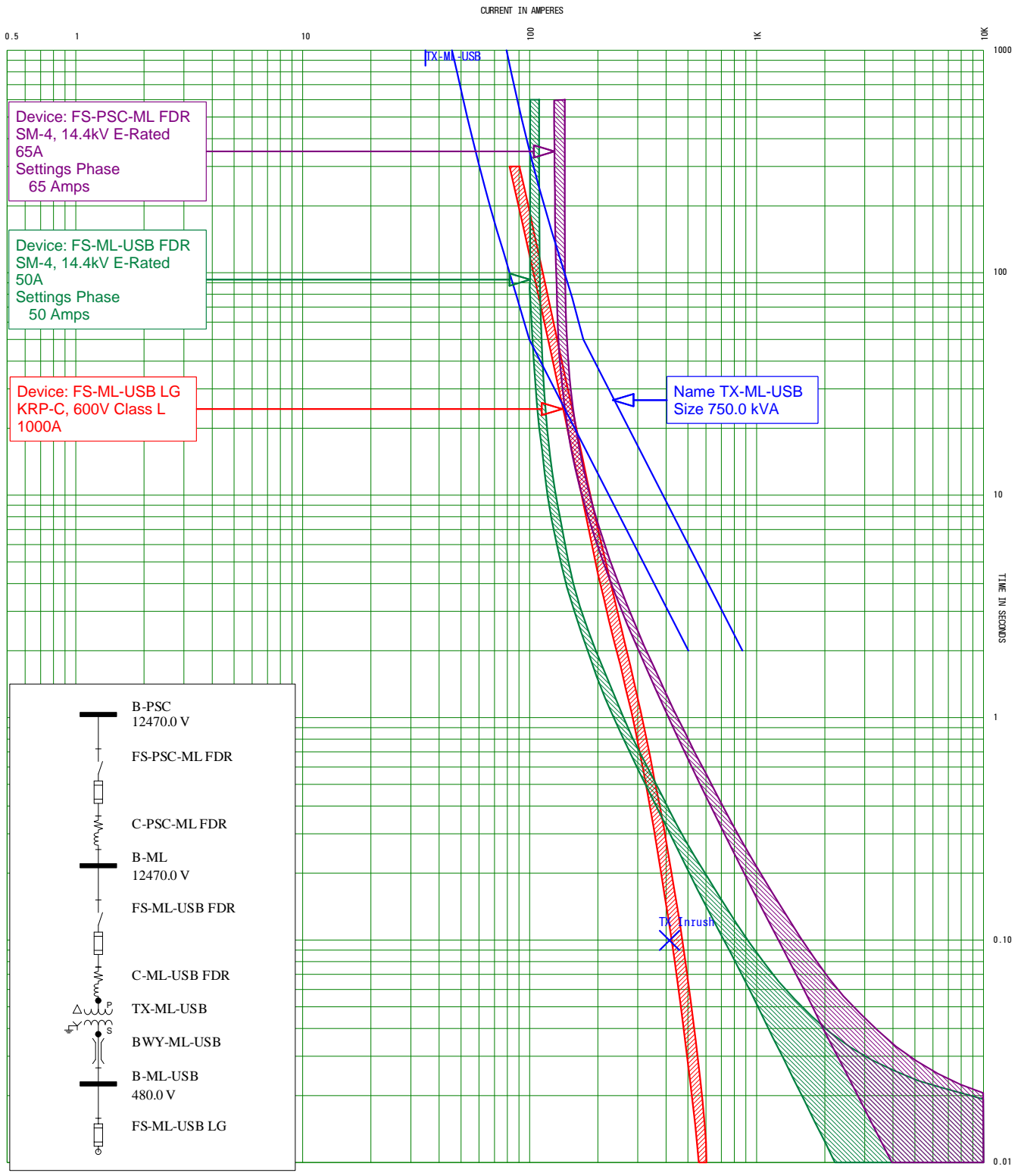
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Ref. Voltage: 12470V
Current Scale: x 10



Eaton Electrical Services and Systems
February 22, 2013

Plot name: XSB USB
Ref. Voltage: 12470V
Current Scale: x 1





Eaton Electrical Services and Systems
February 22, 2013

Plot name: ML USB
Ref. Voltage: 12470V
Current Scale: x 1

4.0 RECOMMENDED PROTECTIVE DEVICE SETTINGS

The following table shows a comprehensive summary of the recommended settings for the adjustable protective devices. The devices are grouped by system bus name/location. Refer to Appendix D for the system one-line diagram.

Table 4.1 - Recommended Low-Voltage Protective Device Settings

BUS NUMBER	FEEDER BREAKER ID	BREAKER MODEL & MANUFACTURER	TRIP UNIT TYPE	CURRENT RATING		LONG DELAY		SHORT DELAY			INST.	GROUND		CURVE NAME
				FRAME	PLUG	PICKUP	TIME	PICKUP	TIME	I ² t		PICKUP	TIME, I ² t	
B-SRTC-SWBD1	BR-SRTC-SWBD1-1 MN Main Breaker	Westinghouse DB100	AC-PRO Retrofit	4000A	4000A	1	20	3	0.1	Out	12	---	---	SB2 SWBD 1-1
B-SRTC-SWBD1	BR-SRTC-SWBD1-2 MN Main Breaker	Westinghouse DB100	RMS 510 LSI	4000A	4000A	1 (1)	24 (2)	3 (2.5)	0.2 (0.2)	Out (Out)	6 (4)	---	---	SB2 SWBD 1-2
B-SRTC-SWBD2	BR-SRTC-SWBD2 MN Main Breaker	Westinghouse PB	T/M	2500A	1600A	---	---	---	---	---	HI (LO)	---	---	SB2 SWBD2
B-SRTC-SWBD3	BR-SRTC-SWBD3 MN Main Breaker	Westinghouse PB	T/M	2500A	1600A	---	---	---	---	---	HI (HI)	---	---	SB2 SWBD3
B-LH-USB	BR-LH-USB MN Main Breaker	Siemens WL	ETU745 LSI	3000A	3000A	1 (1)	30 (30)	6 (3)	0.2 (0.2)	Out (Out)	12 (6)	---	---	LH USB

*Note: If available, as-found settings are shown in parentheses

5.0 ARC FLASH HAZARD ANALYSIS

This section of the report contains the interpretation for the arc flash hazard analysis. The calculations made in this arc flash hazard analysis conform to NFPA 70E, and are based on the information provided by the customer. Actual heat and radiation exposure may be more or less than reflected in the analysis.

Only qualified electricians who are familiar with the installation and maintenance of electrical distribution equipment should perform work associated with such products. All recommendations of the manufacturer, warnings and cautions relating to the safety of personnel and equipment should be followed. All applicable health and safety laws, codes, standards, and procedures should be adhered to. All equipment should be de-energized prior to any maintenance or service. OSHA 1910.333 requirements should be adhered to. All guidelines of NFPA 70E-2012 should be followed, and in particular appropriate personal protective equipment must be provided and worn.

Eaton Corporation will not be responsible for the misuse or misapplication of the information contained in this analysis. Those providing service for electrical equipment should contact an Eaton Electrical Services and Systems representative, or other qualified individual, if any questions arise.

5.1 Introduction

NFPA 70E-2012, Article 110.3(F) requires that an employer developed electrical safety program includes a hazard identification and risk evaluation procedure. This procedure is meant to be used before performing work on or near any equipment at or above 50 volts or any time work is being performed where an electrical hazard exists. This analysis presents only the results of an incident energy evaluation conducted in accordance with 130.5(B). The risk depends on a number of factors. These include the nature of the task being performed and the condition of the equipment. Selection of personal protective equipment (PPE) must be made based on the incident energy level that is presented in this report and a risk assessment to be made by the qualified person. NFPA 70E-2012, Article 130.7(A) requires that employees use and employers provide proper PPE for the tasks being performed. NFPA 70E-2012, Table H.3(b) provides guidance for the selection of PPE based on calculated incident energy exposure.

NFPA 70E-2012 and IEEE Std 1584-2002 provide equations and methods to accurately calculate the arc flash boundary and incident energy at specific locations within a facility's electrical system. Any location where work may be performed on or near energized electrical conductors and circuit parts is subject to the arc flash standards. PPE used to guard against arc flash hazard should be considered the last line of defense. It is also important to note that the use of PPE is not intended to prevent all injuries from an arc flash. The goal of determining PPE levels using the arc flash hazard

approach is to identify the level of protection required to limit the injury to the onset of a second degree burn in the event of an arc flash while avoiding the use of more protection than is needed so as to minimize hazards of heat stress, reduced visibility and limited body movement.

Although the arc flash calculation procedure is based upon NFPA 70E and IEEE Std 1584-2002 equations and methods, it is a relatively new approach to determining the degree of required PPE. The calculations are derived from theory and research involving arc current incident energy measurements conducted under a specific set of controlled test conditions. Therefore, calculation results may be more severe or less severe than the hazard presented by an actual arc flash exposure. Also, the arc flash hazard calculations do not take into account hazards associated with the splattering of molten metal, explosively propelled pieces of equipment and air pressure shock waves.

The results of this arc flash hazard analysis are not intended to imply that personnel be permitted to work on exposed energized equipment or circuits. OSHA 1910.333 restricts the situations in which work is to be performed near or on energized equipment or circuits by stating, "Live parts to which an employee may be exposed shall be deenergized before the employee works on or near them, unless the employer can demonstrate that deenergizing introduces additional or increased hazards or is infeasible due to equipment design or operational limitations."

Even if work is not being performed directly on energized equipment, it is important that the proper PPE be used during some load interruption actions, during visual verification of the state of disconnecting devices, and during lockout/tagout procedures.

5.2 Study Procedure

In accordance with NFPA 70E and IEEE Std 1584-2002, SKM Systems Analysis software provides the calculation of these values. The equations used in these calculations are based on actual test values. These tests measured the calories per square centimeter (cal/cm^2) radiating from a simulated arcing fault. The measurements were performed at a theorized working distance of 18 inches.

The intent of NFPA 70E and IEEE Std 1584-2002 guidelines is to establish standard calculations to determine an approach boundary that will prevent the onset of a second-degree burn to the face and the torso of the worker. An incident energy of $1.2 \text{ cal}/\text{cm}^2$ represents the onset of a second-degree burn.

NFPA 70E-2012, Article 130.7(A), Informational Note 3, states that greater consideration must be given to the decision to work within the limited approach boundary of energized electrical equipment when the incident energy exceeds $40 \text{ cal}/\text{cm}^2$. Locations with a calculated incident energy that exceeds $40 \text{ cal}/\text{cm}^2$ are shown in Table 5.2.

The arc flash analysis considers each medium and low voltage system location within the scope of the work. IEEE Std 1584-2002 states that equipment below 240 V need not be considered unless it involves at least one 125 kVA or larger low-impedance transformer in its immediate power supply. Therefore, no detailed calculations will be performed for 120/208 V locations supplied by a transformer smaller than 125 kVA, however labels will be provided for these locations.

Before the arc flash equations can be applied, a comprehensive short-circuit and protective device coordination study must be completed to include all locations where work may be performed on or near energized components; e.g. motor control centers and power distribution panels. Since the short-circuit current must be calculated at every pertinent location and the clearing time of each location's upstream protective device is required, the arc flash circuit model is more detailed and extends deeper into the facility electrical distribution system than is typical of a basic short-circuit and protective device coordination study. Accurate fault currents and device clearing times are extremely important in deriving reliable results. A conservative (high) fault current value could yield a faster clearing time of a protective device, depending upon its curve shape, and the calculated incident energy may actually be less than the incident energy calculated for a lower magnitude of fault current and a longer clearing time.

1. Arc Flash Scenarios

Since the greatest arc flash hazards may not result from the highest fault current, multiple scenarios must be analyzed and compared. The following modes of operation have been evaluated in order to determine the worst-case incident energy at each location in the system. It is important to determine the available short-circuit current for modes of operation that provide both the maximum and minimum available short-circuit currents.

- Arc Flash Scenario 1 – System supplied from the preferred utility source. B-SRTC-SWBD 1 supplied from the Normal Feed.
- Arc Flash Scenario 2 – System supplied from the preferred utility source with the assumed minimum fault current. B-SRTC-SWBD 1 supplied from the Normal Feed.
- Arc Flash Scenario 3 – System supplied from the alternate utility source. B-SRTC-SWBD 1 supplied from the Normal Feed.
- Arc Flash Scenario 4 – System supplied from the alternate utility source with the assumed minimum fault current. B-SRTC-SWBD 1 supplied from the Normal Feed.
- Arc Flash Scenario 5 – System supplied from the preferred utility source. B-SRTC-SWBD 1 supplied from the Emergency Feed.

- Arc Flash Scenario 6 – System supplied from the preferred utility source with the assumed minimum fault current. B-SRTC-SWBD 1 supplied from the Emergency Feed.
- Arc Flash Scenario 7 – System supplied from the alternate utility source. B-SRTC-SWBD 1 supplied from the Emergency Feed.
- Arc Flash Scenario 8 – System supplied from the alternate utility source with the assumed minimum fault current. B-SRTC-SWBD 1 supplied from the Emergency Feed.

2. Assumptions

The following assumptions were used in performing the arc flash analysis, and ensure conservative, worst-case results:

- The minimum utility fault current from the preferred source is assumed to be 50% of the maximum available fault current values provided by Portland General Electric for the preferred source.
- The minimum utility fault current from the alternate source is assumed to be 50% of the maximum available fault current values provided by Portland General Electric for the alternate source.

For this arc flash hazard analysis of Portland State University the circuit model included the West Campus Loop distribution system. The analysis required energy and boundary calculations for approximately forty-eight (48) locations.

5.3 **Arc Flash Hazard Analysis Results**

The incident energy associated with an arc flash is dependent upon the following parameters:

- The maximum “bolted fault” three-phase short-circuit current available at the equipment and the minimum fault level at which the arc will self-sustain.
- The total protective device clearing time (upstream of the prospective arc location) at the maximum short-circuit current and the minimum fault level at which the arc will self-sustain.
- The distance of the worker from the prospective arc for the task to be performed.

Table 5.3 is provided specifically at the request of Portland State University. It is their requirement that a second incident energy calculation be performed, with a greater working distance, for any location with an incident energy above 40 cal/cm². This is specifically to be used when a qualified person is performing non-contact voltage testing to ensure a piece of equipment is de-energized before performing work. All locations, not just those with an incident energy above 40 cal/cm², were included in Table 5.3 for reference.

The arc flash hazard analysis results shown in Table 5.1, Table 5.2, and Table 5.3 are based on a protective device clearing time that is capped at 2 seconds. This is based on IEEE Std 1584-2002 which states in Annex B, Instructions and Examples; *“If the time is longer than two seconds, consider how long a person is likely to remain in the location of the arc flash. It is likely that a person exposed to an arc flash will move away quickly if it is physically possible, and two seconds is a reasonable maximum time for calculations. A person in a bucket truck or a person who has crawled into equipment will need more time to move away.”*

Two calculations are typically provided for labels on locations where there is adequate separation between the line side terminals of the main protective device, and the work location. The “Load Side” calculation provides the incident energy based on the main protective device clearing in the event of an arc flash incident. If the work location or task is such that the main breaker may not trip in the event of an arc flash incident, then the “Line Side” calculation for incident energy should be observed. This could occur if the main breaker is being racked-out, and a fault occurred on the line terminals. For this case, the next upstream device is the one that must clear the fault.

One should always remember that the terms “Line Side” and “Load Side” are always in reference to the main protective device (see example below).

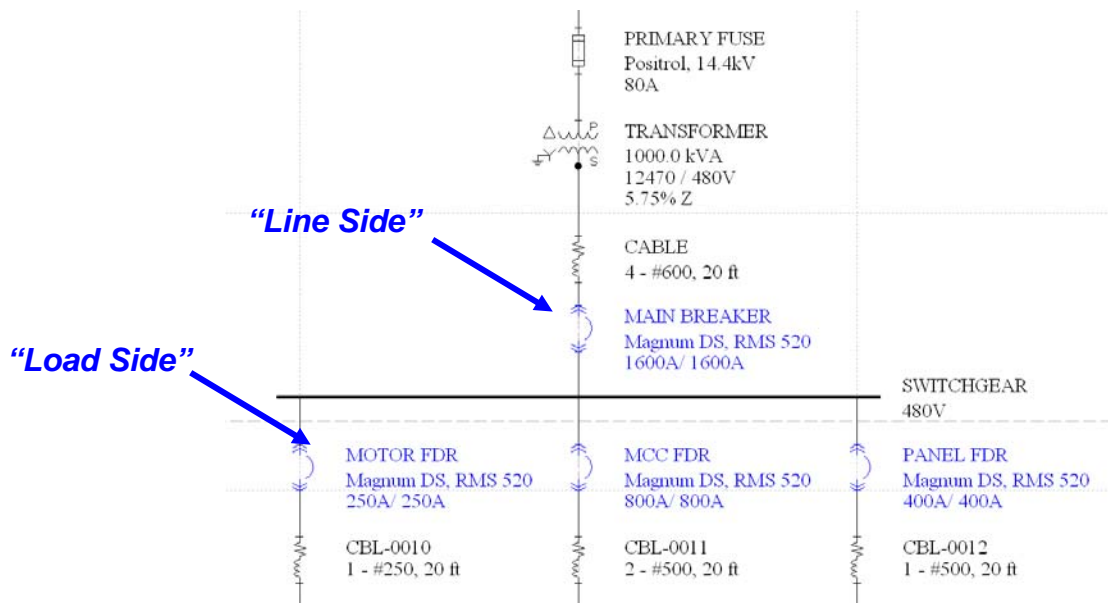


Figure 1: Line Side vs. Load Side

The fault current cannot easily be reduced nor can the working distance be easily increased to lessen the incident energy. In many locations the protective device setting can be adjusted or the trip unit upgraded to decrease the device interrupting time that will in turn decrease the incident energy. For a critical electrical distribution system, such as for the Portland State University campus, it is essential that the system reliability not be compromised. Settings for protective devices cannot be adjusted if the

chance of nuisance trips within critical circuits is introduced. *Each location where the hazard is determined to be unacceptable by “Portland State University” must be individually evaluated to determine the most effective means of reducing the incident energy while maintaining the highest degree of reliability.*

All of the adjustable protective devices listed in Section 4 must be set per the recommended settings of this study to achieve the incident energy levels shown in Table 5.1, Table 5.2, and Table 5.3.

5.4 Arc Flash Summary Table Heading Descriptions

Table 5.1, Table 5.2, and Table 5.3 show results of the SKM PowerTools arc flash hazard analysis. The following column headings describe the results.

Column #1 - Bus Name: The names in this column correlate to the names implemented in the software system model (reference the one-lines included in Appendix D) These locations correspond to plant locations such as main switchboards, panelboards, enclosed breakers, etc.

Column #2 - Protective Device Name: This column lists the name of the device primarily responsible for clearing a potential fault at the associated bus. Again, these device names correlate to the system model.

Column #3 - Bus Voltage (kV): The values in this column show the nominal voltage of the bus location noted in Column #1.

Column #4 - Bus Bolted Fault (kA): This column shows the bolted fault current available for the bus location referenced in Column #1. This current value corresponds to the system operating conditions that will result in the worst-case calculated value for incident energy. (See Column # 14.)

Column #5 - Prot Dev Bolted Fault (kA): This column displays the portion of calculated bolted fault currents (See Column #4) that is contributed through the protective device referenced in Column #2.

Column #6 - Prot Dev Arcing Fault (kA): This column displays the portion of calculated arcing fault currents that is contributed through the protective device referenced in Column #2. These values demonstrate a reduction in available fault current due to the arc resistance.

Column #7 - Trip/Delay Time (sec): This column displays the length of time required by the protective device (See Column #2) to trip in the presence of the arcing fault current calculated in Column #6. For low voltage breakers and fuses, this time represents the total clearing time of the device.

Column #8 - Breaker Opening Time (sec): For circuit breakers tripped by a relay, this column shows the opening time of the breaker. This time is added to the Trip time (See Column #7) to determine the total clearing time used in the calculation of incident energy. (See Column #14.)

Column #9 - Gnd: This column indicates whether the fault location includes a path to ground. Systems with high-resistance or low-resistance grounds are assumed to be ungrounded in the arc flash calculations.

Column #10 - Equip Type: This column indicates whether the equipment is Switchgear, Panel, Cable or Open Air. The equipment type provides a default Gap value, and a distance exponent used in the IEEE incident energy equations.

Column #11 – Gap (mm): This column displays the spacing between bus bars or conductors at the arc location.

Column #12 - Arc Flash Boundary: This column displays the distance within which a person must be clothed in the appropriate PPE (Personal Protection Equipment.) (See Column #14.)

Column #13 - Working Distance: This distance indicates the typical working distance associated with the system location referenced in Column #1.

Column #14 - Incident Energy (cal/cm²): Based on the arcing fault current, the total clearing time of the protective device, the bus bar gap, the grounding method, and the typical working distance, the column displays the results of the arc flash calculations at the reference location. This energy level directly corresponds to the appropriate PPE required for each location. NFPA 70E-2012, Table H.3(b) provides guidance for the selection of PPE based on calculated incident energy exposure.

5.5 Arc Flash Hazard Analysis Recommendations

- 1) All of the adjustable protective devices listed in Section 4 must be set per the recommended settings to achieve the incident energy levels listed in Table 5.1, Table 5.2, and Table 5.3.
- 2) Each location where the arc flash hazard is unacceptable to “Portland State University” should be individually evaluated to determine the most effective means of reducing the incident energy while maintaining the highest degree of reliability.

Table 5.1 – Arc Flash Analysis Summary Table

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-CH	FS-SRTC-USB1-R505	12.47	5.85	5.85	5.73	0.184	0.000	Yes	SWG	153	3' 3"	3'	1.3
B-CH ATS	FS-SRTC-USB1-R505	12.47	5.85	5.85	5.73	0.184	0.000	Yes	SWG	153	3' 3"	3'	1.3
B-CH CHLR	FS-SRTC-USB1-R505	12.47	5.81	5.81	5.70	0.186	0.000	Yes	SWG	153	3' 3"	3'	1.3
B-CH CHLR DS	FS-SRTC-USB1-R505	12.47	5.83	5.83	5.71	0.185	0.000	Yes	SWG	153	3' 3"	3'	1.3
B-CH-EMER USB	FS-CH-EMER USB FDR	0.208	14.59	14.59	5.67	2	0.000	Yes	PNL	25	11' 11"	1' 6"	36.0
B-CH-NW USB DS	FS-CH-NW USB FDR	12.47	5.78	5.78	5.66	0.069	0.000	Yes	SWG	153	1' 2"	3'	0.5
B-CH-PNL B	F-CH-PNL B FDR	0.48	17.31	17.31	8.90	0.997	0.000	Yes	PNL	25	10' 6"	1' 6"	29.2
B-CH-SUB 4A	FS-CH-SUB 4A DS	0.48	36.76	36.76	16.95	0.296	0.000	Yes	PNL	25	7' 8"	1' 6"	17.4
B-CH-SUB 4A DS	FS-SUB 4A FDR	12.47	5.84	5.84	5.72	0.082	0.000	Yes	SWG	153	1' 5"	3'	0.6
B-LE USB DS	FS-SMC-LE USB FDR	12.47	10.36	10.36	10.05	0.02	0.000	Yes	SWG	153	7"	3'	0.3
B-LH-TX DS	FS-SB1-LH FDR	12.47	8.86	8.86	8.62	0.024	0.000	Yes	SWG	153	8"	3'	0.3
B-ML	FS-PSC-ML FDR	12.47	11.17	11.17	10.82	0.02	0.000	Yes	SWG	153	8"	3'	0.3
B-ML-USB	FS-ML-USB FDR	0.48	14.89	14.89	7.83	0.724	0.000	Yes	PNL	25	7' 11"	1' 6"	18.5
B-NH EAST	FS-NH-EAST FDR	12.47	9.56	9.56	9.29	0.021	0.000	Yes	SWG	153	7"	3'	0.3
B-NH WEST	FS-CH-NH FDR	12.47	9.77	9.77	9.48	0.028	0.000	Yes	SWG	153	10"	3'	0.3
B-PS1-TX DS	FS-NH-PS1 FDR	12.47	9.37	9.37	9.10	0.019	0.000	Yes	SWG	153	6"	3'	0.2
B-PS1-USB	FS-PS1-USB FDR	0.208	8.55	8.55	3.90	2	0.000	Yes	PNL	25	9' 4"	1' 6"	24.0
B-PS2-TX DS	FS-CH-PS2 FDR	12.47	10.30	10.30	9.99	0.02	0.000	Yes	SWG	153	7"	3'	0.3
B-PSC	FS-WHP-PSC FDR	12.47	11.36	11.36	11.00	0.022	0.000	Yes	SWG	153	9"	3'	0.3
B-PSC-USB	FS-PSC-USB FDR	0.48	14.27	14.27	7.55	0.779	0.000	Yes	PNL	25	8' 1"	1' 6"	19.1
B-SB1	FS-SRTC-USB2-R495	12.47	6.25	6.25	6.12	0.055	0.000	Yes	SWG	153	1'	3'	0.4
B-SMC	FS-CH-SMC FDR	12.47	10.30	10.30	9.99	0.023	0.000	Yes	SWG	153	9"	3'	0.3
B-SMC 2ND USB DS	FS-SMC 2ND USB FDR	12.47	10.41	10.41	10.09	0.019	0.000	Yes	SWG	153	7"	3'	0.3
B-SRTC-SB2	FS-SRTC-USB-R495	12.47	6.28	6.28	6.14	0.163	0.000	Yes	SWG	153	3' 1"	3'	1.2
B-SRTC-SWBD2	FS-SRTC-SWBD2 FDR	0.48	14.61	14.61	7.71	1.496	0.000	Yes	PNL	25	12' 3"	1' 6"	37.5

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-SRTC-SWBD3	FS-SRTC-SWBD3 FDR	0.48	14.61	14.61	7.71	1.496	0.000	Yes	PNL	25	12' 3"	1' 6"	37.5
B-SRTC-SWBD4	FS-SRTC-SWBD4 FDR	4.16	3.24	3.24	3.20	0.763	0.000	Yes	SWG	104	6' 6"	3'	2.5
B-SRTC-SWBD4 DS	FS-SRTC-SWBD4 FDR	12.47	12.36	12.36	11.96	0.024	0.000	Yes	SWG	153	11"	3'	0.4
B-SRTC-USB1 PREF	MaxTripTime @2.0s	12.47	12.65	12.65	12.23	2	0.000	Yes	SWG	153	87' 11"	3'	32.0
B-SRTC-USB2 ALT	MaxTripTime @2.0s	12.47	12.94	12.94	12.50	2	0.000	Yes	SWG	153	90' 1"	3'	32.7
B-WHP	FS-SRTC-USB1-R501	12.47	6.01	6.01	5.88	0.078	0.000	Yes	SWG	153	1' 5"	3'	0.6
B-WHP-USB	FS-WHP-USB FDR	0.48	3.21	3.21	2.11	0.485	0.000	Yes	PNL	25	2' 8"	1' 6"	3.0
B-XSB USB	FS-XSB USB FDR	0.208	19.94	19.94	6.00	0.707	0.000	Yes	PNL	25	6' 7"	1' 6"	13.5
B-XSB USB DS	FS-XSB USB FDR	0.208	20.05	20.05	6.03	0.702	0.000	Yes	PNL	25	6' 7"	1' 6"	13.5
B-XSB-TX DS	FS-SB1-XSB FDR	12.47	6.63	6.63	6.48	0.021	0.000	Yes	SWG	153	5"	3'	0.2

Table 5.2 – Arc Flash Analysis Summary Table for Locations Greater Than 40 cal/cm²

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-CH-NW USB	FS-CH-NW USB DS	0.208	57.73	57.73	12.66	0.972	0.000	Yes	PNL	25	13'	1' 6"	41.6
B-CH-PNL B DS	FS-CH-PNL B FDR	0.48	19.04	19.04	9.66	2	0.000	Yes	PNL	25	17'	1' 6"	64.0
B-CH-SE USB	FS-CH-SE USB FDR	0.208	46.54	46.54	12.81	2	0.000	Yes	PNL	25	20' 5"	1' 6"	86.8
B-LE USB	FS-LE-TX FDR	0.208	25.76	25.76	8.45	2	0.000	Yes	PNL	25	15' 6"	1' 6"	55.4
B-LH-USB	FS-SB1-LH FDR	0.208	43.96	43.96	12.30	2	0.000	Yes	PNL	25	19' 11"	1' 6"	83.1
B-NH-USB EAST	FS-NH-USB EAST FDR	0.208	45.92	45.92	12.69	2	0.000	Yes	PNL	25	20' 4"	1' 6"	85.9
B-NH-USB WEST	FS-NH-USB WEST FDR	0.208	42.85	42.85	12.08	2	0.000	Yes	PNL	25	19' 8"	1' 6"	81.5
B-PS2-USB	FS-PS2-USB FDR	0.208	32.39	32.39	9.93	2	0.000	Yes	PNL	25	17' 3"	1' 6"	65.9
B-SB1-USB	FS-SB1-USB FDR	0.208	41.56	41.56	11.83	2	0.000	Yes	PNL	25	19' 5"	1' 6"	79.6
B-SMC 2ND USB	FS-SMC 2ND USB FDR	0.208	26.66	26.66	8.66	2	0.000	Yes	PNL	25	15' 9"	1' 6"	56.8
B-SMC USB	FS-SMC USB FDR	0.208	34.05	34.05	10.28	2	0.000	Yes	PNL	25	17' 8"	1' 6"	68.4
B-SRTC-SWBD1	FS-SRTC-SWBD1 EFD	0.208	44.62	44.62	12.43	2	0.000	Yes	PNL	25	20'	1' 6"	84.0
B-SRTC-SWBD5	FS-SRTC-USB2-SUB5	0.48	38.29	38.29	20.64	2	0.000	Yes	PNL	25	28'	1' 6"	145.3
B-CH-NW USB	FS-CH-NW USB DS	0.208	57.73	57.73	12.66	0.972	0.000	Yes	PNL	25	13'	1' 6"	41.6
B-CH-PNL B DS	FS-CH-PNL B FDR	0.48	19.04	19.04	9.66	2	0.000	Yes	PNL	25	17'	1' 6"	64.0
B-CH-SE USB	FS-CH-SE USB FDR	0.208	46.54	46.54	12.81	2	0.000	Yes	PNL	25	20' 5"	1' 6"	86.8

Table 5.3 – Arc Flash Analysis Summary Table for With Working Distance of 8’

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/ Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
<p>Table 5.3 illustrates the arc-flash incident energy at a working distance of 8’. This is the approximate distance the face and body of a qualified person would be from energized equipment when performing a task with a 6’ hot stick. It is important to note that the incident energy values in this table are only applicable when the body and torso are 8’ or over from energized equipment. For arc-flash incident energies at standard working distances as defined by IEEE 1584-2002, please refer to Table 5.1 and Table 5.2.</p>													
B-CH	FS-SRTC-USB1-R505	12.47	5.85	5.85	5.73	0.184	0.000	Yes	SWG	153	3' 3"	8'	0.5
B-CH ATS	FS-SRTC-USB1-R505	12.47	5.85	5.85	5.73	0.184	0.000	Yes	SWG	153	3' 3"	8'	0.5
B-CH CHLR	FS-SRTC-USB1-R505	12.47	5.81	5.81	5.70	0.186	0.000	Yes	SWG	153	3' 3"	8'	0.5
B-CH CHLR DS	FS-SRTC-USB1-R505	12.47	5.83	5.83	5.71	0.185	0.000	Yes	SWG	153	3' 3"	8'	0.5
B-CH-EMER USB	FS-CH-EMER USB FDR	0.208	14.58	14.58	5.67	2	0.000	Yes	PNL	25	11' 11"	8'	2.3
B-CH-NW USB	FS-CH-NW USB DS	0.208	57.73	57.73	12.66	0.972	0.000	Yes	PNL	25	13'	8'	2.7
B-CH-NW USB DS	FS-CH-NW USB FDR	12.47	5.68	5.68	5.56	0.071	0.000	Yes	SWG	153	1' 2"	8'	0.2
B-CH-PNL B	F-CH-PNL B FDR	0.48	17.31	17.31	8.90	0.997	0.000	Yes	PNL	25	10' 6"	8'	1.9
B-CH-PNL B DS	FS-CH-PNL B FDR	0.48	19.01	19.01	9.65	2	0.000	Yes	PNL	25	16' 11"	8'	4.1
B-CH-SE USB	FS-CH-SE USB FDR	0.208	46.48	46.48	12.79	2	0.000	Yes	PNL	25	20' 5"	8'	5.6
B-CH-SUB 4A	FS-CH-SUB 4A DS	0.48	36.76	36.76	16.95	0.296	0.000	Yes	PNL	25	7' 8"	8'	1.1
B-CH-SUB 4A DS	FS-SUB 4A FDR	12.47	5.84	5.84	5.72	0.082	0.000	Yes	SWG	153	1' 5"	8'	0.2
B-LE USB	FS-LE-TX FDR	0.208	25.74	25.74	8.45	2	0.000	Yes	PNL	25	15' 6"	8'	3.6
B-LE USB DS	FS-SMC-LE USB FDR	12.47	10.20	10.20	9.90	0.02	0.000	Yes	SWG	153	7"	8'	0.1
B-LH-TX DS	FS-SB1-LH FDR	12.47	8.86	8.86	8.62	0.024	0.000	Yes	SWG	153	8"	8'	0.1
B-LH-USB	FS-SB1-LH FDR	0.208	43.96	43.96	12.30	2	0.000	Yes	PNL	25	19' 11"	8'	5.3
B-ML	FS-PSC-ML FDR	12.47	10.98	10.98	10.64	0.02	0.000	Yes	SWG	153	8"	8'	0.1
B-ML-USB	FS-ML-USB FDR	0.48	14.92	14.92	7.85	0.722	0.000	Yes	PNL	25	7' 11"	8'	1.2
B-NH EAST	FS-NH-EAST FDR	12.47	9.56	9.56	9.29	0.021	0.000	Yes	SWG	153	7"	8'	0.1

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-NH WEST	FS-CH-NH FDR	12.47	5.66	5.66	5.54	0.048	0.000	Yes	SWG	153	9"	8'	0.1
B-NH-USB EAST	FS-NH-USB EAST FDR	0.208	45.92	45.92	12.69	2	0.000	Yes	PNL	25	20' 4"	8'	5.5
B-NH-USB WEST	FS-NH-USB WEST FDR	0.208	42.79	42.79	12.07	2	0.000	Yes	PNL	25	19' 8"	8'	5.2
B-PS1-TX DS	FS-NH-PS1 FDR	12.47	9.37	9.37	9.10	0.019	0.000	Yes	SWG	153	6"	8'	0.1
B-PS1-USB	FS-PS1-USB FDR	0.208	8.55	8.55	3.90	2	0.000	Yes	PNL	25	9' 4"	8'	1.5
B-PS2-TX DS	FS-CH-PS2 FDR	12.47	10.30	10.30	9.99	0.02	0.000	Yes	SWG	153	7"	8'	0.1
B-PS2-USB	FS-PS2-USB FDR	0.208	32.36	32.36	9.92	2	0.000	Yes	PNL	25	17' 3"	8'	4.2
B-PSC	FS-WHP-PSC FDR	12.47	11.36	11.36	11.00	0.022	0.000	Yes	SWG	153	9"	8'	0.1
B-PSC-USB	FS-PSC-USB FDR	0.48	14.30	14.30	7.57	0.777	0.000	Yes	PNL	25	8' 1"	8'	1.2
B-SB1	FS-SRTC-USB2-R495	12.47	6.25	6.25	6.12	0.055	0.000	Yes	SWG	153	1'	8'	0.2
B-SB1-USB	FS-SB1-USB FDR	0.208	41.51	41.51	11.82	2	0.000	Yes	PNL	25	19' 4"	8'	5.1
B-SMC	FS-CH-SMC FDR	12.47	10.30	10.30	9.99	0.023	0.000	Yes	SWG	153	9"	8'	0.1
B-SMC 2ND USB	FS-SMC 2ND USB FDR	0.208	26.64	26.64	8.65	2	0.000	Yes	PNL	25	15' 9"	8'	3.6
B-SMC 2ND USB DS	FS-SMC 2ND USB FDR	12.47	10.41	10.41	10.09	0.019	0.000	Yes	SWG	153	7"	8'	0.1
B-SMC USB	FS-SMC USB FDR	0.208	34.05	34.05	10.28	2	0.000	Yes	PNL	25	17' 8"	8'	4.4
B-SRTC-SB2	FS-SRTC-USB-R495	12.47	6.28	6.28	6.14	0.163	0.000	Yes	SWG	153	3' 1"	8'	0.5
B-SRTC-SWBD1	FS-SRTC-SWBD1 EFD	0.208	44.62	44.62	12.43	2	0.000	Yes	PNL	25	20'	8'	5.4
B-SRTC-SWBD2	FS-SRTC-SWBD2 FDR	0.48	14.64	14.64	7.72	1.489	0.000	Yes	PNL	25	12' 3"	8'	2.4
B-SRTC-SWBD3	FS-SRTC-SWBD3 FDR	0.48	14.64	14.64	7.72	1.489	0.000	Yes	PNL	25	12' 3"	8'	2.4
B-SRTC-SWBD4	FS-SRTC-SWBD4 FDR	4.16	3.25	3.25	3.21	0.757	0.000	Yes	SWG	104	6' 6"	8'	1.0
B-SRTC-SWBD4 DS	FS-SRTC-SWBD4 FDR	12.47	12.36	12.36	11.96	0.024	0.000	Yes	SWG	153	11"	8'	0.1
B-SRTC-SWBD5	FS-SRTC-USB2-SUB5	0.48	38.29	38.29	20.64	2	0.000	Yes	PNL	25	28'	8'	9.3
B-SRTC-USB1 PREF	MaxTripTime @2.0s	12.47	12.65	12.65	12.23	2	0.000	Yes	SWG	153	87' 11"	8'	12.3
B-SRTC-USB2 ALT	MaxTripTime @2.0s	12.47	12.94	12.94	12.50	2	0.000	Yes	SWG	153	90' 1"	8'	12.6
B-WHP	FS-SRTC-USB2-R497	12.47	6.14	6.14	6.01	0.076	0.000	Yes	SWG	153	1' 5"	8'	0.2
B-WHP-USB	FS-WHP-USB FDR	0.48	3.21	3.21	2.11	0.485	0.000	Yes	PNL	25	2' 8"	8'	0.2
B-XSB USB	FS-XSB USB FDR	0.208	19.96	19.96	6.01	0.706	0.000	Yes	PNL	25	6' 7"	8'	0.9

Bus Name	Protective Device Name	Bus Voltage (kV)	Bus Bolted Fault (kA)	Prot Dev Bolted Fault (kA)	Prot Dev Arcing Fault (kA)	Trip/Delay Time (sec.)	Breaker Opening Time (sec.)	Gnd	Equip Type	Gap (mm)	Arc Flash Boundary	Working Distance	Incident Energy (cal/cm ²)
B-XSB USB DS	FS-XSB USB FDR	0.208	20.07	20.07	6.03	0.701	0.000	Yes	PNL	25	6' 7"	8'	0.9
B-XSB-TX DS	FS-SB1-XSB FDR	12.47	6.63	6.63	6.48	0.021	0.000	Yes	SWG	153	5"	8'	0.1

A. APPENDIX A – SHORT-CIRCUIT INPUT REPORT

Input Report Interpretation

Input Data Tables are provided on the following pages. The following is a guide for interpreting the input data.

1. Generation Contribution Data

- Utility contribution data includes the available fault current in MVA and amps, per unit impedance on a 100 MVA base, X/R, and the line-to-line bus voltage.
- Generator data includes the generator kW rating, X”d, X/R, line-to-line voltage and per unit impedance on a 100 MVA base.

2. Motor Contribution Data

Motor Contribution Data includes the horsepower rating (base kVA rating), speed, subtransient reactance adjusted per the *First Cycle Duty* multipliers described in IEEE Std 141-1993 (Red Book), per-unit impedance on a 100 MVA base, and the bus voltage. X/R ratios for induction motors are obtained from IEEE Std C37.010-1999.

3. Feeder Data

Feeder data includes the following cable and bus data: length, impedance in ohms per 1,000 feet, and per-unit impedance on a 100 MVA base. Impedance values for conductors were obtained from Tables 4A-7 and 4A-8 of IEEE Std 141-1993 (Red Book). The impedance values are based on conductor temperatures of 75°C for Copper and 90°C for Aluminum.

4. Transformer Data

Transformer data includes the transformer kVA rating and per-unit impedance on a 100 MVA base. Unless otherwise provided, transformer X/R ratios are obtained from IEEE Std C37.010-1999.

Short-Circuit Input Report

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Page 1

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FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
B-SMC 2ND USB FDR	B-SMC	B-SMC 2ND USB DS	1	12470	40.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0033 + J 0.0013	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0052 + J 0.0033	PU				
BWY-LE USB	TX-LE USB S	B-LE USB	1	208	10.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.2126 + J 0.1109	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 1.26 + J 0.5938	PU				
BWY-ML-USB	TX-ML-USB S	B-ML-USB	1	480	10.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.0399 + J 0.0208	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 0.2374 + J 0.1115	PU				
BWY-NH-USB EAST	TX-NH-USB EAST E	B-NH-USB EAST	1	208	10.0 FEET	3000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0046 + J 0.0026	Ohms/1000 ft 0.1063 + J 0.0601	PU				
	Z0 Impedance: 0.0273 + J 0.0139	Ohms/1000 ft 0.6310 + J 0.3213	PU				
BWY-NH-USB WEST	TX-NH-USB WEST S	B-NH-USB WEST	1	208	10.0 FEET	3000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0046 + J 0.0026	Ohms/1000 ft 0.1063 + J 0.0601	PU				
	Z0 Impedance: 0.0273 + J 0.0139	Ohms/1000 ft 0.6310 + J 0.3213	PU				
BWY-PS2-USB	TX-PS2-USB S	B-PS2-USB	1	208	15.0 FEET	2500	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0049 + J 0.0030	Ohms/1000 ft 0.1699 + J 0.1040	PU				
	Z0 Impedance: 0.0291 + J 0.0160	Ohms/1000 ft 1.01 + J 0.5547	PU				
BWY-PSC-USB	TX-PSC-USB S	B-PSC-USB	1	480	20.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.0799 + J 0.0417	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 0.4748 + J 0.2230	PU				
BWY-SB1-USB	TX-SB1-USB S	B-SB1-USB	1	208	50.0 FEET	2500	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0057 + J 0.0032	Ohms/1000 ft 0.6587 + J 0.3698	PU				
	Z0 Impedance: 0.2850 + J 0.1600	Ohms/1000 ft 32.94 + J 18.49	PU				
BWY-SMC 2ND USB	TX-SMC 2ND USB S	B-SMC 2ND USB	1	208	10.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.2126 + J 0.1109	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 1.26 + J 0.5938	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
BWY-SRTC-SWBD1-1	TX-SRTC-SWBD1-1 S	B-SRTC-SWBD1	1	208	10.0 FEET	4000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0033 + J 0.0019	Ohms/1000 ft 0.0763 + J 0.0439	PU				
	Z0 Impedance: 0.0196 + J 0.0101	Ohms/1000 ft 0.4530 + J 0.2335	PU				
BWY-SRTC-SWBD2	TX-SRTC-SWBD2 S	B-SRTC-SWBD2	1	480	10.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.0399 + J 0.0208	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 0.2374 + J 0.1115	PU				
BWY-SRTC-SWBD3	TX-SRTC-SWBD3 S	B-SRTC-SWBD3	1	480	10.0 FEET	1600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0092 + J 0.0048	Ohms/1000 ft 0.0399 + J 0.0208	PU				
	Z0 Impedance: 0.0547 + J 0.0257	Ohms/1000 ft 0.2374 + J 0.1115	PU				
BWY-SRTC-SWBD4	TX-SRTC-SWBD4 S	B-SRTC-SWBD4	1	4160	5.0 FEET	600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0119 + J 0.0619	Ohms/1000 ft 0.00034 + J 0.0018	PU				
	Z0 Impedance: 0.0710 + J 0.3314	Ohms/1000 ft 0.0021 + J 0.0096	PU				
BWY-SRTC-SWBD5	TX-SRTC-SWBD5 S	B-SRTC-SWBD5	1	480	10.0 FEET	3200	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0047 + J 0.0026	Ohms/1000 ft 0.0204 + J 0.0113	PU				
	Z0 Impedance: 0.1175 + J 0.0650	Ohms/1000 ft 0.5100 + J 0.2821	PU				
BWY-WHP-USB	TX-WHP-USB S	B-WHP-USB	1	480	5.0 FEET	225	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0425 + J 0.0323	Ohms/1000 ft 0.0922 + J 0.0701	PU				
	Z0 Impedance: 0.2527 + J 0.1729	Ohms/1000 ft 0.5484 + J 0.3752	PU				
CBL-0002	B-SRTC-USB2 ALT	B-SRTC-USB-ATS1	1	12470	1.000 FEET	600	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0119 + J 0.0619	Ohms/1000 ft 0.00001 + J 0.00004	PU				
	Z0 Impedance: 0.0710 + J 0.3314	Ohms/1000 ft 0.00005 + J 0.00021	PU				
CBL-0048	B-NH WEST	B-PS1-TX DS	1	12470	300.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0247 + J 0.0098	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0393 + J 0.0249	PU				
C-CH CHLR DS FDR	B-CH CHLR DS	B-CH	1	12470	50.0 FEET	4/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1050 + J 0.0410	Ohms/1000 ft 0.0034 + J 0.0013	PU				
	Z0 Impedance: 0.1669 + J 0.1044	Ohms/1000 ft 0.0054 + J 0.0034	PU				

FEEDER INPUT DATA									
CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE		
C-CH CHLR FDR	B-CH CHLR DS	B-CH CHLR	1	12470	48.0 FEET	4/0	Aluminum		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.1050 + J 0.0410	Ohms/1000 ft		0.0032 + J 0.0013	PU				
	Z0 Impedance: 0.1669 + J 0.1044	Ohms/1000 ft		0.0052 + J 0.0032	PU				
C-CH-EMER USB	TX-CH-003 S	B-CH-EMER USB	3	208	20.0 FEET	250	Aluminum		
	Duct Material: Magnetic								
	+/- Impedance: 0.0896 + J 0.0384	Ohms/1000 ft		1.38 + J 0.5917	PU				
	Z0 Impedance: 0.2824 + J 0.0946	Ohms/1000 ft		4.35 + J 1.46	PU				
C-CH-EMER USB FDR	B-CH	TX-CH-003 P	1	12470	10.0 FEET	350	Copper		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.0375 + J 0.0450	Ohms/1000 ft		0.00024 + J 0.00029	PU				
	Z0 Impedance: 0.0596 + J 0.1144	Ohms/1000 ft		0.00038 + J 0.00074	PU				
C-CH FDR	B-CH ATS	B-CH	1	12470	8.0 FEET	350	Copper		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.0375 + J 0.0450	Ohms/1000 ft		0.00019 + J 0.00023	PU				
	Z0 Impedance: 0.0596 + J 0.1144	Ohms/1000 ft		0.00031 + J 0.00059	PU				
C-CH-NH FDR	B-CH	B-NH WEST	1	12470	600.0 FEET	1/0	Aluminum		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft		0.0810 + J 0.0174	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft		0.1288 + J 0.0442	PU				
C-CH-NW TX FDR	B-CH-NW USB DS	TX-CH-NW USB P	1	12470	15.0 FEET	1/0	Copper		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft		0.0012 + J 0.00049	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft		0.0020 + J 0.0012	PU				
C-CH-NW USB	TX-CH-NW USB S	B-CH-NW USB	4	208	10.0 FEET	600	Copper		
	Duct Material: Magnetic								
	+/- Impedance: 0.0257 + J 0.0463	Ohms/1000 ft		0.1485 + J 0.2675	PU				
	Z0 Impedance: 0.0809 + J 0.1140	Ohms/1000 ft		0.4675 + J 0.6587	PU				
C-CH-NW USB FDR	B-CH	B-CH-NW USB DS	1	12470	360.0 FEET	1/0	Aluminum		
	Duct Material: Non-Magnetic								
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft		0.0486 + J 0.0104	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft		0.0773 + J 0.0265	PU				
C-CH-PNL B	B-CH-PNL B DS	B-CH-PNL B	9	480	90.0 FEET	250	Copper		
	Duct Material: Magnetic								
	+/- Impedance: 0.0552 + J 0.0495	Ohms/1000 ft		0.2396 + J 0.2148	PU				
	Z0 Impedance: 0.1739 + J 0.1219	Ohms/1000 ft		0.7548 + J 0.5291	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-CH-PNL B DS	TX-CH-002 S Duct Material: Magnetic	B-CH-PNL B DS	9	480	10.0 FEET	250	Copper
	+/- Impedance: 0.0552 + J 0.0495	Ohms/1000 ft 0.0266 + J 0.0239	PU				
	Z0 Impedance: 0.1739 + J 0.1219	Ohms/1000 ft 0.0839 + J 0.0588	PU				
C-CH-PNL B FDR	B-CH CHLR Duct Material: Non-Magnetic	TX-CH-002 P	1	12470	5.0 FEET	1/0	Copper
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-CH-PS2 FDR	B-CH Duct Material: Non-Magnetic	B-PS2-TX DS	1	12470	300.0 FEET	1/0	Aluminum
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft 0.0405 + J 0.0087	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft 0.0644 + J 0.0221	PU				
C-CH-SE USB	TX-CH-001 S Duct Material: Magnetic	B-CH-SE USB	8	208	10.0 FEET	500	Copper
	+/- Impedance: 0.0294 + J 0.0466	Ohms/1000 ft 0.0849 + J 0.1346	PU				
	Z0 Impedance: 0.0926 + J 0.1147	Ohms/1000 ft 0.2675 + J 0.3314	PU				
C-CH-SE USB FDR	B-CH Duct Material: Non-Magnetic	TX-CH-001 P	1	12470	10.0 FEET	350	Copper
	+/- Impedance: 0.0375 + J 0.0450	Ohms/1000 ft 0.00024 + J 0.00029	PU				
	Z0 Impedance: 0.0596 + J 0.1144	Ohms/1000 ft 0.00038 + J 0.00074	PU				
C-CH-SMC FDR	B-CH Duct Material: Non-Magnetic	B-SMC	1	12470	300.0 FEET	1/0	Aluminum
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft 0.0405 + J 0.0087	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft 0.0644 + J 0.0221	PU				
C-CH-SUB 4A	TX-CH-006 S Duct Material: Busway	B-CH-SUB 4A	1	480	10.0 FEET	3000	Copper
	+/- Impedance: 0.0046 + J 0.0026	Ohms/1000 ft 0.0200 + J 0.0113	PU				
	Z0 Impedance: 0.0273 + J 0.0139	Ohms/1000 ft 0.1185 + J 0.0603	PU				
C-CH-SUB 4A DS FDR	B-CH CHLR Duct Material: Non-Magnetic	B-CH-SUB 4A DS	1	12470	300.0 FEET	4/0	Copper
	+/- Impedance: 0.0640 + J 0.0466	Ohms/1000 ft 0.0123 + J 0.0090	PU				
	Z0 Impedance: 0.1017 + J 0.1185	Ohms/1000 ft 0.0196 + J 0.0229	PU				
C-CH-SUB 4A FDR	B-CH-SUB 4A DS Duct Material: Non-Magnetic	TX-CH-006 P	1	12470	5.0 FEET	4/0	Copper
	+/- Impedance: 0.0640 + J 0.0466	Ohms/1000 ft 0.00021 + J 0.00015	PU				
	Z0 Impedance: 0.1017 + J 0.1185	Ohms/1000 ft 0.00033 + J 0.00038	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-LE- TX FDR	B-LE USB DS	TX-LE USB P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-LE USB FDR	B-SMC	B-LE USB DS	1	12470	70.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0058 + J 0.0023	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0092 + J 0.0058	PU				
C-LH-TX FDR	B-LH-TX DS	TX-LH-USB P	1	12470	175.0 FEET	2	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2020 + J 0.0547	Ohms/1000 ft 0.0227 + J 0.0062	PU				
	Z0 Impedance: 0.3211 + J 0.1392	Ohms/1000 ft 0.0361 + J 0.0157	PU				
C-LH-USB	TX-LH-USB S	B-LH-USB	8	208	35.0 FEET	500	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0294 + J 0.0466	Ohms/1000 ft 0.2973 + J 0.4712	PU				
	Z0 Impedance: 0.0926 + J 0.1147	Ohms/1000 ft 0.9364 + J 1.16	PU				
C-ML-USB FDR	B-ML	TX-ML-USB P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-NH-EAST FDR	B-NH WEST	B-NH EAST	1	12470	115.0 FEET	1/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft 0.0155 + J 0.0033	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft 0.0247 + J 0.0085	PU				
C-NH-USB EAST FDR	B-NH EAST	TX-NH-USB EAST P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-NH-USB WEST FDR	B-NH WEST	TX-NH-USB WEST P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-PS1-USB	TX-PS1-USB S	B-PS1-USB	1	208	5.0 FEET	500	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0276 + J 0.0373	Ohms/1000 ft 0.3190 + J 0.4311	PU				
	Z0 Impedance: 0.0438 + J 0.0999	Ohms/1000 ft 0.5062 + J 1.15	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-PS1-USB FDR	B-PS1-TX DS	TX-PS1-USB P	1	12470	5.0 FEET	1	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1600 + J 0.0540	Ohms/1000 ft 0.00051 + J 0.00017	PU				
	Z0 Impedance: 0.2543 + J 0.1374	Ohms/1000 ft 0.00082 + J 0.00044	PU				
C-PS2-USB FDR	B-PS2-TX DS	TX-PS2-USB P	1	12470	10.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00082 + J 0.00033	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0013 + J 0.00083	PU				
C-PSC-ML FDR	B-PSC	B-ML	1	12470	200.0 FEET	1/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2100 + J 0.0450	Ohms/1000 ft 0.0270 + J 0.0058	PU				
	Z0 Impedance: 0.3339 + J 0.1145	Ohms/1000 ft 0.0429 + J 0.0147	PU				
C-PSC-USB FDR	B-PSC	TX-PSC-USB P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-R491	B-SRTC-USB-ATS1	B-SRTC-SB2	1	12470	140.0 FEET	4/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1050 + J 0.0410	Ohms/1000 ft 0.0095 + J 0.0037	PU				
	Z0 Impedance: 0.1669 + J 0.1044	Ohms/1000 ft 0.0150 + J 0.0094	PU				
C-R495	B-SRTC-USB2 ALT	B-SB1	1	12470	600.0 FEET	4/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1050 + J 0.0410	Ohms/1000 ft 0.0405 + J 0.0158	PU				
	Z0 Impedance: 0.1669 + J 0.1044	Ohms/1000 ft 0.0644 + J 0.0403	PU				
C-R497	B-SRTC-USB2 ALT	B-WHP	1	12470	1000.0 FEET	4/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0640 + J 0.0466	Ohms/1000 ft 0.0412 + J 0.0300	PU				
	Z0 Impedance: 0.1017 + J 0.1185	Ohms/1000 ft 0.0654 + J 0.0762	PU				
C-R499-1	B-SRTC-USB2 ALT	C-R499 SPLICE	1	12470	900.0 FEET	350	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0638 + J 0.0374	Ohms/1000 ft 0.0369 + J 0.0216	PU				
	Z0 Impedance: 0.1014 + J 0.0951	Ohms/1000 ft 0.0587 + J 0.0550	PU				
C-R499-2	C-R499 SPLICE	B-CH ATS	1	12470	900.0 FEET	350	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0375 + J 0.0450	Ohms/1000 ft 0.0217 + J 0.0260	PU				
	Z0 Impedance: 0.0596 + J 0.1144	Ohms/1000 ft 0.0345 + J 0.0662	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-R505-1	B-SRTC-USB1 PREF	C-R505 SPLICE	1	12470	900.0 FEET	350	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0638 + J 0.0374	Ohms/1000 ft 0.0369 + J 0.0216	PU				
	Z0 Impedance: 0.1014 + J 0.0951	Ohms/1000 ft 0.0587 + J 0.0550	PU				
C-SB1-LH FDR	B-SB1	B-LH-TX DS	1	12470	1000.0 FEET	2	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.3350 + J 0.0500	Ohms/1000 ft 0.2154 + J 0.0322	PU				
	Z0 Impedance: 0.5326 + J 0.1272	Ohms/1000 ft 0.3425 + J 0.0818	PU				
C-SB1-USB FDR	B-SB1	TX-SB1-USB P	1	12470	10.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00082 + J 0.00033	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0013 + J 0.00083	PU				
C-SB1-XSB FDR	B-SB1	B-XSB-TX DS	1	12470	2000.0 FEET	2	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.3350 + J 0.0500	Ohms/1000 ft 0.4309 + J 0.0643	PU				
	Z0 Impedance: 0.5326 + J 0.1272	Ohms/1000 ft 0.6850 + J 0.1636	PU				
C-SMC 2ND USB	B-SMC 2ND USB DS	TX-SMC 2ND USB P	1	12470	5.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.00041 + J 0.00016	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.00065 + J 0.00041	PU				
C-SMC SWBD FDR	B-SMC	TX-SMC-USB P	1	12470	30.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0025 + J 0.00098	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0039 + J 0.0025	PU				
C-SMC USB	TX-SMC-USB S	B-SMC USB	4	208	20.0 FEET	500	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0294 + J 0.0466	Ohms/1000 ft 0.3398 + J 0.5386	PU				
	Z0 Impedance: 0.0926 + J 0.1147	Ohms/1000 ft 1.07 + J 1.33	PU				
C-SRTC-SWBD1 EFD	B-SRTC-SB2	TX-SRTC-SWBD1-1 P	1	12470	30.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0025 + J 0.00098	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0039 + J 0.0025	PU				
C-SRTC-SWBD1 NFD	B-SRTC-SB2	TX-SRTC-SWBD1-2 P	1	12470	60.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J 0.0507	Ohms/1000 ft 0.0049 + J 0.0020	PU				
	Z0 Impedance: 0.2035 + J 0.1290	Ohms/1000 ft 0.0079 + J 0.0050	PU				

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-SRTC-SWBD2 FDR	B-SRTC-SB2	TX-SRTC-SWBD2 P	1	12470	20.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0016 + J	0.00065	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0026 + J	0.0017	PU		
C-SRTC-SWBD3 FDR	B-SRTC-SB2	TX-SRTC-SWBD3 P	1	12470	20.0 FEET	1/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1280 + J	0.0507 Ohms/1000 ft	0.0016 + J	0.00065	PU		
	Z0 Impedance: 0.2035 + J	0.1290 Ohms/1000 ft	0.0026 + J	0.0017	PU		
C-SRTC-SWBD4 FDR	B-SRTC-SB2	B-SRTC-SWBD4 DS	1	12470	75.0 FEET	4/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0640 + J	0.0466 Ohms/1000 ft	0.0031 + J	0.0022	PU		
	Z0 Impedance: 0.1017 + J	0.1185 Ohms/1000 ft	0.0049 + J	0.0057	PU		
C-SRTC-SWBD4 XFMR	B-SRTC-SWBD4 DS	TX-SRTC-SWBD4 P	1	12470	5.0 FEET	4/0	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.0640 + J	0.0466 Ohms/1000 ft	0.00021 + J	0.00015	PU		
	Z0 Impedance: 0.1017 + J	0.1185 Ohms/1000 ft	0.00033 + J	0.00038	PU		
C-SRTC-SWBD5	B-SRTC-USB2 ALT	TX-SRTC-SWBD5 P	1	12470	190.0 FEET	2	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2020 + J	0.0547 Ohms/1000 ft	0.0247 + J	0.0067	PU		
	Z0 Impedance: 0.3211 + J	0.1392 Ohms/1000 ft	0.0392 + J	0.0170	PU		
C-WHP-PSC FDR	B-WHP	B-PSC	1	12470	40.0 FEET	1/0	Aluminum
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2100 + J	0.0450 Ohms/1000 ft	0.0054 + J	0.0012	PU		
	Z0 Impedance: 0.3339 + J	0.1145 Ohms/1000 ft	0.0086 + J	0.0029	PU		
C-WHP-USB FDR	B-WHP	TX-WHP-USB P	1	12470	40.0 FEET	1	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.1600 + J	0.0540 Ohms/1000 ft	0.0041 + J	0.0014	PU		
	Z0 Impedance: 0.2543 + J	0.1374 Ohms/1000 ft	0.0065 + J	0.0035	PU		
C-XSB SWBD	B-XSB USB DS	B-XSB USB	1	208	3.0 FEET	1000	Copper
	Duct Material: Busway						
	+/- Impedance: 0.0142 + J	0.0066 Ohms/1000 ft	0.0985 + J	0.0458	PU		
	Z0 Impedance: 0.0844 + J	0.0353 Ohms/1000 ft	0.5852 + J	0.2448	PU		
C-XSB TX FDR	B-XSB-TX DS	TX-XSB-USB P	1	12470	5.0 FEET	2	Copper
	Duct Material: Non-Magnetic						
	+/- Impedance: 0.2020 + J	0.0547 Ohms/1000 ft	0.00065 + J	0.00018	PU		
	Z0 Impedance: 0.3211 + J	0.1392 Ohms/1000 ft	0.0010 + J	0.00045	PU		

FEEDER INPUT DATA

CABLE NAME	FEEDER FROM NAME	FEEDER TO NAME	QTY /PH	VOLTS L-L	LENGTH	FEEDER SIZE	FEEDER TYPE
C-XSB USB DS	TX-XSB-USB S	B-XSB USB DS	2	208	35.0 FEET	500	Copper
	Duct Material: Magnetic						
	+/- Impedance: 0.0294 + J 0.0466	Ohms/1000 ft	1.19 + J	1.88	PU		
	Z0 Impedance: 0.0926 + J 0.1147	Ohms/1000 ft	3.75 + J	4.64	PU		

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-CH-001	TX-CH-001 P	D 12470.0	TX-CH-001 S	YG 208.00	1573.00	1000.00
	Pos. Seq. Z%: 0.931 + J 5.32	(Zpu 0.931 + j 5.32)	Shell Type			
	Zero Seq. Z%: 0.931 + J 5.32	(Sec 0.931 + j 5.32 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-CH-002	TX-CH-002 P	D 12470.0	TX-CH-002 S	YG 480.00	1000.00	1000.00
	Pos. Seq. Z%: 1.01 + J 5.78	(Zpu 1.01 + j 5.78)	Shell Type			
	Zero Seq. Z%: 1.01 + J 5.78	(Sec 1.01 + j 5.78 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-CH-003	TX-CH-003 P	D 12470.0	TX-CH-003 S	YG 208.00	472.00	300.00
	Pos. Seq. Z%: 1.24 + J 5.15	(Zpu 4.14 + j 17.18)	Shell Type			
	Zero Seq. Z%: 1.24 + J 5.15	(Sec 4.14 + j 17.18 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-CH-006	TX-CH-006 P	D 12470.0	TX-CH-006 S	YG 480.00	2500.00	2500.00
	Pos. Seq. Z%: 0.584 + J 6.12	(Zpu 0.233 + j 2.45)	Shell Type			
	Zero Seq. Z%: 0.584 + J 6.12	(Sec 0.233 + j 2.45 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-CH-NW USB	TX-CH-NW USB P	D 12470.0	TX-CH-NW USB S	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 0.385 + J 1.81	(Zpu 0.770 + j 3.62)	Shell Type			
	Zero Seq. Z%: 0.385 + J 1.81	(Sec 0.770 + j 3.62 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-LE USB	TX-LE USB P	D 12470.0	TX-LE USB S	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 1.06 + J 4.98	(Zpu 2.12 + j 9.96)	Shell Type			
	Zero Seq. Z%: 1.06 + J 4.98	(Sec 2.12 + j 9.96 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-LH-USB	TX-LH-USB P	D 12470.0	TX-LH-USB S	YG 208.00	1000.00	1000.00
	Pos. Seq. Z%: 0.917 + j 5.24 (Zpu 0.917 + j 5.24)		Shell Type			
	Zero Seq. Z%: 0.917 + j 5.24 (Sec 0.917 + j 5.24 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-ML-USB	TX-ML-USB P	D 12470.0	TX-ML-USB S	YG 480.00	750.00	750.00
	Pos. Seq. Z%: 1.02 + j 5.35 (Zpu 1.36 + j 7.14)		Shell Type			
	Zero Seq. Z%: 1.02 + j 5.35 (Sec 1.36 + j 7.14 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-NH-USB EAST	TX-NH-USB EAST P	D 12470.0	TX-NH-USB EAST E	YG 208.00	1333.00	1000.00
	Pos. Seq. Z%: 0.950 + j 5.43 (Zpu 0.950 + j 5.43)		Shell Type			
	Zero Seq. Z%: 0.950 + j 5.43 (Sec 0.950 + j 5.43 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-NH-USB WEST	TX-NH-USB WEST P	D 12470.0	TX-NH-USB WEST S	YG 208.00	1000.00	1000.00
	Pos. Seq. Z%: 1.03 + j 5.86 (Zpu 1.03 + j 5.86)		Shell Type			
	Zero Seq. Z%: 1.03 + j 5.86 (Sec 1.03 + j 5.86 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-PS1-USB	TX-PS1-USB P	D 12470.0	TX-PS1-USB S	YG 208.00	150.00	150.00
	Pos. Seq. Z%: 1.27 + j 4.55 (Zpu 8.45 + j 30.31)		Shell Type			
	Zero Seq. Z%: 1.27 + j 4.55 (Sec 8.45 + j 30.31 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-PS2-USB	TX-PS2-USB P	D 12470.0	TX-PS2-USB S	YG 208.00	750.00	750.00
	Pos. Seq. Z%: 1.12 + j 5.89 (Zpu 1.50 + j 7.86)		Shell Type			
	Zero Seq. Z%: 1.12 + j 5.89 (Sec 1.50 + j 7.86 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-PSC-USB	TX-PSC-USB P	D 12470.0	TX-PSC-USB S	YG 480.00	750.00	750.00
	Pos. Seq. Z%: 1.07 + J 5.60 (Zpu 1.42 + j 7.47)		Shell Type			
	Zero Seq. Z%: 1.07 + J 5.60 (Sec 1.42 + j 7.47 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-SB1-USB	TX-SB1-USB P	D 12470.0	TX-SB1-USB S	YG 208.00	1333.00	1000.00
	Pos. Seq. Z%: 0.998 + J 5.70 (Zpu 0.998 + j 5.70)		Shell Type			
	Zero Seq. Z%: 0.998 + J 5.70 (Sec 0.998 + j 5.70 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-SMC 2ND USB	TX-SMC 2ND USB P	D 12470.0	TX-SMC 2ND USB S	YG 208.00	500.00	500.00
	Pos. Seq. Z%: 1.02 + J 4.80 (Zpu 2.05 + j 9.60)		Shell Type			
	Zero Seq. Z%: 1.02 + J 4.80 (Sec 2.05 + j 9.60 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-SMC-USB	TX-SMC-USB P	D 12470.0	TX-SMC-USB S	YG 208.00	750.00	750.00
	Pos. Seq. Z%: 1.00 + J 5.25 (Zpu 1.33 + j 6.99)		Shell Type			
	Zero Seq. Z%: 1.00 + J 5.25 (Sec 1.33 + j 6.99 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-SRTC-SWBD1-1	TX-SRTC-SWBD1-1 P	D 12470.0	TX-SRTC-SWBD1-1 S	YG 208.00	1333.00	1000.00
	Pos. Seq. Z%: 1.00 + J 5.71 (Zpu 1.00 + j 5.71)		Shell Type			
	Zero Seq. Z%: 1.00 + J 5.71 (Sec 1.00 + j 5.71 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					
TX-SRTC-SWBD1-2	TX-SRTC-SWBD1-2 P	D 12470.0	TX-SRTC-SWBD1-2 S	YG 208.00	1333.00	1000.00
	Pos. Seq. Z%: 1.02 + J 5.81 (Zpu 1.02 + j 5.81)		Shell Type			
	Zero Seq. Z%: 1.02 + J 5.81 (Sec 1.02 + j 5.81 Pri Open)					
	Taps Pri. 0.000 % Sec. 0.000 % Phase Shift (Pri. Leads Sec.): 30.00 Deg.					

TRANSFORMER INPUT DATA

TRANSFORMER NAME	PRIMARY RECORD NO NAME	VOLTS L-L	* SECONDARY RECORD NO NAME	VOLTS L-L	FULL-LOAD KVA	NOMINAL KVA
TX-SRTC-SWBD2	TX-SRTC-SWBD2 P	D 12470.0	TX-SRTC-SWBD2 S	YG 480.00	1000.00	750.00
	Pos. Seq. Z%: 1.05 + J 5.50	(Zpu 1.40 + j 7.33)	Shell Type			
	Zero Seq. Z%: 1.05 + J 5.50	(Sec 1.40 + j 7.33 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				
TX-SRTC-SWBD3	TX-SRTC-SWBD3 P	D 12470.0	TX-SRTC-SWBD3 S	YG 480.00	1000.00	750.00
	Pos. Seq. Z%: 1.05 + J 5.50	(Zpu 1.40 + j 7.33)	Shell Type			
	Zero Seq. Z%: 1.05 + J 5.50	(Sec 1.40 + j 7.33 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				
TX-SRTC-SWBD4	TX-SRTC-SWBD4 P	D 12470.0	TX-SRTC-SWBD4 S	YG 4160.00	2000.00	1500.00
	Pos. Seq. Z%: 0.804 + J 5.26	(Zpu 0.536 + j 3.51)	Shell Type			
	Zero Seq. Z%: 0.804 + J 5.26	(Sec 0.536 + j 3.51 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				
TX-SRTC-SWBD5	TX-SRTC-SWBD5 P	D 12470.0	TX-SRTC-SWBD5 S	YG 480.00	2667.00	2000.00
	Pos. Seq. Z%: 0.750 + J 5.47	(Zpu 0.375 + j 2.73)	Shell Type			
	Zero Seq. Z%: 0.750 + J 5.47	(Sec 0.375 + j 2.73 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				
TX-WHP-USB	TX-WHP-USB P	D 12470.0	TX-WHP-USB S	YG 480.00	150.00	150.00
	Pos. Seq. Z%: 1.48 + J 5.30	(Zpu 9.85 + j 35.32)	Shell Type			
	Zero Seq. Z%: 1.48 + J 5.30	(Sec 9.85 + j 35.32 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				
TX-XSB-USB	TX-XSB-USB P	D 12470.0	TX-XSB-USB S	YG 208.00	200.00	200.00
	Pos. Seq. Z%: 0.547 + J 2.08	(Zpu 2.74 + j 10.40)	Shell Type			
	Zero Seq. Z%: 0.547 + J 2.08	(Sec 2.74 + j 10.40 Pri Open)				
	Taps Pri. 0.000 % Sec. 0.000 %	Phase Shift (Pri. Leads Sec.): 30.00 Deg.				

GENERATION CONTRIBUTION DATA

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=====
BUS          CONTRIBUTION          VOLTAGE
NAME        NAME                    L-L    MVA    X"d  X/R
=====
B-SRTC-USB1 PEF  PGE-PREF                    12470.0  273.21
  Three Phase      Contribution:  12649.2 AMPS      5.00
  Single Line to Ground Contribution:  10378.9 AMPS      2.06
  Pos Sequence Impedance (100 MVA Base)  0.0718 + J    0.3589 PU
  Zero Sequence Impedance (100 MVA Base)  0.4397 + J    0.4866 PU

B-SRTC-USB2 ALT  PGE-ALT                    12470.0  279.45
  Three Phase      Contribution:  12938.4 AMPS      4.63
  Single Line to Ground Contribution:  12870.3 AMPS      2.78
  Pos Sequence Impedance (100 MVA Base)  0.0756 + J    0.3498 PU
  Zero Sequence Impedance (100 MVA Base)  0.2140 + J    0.3160 PU
  
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B. APPENDIX B – SHORT-CIRCUIT RESULTS

PSU - West Campus Loop
Portland, OR
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ALL INFORMATION PRESENTED IS FOR REVIEW, APPROVAL
INTERPRETATION AND APPLICATION BY A REGISTERED ENGINEER ONLY
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SKM POWER*TOOLS FOR WINDOWS
A_FAULT SHORT CIRCUIT ANALYSIS REPORT
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T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

B-CH	3P Duty: 11.029 KA AT -71.33 DEG (238.22 MVA) VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2090 + J 0.6184 OHMS C-CH FDR B-CH ATS	X/R: 2.96 11.029 KA	ANG: -71.33
B-CH ATS	3P Duty: 11.037 KA AT -71.34 DEG (238.38 MVA) VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2087 + J 0.6181 OHMS C-R499-2 C-R499 SPLICE	X/R: 2.96 11.037 KA	ANG: 108.66
B-CH CHLR	3P Duty: 10.910 KA AT -70.59 DEG (235.63 MVA) VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2193 + J 0.6224 OHMS C-CH CHLR FDR B-CH CHLR DS	X/R: 2.84 10.910 KA	ANG: -250.59
B-CH CHLR DS	3P Duty: 10.968 KA AT -70.95 DEG (236.90 MVA) VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2142 + J 0.6205 OHMS C-CH CHLR DS FDR B-CH	X/R: 2.90 10.968 KA	ANG: -70.95
B-CH-EMER USB	3P Duty: 14.590 KA AT -72.71 DEG (5.26 MVA) VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0024 + J 0.0079 OHMS LOW VOLTAGE POWER CIRCUIT BREAKER 14.590 KA MOLDED CASE CIRCUIT BREAKER < 20KA 14.631 KA MOLDED CASE CIRCUIT BREAKER > 20KA 14.590 KA C-CH-EMER USB TX-CH-003 S	X/R: 3.21 14.590 KA	ANG: -72.71
B-CH-NW USB	3P Duty: 62.595 KA AT -75.59 DEG (22.55 MVA) VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0005 + J 0.0019 OHMS LOW VOLTAGE POWER CIRCUIT BREAKER 62.595 KA MOLDED CASE CIRCUIT BREAKER > 20KA 62.595 KA C-CH-NW USB TX-CH-NW USB S	X/R: 3.89 62.595 KA	ANG: -75.59
B-CH-NW USB DS	3P Duty: 10.352 KA AT -65.85 DEG (223.58 MVA) VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2846 + J 0.6346 OHMS C-CH-NW USB FDR B-CH	X/R: 2.23 10.352 KA	ANG: -65.85
B-CH-PNL B	3P Duty: 18.290 KA AT -77.53 DEG (15.21 MVA) VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0033 + J 0.0148 OHMS LOW VOLTAGE POWER CIRCUIT BREAKER 18.290 KA MOLDED CASE CIRCUIT BREAKER < 20KA 19.981 KA MOLDED CASE CIRCUIT BREAKER > 20KA 18.290 KA C-CH-PNL B B-CH-PNL B DS	X/R: 4.52 18.290 KA	ANG: -257.53
B-CH-PNL B DS	3P Duty: 19.039 KA AT -79.23 DEG (15.83 MVA) VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0027 + J 0.0143 OHMS LOW VOLTAGE POWER CIRCUIT BREAKER 19.039 KA MOLDED CASE CIRCUIT BREAKER > 20KA 19.333 KA C-CH-PNL B DS TX-CH-002 S	X/R: 5.26 19.039 KA	ANG: -79.23

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-CH-SE USB          3P Duty: 46.543 KA AT -78.87 DEG ( 16.77 MVA) X/R: 5.08
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0005 + J 0.0025 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 46.543 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 46.923 KA
C-CH-SE USB          TX-CH-001 S          46.543 KA    ANG: -78.87

B-CH-SUB 4A         3P Duty: 41.500 KA AT -81.92 DEG ( 34.50 MVA) X/R: 7.04
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0009 + J 0.0066 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 41.995 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 44.587 KA
C-CH-SUB 4A         TX-CH-006 S          41.500 KA    ANG: -81.92

B-CH-SUB 4A DS     3P Duty: 10.593 KA AT -69.46 DEG ( 228.80 MVA) X/R: 2.67
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2385 + J 0.6364 OHMS
C-CH-SUB 4A DS FDR B-CH CHLR          10.593 KA    ANG: -69.46

B-LE USB           3P Duty: 25.763 KA AT -76.50 DEG ( 9.28 MVA) X/R: 4.17
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0011 + J 0.0045 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 25.763 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 25.763 KA
BWY-LE USB          TX-LE USB S          25.763 KA    ANG: -76.50

B-LE USB DS       3P Duty: 10.362 KA AT -66.15 DEG ( 223.81 MVA) X/R: 2.26
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2809 + J 0.6355 OHMS
C-LE USB FDR        B-SMC          10.362 KA    ANG: -66.15

B-LH-TX DS        3P Duty: 8.942 KA AT -50.19 DEG ( 193.13 MVA) X/R: 1.20
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.5155 + J 0.6185 OHMS
C-SB1-LH FDR        B-SB1          8.942 KA    ANG: -50.19

B-LH-USB          3P Duty: 43.965 KA AT -75.61 DEG ( 15.84 MVA) X/R: 3.90
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0007 + J 0.0026 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 43.965 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 43.965 KA
C-LH-USB            TX-LH-USB S          43.965 KA    ANG: -75.61

B-ML              3P Duty: 11.171 KA AT -68.91 DEG ( 241.29 MVA) X/R: 2.59
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2319 + J 0.6013 OHMS
C-PSC-ML FDR        B-PSC          11.171 KA    ANG: -68.91
  
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T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

B-ML-USB	3P Duty: 15.614 KA AT -78.38 DEG (12.98 MVA)	X/R: 4.86	
	VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0036 + J 0.0174 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER 15.614 KA		
	MOLDED CASE CIRCUIT BREAKER < 20KA 17.341 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA 15.614 KA		
	BWY-ML-USB TX-ML-USB S	15.614 KA	ANG: -78.38
B-NH EAST	3P Duty: 9.688 KA AT -61.10 DEG (209.25 MVA)	X/R: 1.81	
	VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3591 + J 0.6506 OHMS		
	C-NH-EAST FDR B-NH WEST	9.688 KA	ANG: -61.10
B-NH WEST	3P Duty: 9.901 KA AT -62.57 DEG (213.84 MVA)	X/R: 1.93	
	VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3350 + J 0.6454 OHMS		
	C-CH-NH FDR B-CH	9.901 KA	ANG: -62.57
B-NH-USB EAST	3P Duty: 45.919 KA AT -77.70 DEG (16.54 MVA)	X/R: 4.59	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0006 + J 0.0026 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER 45.919 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA 45.919 KA		
	BWY-NH-USB EAST TX-NH-USB EAST E	45.919 KA	ANG: -77.70
B-NH-USB WEST	3P Duty: 42.848 KA AT -77.99 DEG (15.44 MVA)	X/R: 4.70	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0006 + J 0.0027 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER 42.848 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA 42.848 KA		
	BWY-NH-USB WEST TX-NH-USB WEST S	42.848 KA	ANG: -77.99
B-PS1-TX DS	3P Duty: 9.488 KA AT -60.53 DEG (204.92 MVA)	X/R: 1.77	
	VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3734 + J 0.6606 OHMS		
	CBL-0048 B-NH WEST	9.488 KA	ANG: -60.53
B-PS1-USB	3P Duty: 8.556 KA AT -73.87 DEG (3.08 MVA)	X/R: 3.46	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0039 + J 0.0135 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER 8.556 KA		
	MOLDED CASE CIRCUIT BREAKER < 20KA 8.748 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA 8.556 KA		
	C-PS1-USB TX-PS1-USB S	8.556 KA	ANG: -73.87
B-PS2-TX DS	3P Duty: 10.465 KA AT -66.71 DEG (226.03 MVA)	X/R: 2.32	
	VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2720 + J 0.6319 OHMS		
	C-CH-PS2 FDR B-CH	10.465 KA	ANG: -66.71
B-PS2-USB	3P Duty: 32.389 KA AT -77.57 DEG (11.67 MVA)	X/R: 4.54	
	VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0008 + J 0.0036 OHMS		
	LOW VOLTAGE POWER CIRCUIT BREAKER 32.389 KA		
	MOLDED CASE CIRCUIT BREAKER > 20KA 32.389 KA		
	BWY-PS2-USB TX-PS2-USB S	32.389 KA	ANG: -77.57

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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=====
B-PSC          3P Duty: 11.575 KA AT -72.22 DEG ( 250.00 MVA) X/R: 3.12
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1899 + J 0.5923 OHMS
C-WHP-PSC FDR          B-WHP          11.575 KA      ANG: -72.22

B-PSC-USB     3P Duty: 14.934 KA AT -78.35 DEG ( 12.42 MVA) X/R: 4.85
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0037 + J 0.0182 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 14.934 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 16.575 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 14.934 KA
BWY-PSC-USB          TX-PSC-USB S          14.934 KA      ANG: -78.35

B-SB1         3P Duty: 12.070 KA AT -72.39 DEG ( 260.70 MVA) X/R: 3.15
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1805 + J 0.5685 OHMS
C-R495          B-SRTC-USB2 ALT          12.070 KA      ANG: -72.39

B-SB1-USB     3P Duty: 41.559 KA AT -74.59 DEG ( 14.97 MVA) X/R: 3.63
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0008 + J 0.0028 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 41.559 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 41.559 KA
BWY-SB1-USB          TX-SB1-USB S          41.559 KA      ANG: -74.59

B-SMC         3P Duty: 10.465 KA AT -66.71 DEG ( 226.03 MVA) X/R: 2.32
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2720 + J 0.6319 OHMS
C-CH-SMC FDR          B-CH          10.465 KA      ANG: -66.71

B-SMC 2ND USB 3P Duty: 26.657 KA AT -76.46 DEG ( 9.60 MVA) X/R: 4.15
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0011 + J 0.0044 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 26.657 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 26.657 KA
BWY-SMC 2ND USB          TX-SMC 2ND USB S          26.657 KA      ANG: -76.46

B-SMC 2ND USB DS 3P Duty: 10.406 KA AT -66.39 DEG ( 224.76 MVA) X/R: 2.29
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2771 + J 0.6339 OHMS
B-SMC 2ND USB FDR          B-SMC          10.406 KA      ANG: -66.39

B-SMC USB     3P Duty: 34.047 KA AT -76.87 DEG ( 12.27 MVA) X/R: 4.29
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0008 + J 0.0034 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 34.047 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 34.047 KA
C-SMC USB          TX-SMC-USB S          34.047 KA      ANG: -76.87
  
```

T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-SRTC-SB2          3P Duty: 12.734 KA AT -76.48 DEG ( 275.04 MVA) X/R: 4.16
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1322 + J 0.5497 OHMS
C-R491              B-SRTC-USB-ATS1          12.734 KA    ANG: -76.48

B-SRTC-SWBD1       3P Duty: 44.616 KA AT -79.22 DEG ( 16.07 MVA) X/R: 5.25
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0005 + J 0.0026 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 44.616 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 45.290 KA
BWY-SRTC-SWBD1-1   TX-SRTC-SWBD1-1 S          44.616 KA    ANG: -79.22

B-SRTC-SWBD2       3P Duty: 15.305 KA AT -78.80 DEG ( 12.72 MVA) X/R: 5.05
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0035 + J 0.0178 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 15.305 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 17.141 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 15.408 KA
BWY-SRTC-SWBD2     TX-SRTC-SWBD2 S          15.305 KA    ANG: -78.80

B-SRTC-SWBD3       3P Duty: 15.305 KA AT -78.80 DEG ( 12.72 MVA) X/R: 5.05
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0035 + J 0.0178 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 15.305 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 17.141 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 15.408 KA
BWY-SRTC-SWBD3     TX-SRTC-SWBD3 S          15.305 KA    ANG: -78.80

B-SRTC-SWBD4       3P Duty: 3.546 KA AT -80.82 DEG ( 25.55 MVA) X/R: 6.18
VOLTAGE: 4160. EQUIV. IMPEDANCE= 0.1081 + J 0.6686 OHMS
BWY-SRTC-SWBD4     TX-SRTC-SWBD4 S          3.546 KA    ANG: -80.82

B-SRTC-SWBD4 DS    3P Duty: 12.633 KA AT -76.09 DEG ( 272.85 MVA) X/R: 4.04
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1370 + J 0.5532 OHMS
C-SRTC-SWBD4 FDR   B-SRTC-SB2          12.633 KA    ANG: -76.09

B-SRTC-SWBD5       3P Duty: 38.288 KA AT -80.92 DEG ( 31.83 MVA) X/R: 6.26
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0011 + J 0.0071 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 38.288 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 40.262 KA
BWY-SRTC-SWBD5     TX-SRTC-SWBD5 S          38.288 KA    ANG: -80.92

B-SRTC-USB1 PREF   3P Duty: 12.649 KA AT -78.68 DEG ( 273.21 MVA) X/R: 5.00
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1117 + J 0.5581 OHMS
CONTRIBUTIONS TO B-SRTC-USB1 PREF (CONTINUED)
CONTRIBUTIONS: PGE-PREF          12.649 KA    ANG: -78.68
  
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T H R E E P H A S E F A U L T R E P O R T
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-SRTC-USB2 ALT          3P Duty: 12.938 KA AT -77.81 DEG ( 279.45 MVA) X/R: 4.63
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1175 + J 0.5439 OHMS
CONTRIBUTIONS: PGE-ALT                                     12.938 KA    ANG: -77.81

B-WHP                    3P Duty: 11.654 KA AT -72.91 DEG ( 251.72 MVA) X/R: 3.25
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1815 + J 0.5905 OHMS
C-R497                  B-SRTC-USB2 ALT                                     11.654 KA    ANG: -72.91

B-WHP-USB                3P Duty: 3.237 KA AT -74.29 DEG ( 2.69 MVA) X/R: 3.55
VOLTAGE: 480. EQUIV. IMPEDANCE= 0.0232 + J 0.0824 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 3.237 KA
MOLDED CASE CIRCUIT BREAKER < 10KA 3.933 KA
MOLDED CASE CIRCUIT BREAKER < 20KA 3.333 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 3.237 KA
BWY-WHP-USB           TX-WHP-USB S                                     3.237 KA    ANG: -74.29

B-XSB USB                3P Duty: 20.483 KA AT -70.29 DEG ( 7.38 MVA) X/R: 2.79
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0020 + J 0.0055 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 20.483 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 20.483 KA
C-XSB SWBD             B-XSB USB DS                                     20.483 KA    ANG: -70.29

B-XSB USB DS            3P Duty: 20.599 KA AT -70.61 DEG ( 7.42 MVA) X/R: 2.84
VOLTAGE: 208. EQUIV. IMPEDANCE= 0.0019 + J 0.0055 OHMS
LOW VOLTAGE POWER CIRCUIT BREAKER 20.599 KA
MOLDED CASE CIRCUIT BREAKER > 20KA 20.599 KA
C-XSB USB DS           TX-XSB-USB S                                     20.599 KA    ANG: -70.61

B-XSB-TX DS             3P Duty: 6.655 KA AT -38.17 DEG ( 143.75 MVA) X/R: 0.79
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.8505 + J 0.6685 OHMS
C-SB1-XSB FDR          B-SB1                                           6.655 KA    ANG: -38.17
  
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UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION	FAULT	KA	X/R	EQUIVALENT (PU)	ASYM. KA AT 0.5 CYCLES	
VOLTAGE	DUTIES	(RMS)		FAULT IMPEDANCE	* MAX. RMS	AVG. RMS *
B-CH		3P Duty: 11.029	3. Z1=	0.4198	12.278	11.662
		SLG DUTY: 10.204	2. Z2=	0.4198	10.732	
12470. VOLTS	LN/LN:	9.552	Z0=	0.5350		
	LN/LN/GND:	11.476 (9.401 GND RETURN KA)			
B-CH ATS		3P Duty: 11.037	3. Z1=	0.4195	12.289	11.671
		SLG DUTY: 10.213	2. Z2=	0.4195	10.742	
12470. VOLTS	LN/LN:	9.558	Z0=	0.5344		
	LN/LN/GND:	11.486 (9.411 GND RETURN KA)			
B-CH CHLR		3P Duty: 10.910	3. Z1=	0.4244	12.044	11.484
		SLG DUTY: 10.050	2. Z2=	0.4244	10.525	
12470. VOLTS	LN/LN:	9.448	Z0=	0.5465		
	LN/LN/GND:	11.322 (9.228 GND RETURN KA)			
B-CH CHLR DS		3P Duty: 10.968	3. Z1=	0.4221	12.157	11.570
		SLG DUTY: 10.125	2. Z2=	0.4221	10.625	
12470. VOLTS	LN/LN:	9.499	Z0=	0.5409		
	LN/LN/GND:	11.397 (9.312 GND RETURN KA)			
B-CH-EMER USB		3P Duty: 14.590	3. Z1=	19.0243	16.526	15.574
		SLG DUTY: 14.254	3. Z2=	19.0243	15.667	
208. VOLTS	LN/LN:	12.636	Z0=	20.4753		
	LN/LN/GND:	14.937 (13.908 GND RETURN KA)			
B-CH-NW USB		3P Duty: 62.595	4. Z1=	4.4345	74.010	68.427
		SLG DUTY: 62.513	4. Z2=	4.4345	73.219	
208. VOLTS	LN/LN:	54.208	Z0=	4.4532		
	LN/LN/GND:	63.097 (62.425 GND RETURN KA)			
B-CH-NW USB DS		3P Duty: 10.352	2. Z1=	0.4473	10.953	10.654
		SLG DUTY: 9.357	2. Z2=	0.4473	9.589	
12470. VOLTS	LN/LN:	8.965	Z0=	0.6031		
	LN/LN/GND:	10.638 (8.461 GND RETURN KA)			
B-CH-PNL B		3P Duty: 18.290	5. Z1=	6.5763	22.389	20.394
		SLG DUTY: 18.246	4. Z2=	6.5763	21.829	
480. VOLTS	LN/LN:	15.840	Z0=	6.6334		
	LN/LN/GND:	18.606 (18.193 GND RETURN KA)			

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-CH-PNL B DS	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	19.039 19.423 16.488 19.225 (5. Z1= 5. Z2= Z0=	6.3176 6.3176 5.9428 19.823 GND RETURN KA)	24.123 24.633	21.661
B-CH-SE USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	46.543 47.037 40.307 46.995 (5. Z1= 5. Z2= Z0=	5.9638 5.9638 5.7763 47.541 GND RETURN KA)	58.526 58.808	52.715
B-CH-SUB 4A	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	41.500 43.316 35.940 42.463 (7. Z1= 7. Z2= Z0=	2.8984 2.8984 2.5338 45.298 GND RETURN KA)	55.982 58.471	49.030
B-CH-SUB 4A DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	10.593 9.657 9.174 10.912 (3. Z1= 2. Z2= Z0=	0.4371 0.4371 0.5765 8.798 GND RETURN KA)	11.556 10.063	11.080
B-LE USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	25.763 25.538 22.312 26.197 (4. Z1= 4. Z2= Z0=	10.7740 10.7740 11.0802 25.300 GND RETURN KA)	30.944 29.928	28.416
B-LE USB DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	10.362 9.370 8.974 10.648 (2. Z1= 2. Z2= Z0=	0.4468 0.4468 0.6018 8.477 GND RETURN KA)	10.988 9.614	10.677
B-LH-TX DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	8.942 7.801 7.744 9.058 (1. Z1= 1. Z2= Z0=	0.5178 0.5178 0.7599 6.861 GND RETURN KA)	8.989 7.812	8.966
B-LH-USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	43.965 43.172 38.075 43.965 (4. Z1= 4. Z2= Z0=	6.3135 6.3135 6.6633 42.403 GND RETURN KA)	52.000 50.558	48.070

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION	FAULT	KA	X/R	EQUIVALENT (PU)	ASYM. KA AT 0.5 CYCLES	
VOLTAGE	DUTIES	(RMS)		FAULT IMPEDANCE	* MAX. RMS	AVG. RMS *
B-ML	3P Duty:	11.171	3. Z1=	0.4144	12.121	11.651
	SLG DUTY:	10.364	2. Z2=	0.4144	10.725	
12470. VOLTS	LN/LN:	9.675	Z0=	0.5268		
	LN/LN/GND:	11.702 (9.555 GND RETURN KA)			
B-ML-USB	3P Duty:	15.614	5. Z1=	7.7034	19.436	17.580
	SLG DUTY:	15.806	5. Z2=	7.7034	19.569	
480. VOLTS	LN/LN:	13.522	Z0=	7.4237		
	LN/LN/GND:	15.777 (16.002 GND RETURN KA)			
B-NH EAST	3P Duty:	9.688	2. Z1=	0.4779	9.986	9.837
	SLG DUTY:	8.592	1. Z2=	0.4779	8.700	
12470. VOLTS	LN/LN:	8.390	Z0=	0.6732		
	LN/LN/GND:	9.843 (7.660 GND RETURN KA)			
B-NH WEST	3P Duty:	9.901	2. Z1=	0.4676	10.274	10.088
	SLG DUTY:	8.831	2. Z2=	0.4676	8.969	
12470. VOLTS	LN/LN:	8.574	Z0=	0.6502		
	LN/LN/GND:	10.095 (7.907 GND RETURN KA)			
B-NH-USB EAST	3P Duty:	45.919	5. Z1=	6.0449	56.390	51.296
	SLG DUTY:	46.144	4. Z2=	6.0449	55.601	
208. VOLTS	LN/LN:	39.767	Z0=	5.9622		
	LN/LN/GND:	46.737 (46.356 GND RETURN KA)			
B-NH-USB WEST	3P Duty:	42.848	5. Z1=	6.4780	52.918	48.023
	SLG DUTY:	43.033	4. Z2=	6.4780	52.152	
208. VOLTS	LN/LN:	37.108	Z0=	6.4004		
	LN/LN/GND:	43.581 (43.207 GND RETURN KA)			
B-PS1-TX DS	3P Duty:	9.488	2. Z1=	0.4880	9.756	9.622
	SLG DUTY:	8.370	1. Z2=	0.4880	8.469	
12470. VOLTS	LN/LN:	8.216	Z0=	0.6951		
	LN/LN/GND:	9.597 (7.436 GND RETURN KA)			
B-PS1-USB	3P Duty:	8.556	3. Z1=	32.4431	9.848	9.214
	SLG DUTY:	8.532	3. Z2=	32.4431	9.832	
208. VOLTS	LN/LN:	7.409	Z0=	32.7153		
	LN/LN/GND:	8.534 (8.508 GND RETURN KA)			

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION	FAULT	KA	X/R	EQUIVALENT (PU)	ASYM. KA AT 0.5 CYCLES	
VOLTAGE	DUTIES	(RMS)		FAULT IMPEDANCE	* MAX. RMS	AVG. RMS *
B-PS2-TX DS	3P Duty:	10.465	2. Z1=	0.4424	11.143	10.807
	SLG DUTY:	9.493	2. Z2=	0.4424	9.759	
12470. VOLTS	LN/LN:	9.063	Z0=	0.5915		
	LN/LN/GND:	10.776 (8.609 GND RETURN KA)			
B-PS2-USB	3P Duty:	32.389	5. Z1=	8.5699	39.675	36.129
	SLG DUTY:	32.147	4. Z2=	8.5699	38.376	
208. VOLTS	LN/LN:	28.050	Z0=	8.7789		
	LN/LN/GND:	32.936 (31.890 GND RETURN KA)			
B-PSC	3P Duty:	11.575	3. Z1=	0.4000	13.028	12.312
	SLG DUTY:	10.907	2. Z2=	0.4000	11.496	
12470. VOLTS	LN/LN:	10.024	Z0=	0.4890		
	LN/LN/GND:	12.224 (10.187 GND RETURN KA)			
B-PSC-USB	3P Duty:	14.934	5. Z1=	8.0541	18.576	16.807
	SLG DUTY:	15.020	5. Z2=	8.0541	18.415	
480. VOLTS	LN/LN:	12.933	Z0=	7.9195		
	LN/LN/GND:	15.144 (15.105 GND RETURN KA)			
B-SB1	3P Duty:	12.070	3. Z1=	0.3836	13.614	12.854
	SLG DUTY:	11.562	2. Z2=	0.3836	12.152	
12470. VOLTS	LN/LN:	10.453	Z0=	0.4522		
	LN/LN/GND:	12.940 (10.929 GND RETURN KA)			
B-SB1-USB	3P Duty:	41.559	4. Z1=	6.6789	48.361	45.027
	SLG DUTY:	15.795	1. Z2=	6.6789	15.822	
208. VOLTS	LN/LN:	35.992	Z0=	41.6775		
	LN/LN/GND:	38.962 (9.395 GND RETURN KA)			
B-SMC	3P Duty:	10.465	2. Z1=	0.4424	11.143	10.807
	SLG DUTY:	9.493	2. Z2=	0.4424	9.759	
12470. VOLTS	LN/LN:	9.063	Z0=	0.5915		
	LN/LN/GND:	10.776 (8.609 GND RETURN KA)			
B-SMC 2ND USB	3P Duty:	26.657	4. Z1=	10.4126	31.996	29.390
	SLG DUTY:	26.414	4. Z2=	10.4126	30.909	
208. VOLTS	LN/LN:	23.086	Z0=	10.7222		
	LN/LN/GND:	27.121 (26.157 GND RETURN KA)			

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-SMC 2ND USB DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	10.406 9.423 9.012 10.702 (2. Z1= 2. Z2= Z0=	0.4449 0.4449 0.5974 8.533 GND RETURN KA)	11.054 9.675	10.732
B-SMC USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	34.047 33.365 29.485 34.219 (4. Z1= 4. Z2= Z0=	8.1527 8.1527 8.6599 32.700 GND RETURN KA)	41.166 39.611	37.694
B-SRTC-SB2	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	12.734 12.546 11.028 13.893 (4. Z1= 3. Z2= Z0=	0.3636 0.3636 0.3981 12.161 GND RETURN KA)	15.288 13.607	14.041
B-SRTC-SWBD1	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	44.616 44.869 38.639 45.400 (5. Z1= 5. Z2= Z0=	6.2214 6.2214 6.1216 45.112 GND RETURN KA)	56.512 55.697	50.749
B-SRTC-SWBD2	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	15.305 15.460 13.255 15.477 (5. Z1= 5. Z2= Z0=	7.8589 7.8589 7.6236 15.618 GND RETURN KA)	19.217 19.256	17.320
B-SRTC-SWBD3	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	15.305 15.460 13.255 15.477 (5. Z1= 5. Z2= Z0=	7.8589 7.8589 7.6236 15.618 GND RETURN KA)	19.217 19.256	17.320
B-SRTC-SWBD4	3P Duty: SLG DUTY: 4160. VOLTS LN/LN: LN/LN/GND:	3.546 3.657 3.071 3.596 (6. Z1= 6. Z2= Z0=	3.9138 3.9138 3.5565 3.776 GND RETURN KA)	4.656 4.820	4.121
B-SRTC-SWBD4 DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	12.633 12.395 10.940 13.740 (4. Z1= 3. Z2= Z0=	0.3665 0.3665 0.4056 11.970 GND RETURN KA)	15.064 13.401	13.876

UNBALANCED FAULT REPORT
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

LOCATION VOLTAGE	FAULT DUTIES	KA (RMS)	X/R	EQUIVALENT (PU) FAULT IMPEDANCE	ASYM. KA AT 0.5 CYCLES * MAX. RMS	AVG. RMS *
B-SRTC-SWBD5	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	38.288 38.348 33.158 39.679 (6. Z1= 5. Z2= Z0=	3.1415 3.1415 3.1437 38.339 GND RETURN KA)	50.401 47.848	44.566
B-SRTC-USB1 PREF	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	12.649 10.379 10.955 13.271 (5. Z1= 2. Z2= Z0=	0.3660 0.3660 0.6558 8.486 GND RETURN KA)	15.843 10.863	14.293
B-SRTC-USB2 ALT	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	12.938 12.870 11.205 14.198 (5. Z1= 3. Z2= Z0=	0.3578 0.3578 0.3817 12.588 GND RETURN KA)	15.924 14.151	14.472
B-WHP	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	11.654 11.017 10.093 12.328 (3. Z1= 2. Z2= Z0=	0.3973 0.3973 0.4816 10.319 GND RETURN KA)	13.236 11.669	12.458
B-WHP-USB	3P Duty: SLG DUTY: 480. VOLTS LN/LN: LN/LN/GND:	3.237 3.236 2.803 3.245 (4. Z1= 4. Z2= Z0=	37.1586 37.1586 37.1779 3.236 GND RETURN KA)	3.749 3.739	3.498
B-XSB USB	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	20.483 18.970 17.739 20.308 (3. Z1= 3. Z2= Z0=	13.5511 13.5511 16.8353 17.649 GND RETURN KA)	22.536 20.473	21.522
B-XSB USB DS	3P Duty: SLG DUTY: 208. VOLTS LN/LN: LN/LN/GND:	20.599 19.232 17.839 20.374 (3. Z1= 3. Z2= Z0=	13.4750 13.4750 16.3731 18.025 GND RETURN KA)	22.745 20.910	21.686
B-XSB-TX DS	3P Duty: SLG DUTY: 12470. VOLTS LN/LN: LN/LN/GND:	6.655 5.607 5.764 6.531 (1. Z1= 1. Z2= Z0=	0.6957 0.6957 1.0948 4.827 GND RETURN KA)	6.658 5.608	6.656

FAULT STUDY SUMMARY
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

BUS RECORD NO NAME	VOLTAGE AVAILABLE			FAULT DUTIES (KA)	
	L-L	3 PHASE	X/R	LINE/GRND	X/R
B-CH	12470.	11.029	2.96	10.204	2.14
B-CH ATS	12470.	11.037	2.96	10.213	2.14
B-CH CHLR	12470.	10.910	2.84	10.050	2.07
B-CH CHLR DS	12470.	10.968	2.90	10.125	2.11
B-CH-EMER USB	208.	14.590	3.21	14.254	2.78
B-CH-NW USB	208.	62.595	3.89	62.513	3.73
B-CH-NW USB DS	12470.	10.352	2.23	9.357	1.71
B-CH-PNL B	480.	18.290	4.52	18.246	4.10
B-CH-PNL B DS	480.	19.039	5.26	19.423	5.28
B-CH-SE USB	208.	46.543	5.08	47.037	4.96
B-CH-SUB 4A	480.	41.500	7.04	43.316	7.07
B-CH-SUB 4A DS	12470.	10.593	2.67	9.657	2.00
B-LE USB	208.	25.763	4.17	25.538	3.74
B-LE USB DS	12470.	10.362	2.26	9.370	1.73
B-LH-TX DS	12470.	8.942	1.20	7.801	0.96
B-LH-USB	208.	43.965	3.90	43.172	3.73
B-ML	12470.	11.171	2.59	10.364	1.88
B-ML-USB	480.	15.614	4.86	15.806	4.75
B-NH EAST	12470.	9.688	1.81	8.592	1.44
B-NH WEST	12470.	9.901	1.93	8.831	1.51
B-NH-USB EAST	208.	45.919	4.59	46.144	4.22
B-NH-USB WEST	208.	42.848	4.70	43.033	4.33
B-PS1-TX DS	12470.	9.488	1.77	8.370	1.42
B-PS1-USB	208.	8.556	3.46	8.532	3.48
B-PS2-TX DS	12470.	10.465	2.32	9.493	1.76
B-PS2-USB	208.	32.389	4.54	32.147	4.06
B-PSC	12470.	11.575	3.12	10.907	2.17
B-PSC-USB	480.	14.934	4.85	15.020	4.55
B-SB1	12470.	12.070	3.15	11.562	2.13
B-SB1-USB	208.	41.559	3.63	15.795	0.99
B-SMC	12470.	10.465	2.32	9.493	1.76
B-SMC 2ND USB	208.	26.657	4.15	26.414	3.72
B-SMC 2ND USB DS	12470.	10.406	2.29	9.423	1.74
B-SMC USB	208.	34.047	4.29	33.365	3.96
B-SRTC-SB2	12470.	12.734	4.16	12.546	2.59
B-SRTC-SWBD1	208.	44.616	5.25	44.869	4.80
B-SRTC-SWBD2	480.	15.305	5.05	15.460	4.88
B-SRTC-SWBD3	480.	15.305	5.05	15.460	4.88
B-SRTC-SWBD4	4160.	3.546	6.18	3.657	6.29
B-SRTC-SWBD4 DS	12470.	12.633	4.04	12.395	2.54
B-SRTC-SWBD5	480.	38.288	6.26	38.348	4.91
B-SRTC-USB1 PREF	12470.	12.649	5.00	10.379	2.06
B-SRTC-USB2 ALT	12470.	12.938	4.63	12.870	2.78
B-WHP	12470.	11.654	3.25	11.017	2.25

Feb 22, 2013 15:42:55 UNBALANCED LOW VOLTAGE DUTY PAGE 8
 PSU - West Campus Loop
 Portland, OR
 ESE0008353 / TQSISE0008353.1

FAULT STUDY SUMMARY
 (FOR APPLICATION OF LOW VOLTAGE BREAKERS)
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

BUS RECORD NO NAME	VOLTAGE AVAILABLE		FAULT DUTIES (KA)	
	L-L	3 PHASE	X/R	LINE/GRND
B-WHP-USB	480.	3.237	3.55	3.236
B-XSB USB	208.	20.483	2.79	18.970
B-XSB USB DS	208.	20.599	2.84	19.232
B-XSB-TX DS	12470.	6.655	0.79	5.607

99 FAULTED BUSES, 99 BRANCHES, 2 CONTRIBUTIONS
 UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

Feb 22, 2013 15:42:55
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THREE PHASE MOMENTARY DUTY PAGE 1

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-CH          E/Z:      11.029 KA AT  -71.33 DEG ( 238.22 MVA) X/R:      2.96
              SYM*1.6:  17.647 KA          MOMENTARY BASED ON X/R:    12.278 KA
              SYM*2.7:  29.779 KA          CREST BASED ON X/R:     20.993 KA
              VOLTAGE:  12470.    EQUIV. IMPEDANCE=  0.2090 + J  0.6184 OHMS

B-CH ATS      E/Z:      11.037 KA AT  -71.34 DEG ( 238.38 MVA) X/R:      2.96
              SYM*1.6:  17.659 KA          MOMENTARY BASED ON X/R:    12.289 KA
              SYM*2.7:  29.799 KA          CREST BASED ON X/R:     21.012 KA
              VOLTAGE:  12470.    EQUIV. IMPEDANCE=  0.2087 + J  0.6181 OHMS

B-CH CHLR     E/Z:      10.910 KA AT  -70.59 DEG ( 235.63 MVA) X/R:      2.84
              SYM*1.6:  17.455 KA          MOMENTARY BASED ON X/R:    12.044 KA
              SYM*2.7:  29.456 KA          CREST BASED ON X/R:     20.530 KA
              VOLTAGE:  12470.    EQUIV. IMPEDANCE=  0.2193 + J  0.6224 OHMS

B-CH CHLR DS  E/Z:      10.968 KA AT  -70.95 DEG ( 236.90 MVA) X/R:      2.90
              SYM*1.6:  17.549 KA          MOMENTARY BASED ON X/R:    12.157 KA
              SYM*2.7:  29.614 KA          CREST BASED ON X/R:     20.754 KA
              VOLTAGE:  12470.    EQUIV. IMPEDANCE=  0.2142 + J  0.6205 OHMS

B-CH-EMER USB VOLTAGE:    208.    ( SEE LOW VOLTAGE REPORT )

B-CH-NW USB   VOLTAGE:    208.    ( SEE LOW VOLTAGE REPORT )

B-CH-NW USB DS E/Z:      10.352 KA AT  -65.85 DEG ( 223.58 MVA) X/R:      2.23
              SYM*1.6:  16.563 KA          MOMENTARY BASED ON X/R:    10.953 KA
              SYM*2.7:  27.949 KA          CREST BASED ON X/R:     18.218 KA
              VOLTAGE:  12470.    EQUIV. IMPEDANCE=  0.2846 + J  0.6346 OHMS
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T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-CH-PNL B	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-CH-PNL B DS	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-CH-SE USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)
B-CH-SUB 4A	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-CH-SUB 4A DS	E/Z:	10.593 KA AT -69.46 DEG (228.80 MVA)	X/R: 2.67
	SYM*1.6:	16.949 KA	MOMENTARY BASED ON X/R: 11.556 KA
	SYM*2.7:	28.602 KA	CREST BASED ON X/R: 19.598 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.2385 + J 0.6364 OHMS
B-LE USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)
B-LE USB DS	E/Z:	10.362 KA AT -66.15 DEG (223.81 MVA)	X/R: 2.26
	SYM*1.6:	16.579 KA	MOMENTARY BASED ON X/R: 10.988 KA
	SYM*2.7:	27.978 KA	CREST BASED ON X/R: 18.308 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.2809 + J 0.6355 OHMS
B-LH-TX DS	E/Z:	8.942 KA AT -50.19 DEG (193.13 MVA)	X/R: 1.20
	SYM*1.6:	14.307 KA	MOMENTARY BASED ON X/R: 8.989 KA
	SYM*2.7:	24.143 KA	CREST BASED ON X/R: 13.568 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.5155 + J 0.6185 OHMS
B-LH-USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)
B-ML	E/Z:	11.171 KA AT -68.91 DEG (241.29 MVA)	X/R: 2.59
	SYM*1.6:	17.874 KA	MOMENTARY BASED ON X/R: 12.121 KA
	SYM*2.7:	30.163 KA	CREST BASED ON X/R: 20.502 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.2319 + J 0.6013 OHMS
B-ML-USB	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-NH EAST	E/Z:	9.688 KA AT -61.10 DEG (209.25 MVA)	X/R: 1.81
	SYM*1.6:	15.501 KA	MOMENTARY BASED ON X/R: 9.986 KA
	SYM*2.7:	26.158 KA	CREST BASED ON X/R: 16.120 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.3591 + J 0.6506 OHMS

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-NH WEST          E/Z:      9.901 KA AT  -62.57 DEG ( 213.84 MVA) X/R:      1.93
                   SYM*1.6:  15.841 KA      MOMENTARY BASED ON X/R:  10.274 KA
                   SYM*2.7:  26.732 KA      CREST BASED ON X/R:   16.744 KA
                   VOLTAGE: 12470.   EQUIV. IMPEDANCE=  0.3350 + J  0.6454 OHMS

B-NH-USB EAST      VOLTAGE:   208. ( SEE LOW VOLTAGE REPORT )

B-NH-USB WEST      VOLTAGE:   208. ( SEE LOW VOLTAGE REPORT )

B-PS1-TX DS        E/Z:      9.488 KA AT  -60.53 DEG ( 204.92 MVA) X/R:      1.77
                   SYM*1.6:  15.180 KA      MOMENTARY BASED ON X/R:  9.756 KA
                   SYM*2.7:  25.617 KA      CREST BASED ON X/R:   15.690 KA
                   VOLTAGE: 12470.   EQUIV. IMPEDANCE=  0.3734 + J  0.6606 OHMS

B-PS1-USB          VOLTAGE:   208. ( SEE LOW VOLTAGE REPORT )

B-PS2-TX DS        E/Z:     10.465 KA AT  -66.71 DEG ( 226.03 MVA) X/R:      2.32
                   SYM*1.6:  16.744 KA      MOMENTARY BASED ON X/R: 11.143 KA
                   SYM*2.7:  28.256 KA      CREST BASED ON X/R:   18.629 KA
                   VOLTAGE: 12470.   EQUIV. IMPEDANCE=  0.2720 + J  0.6319 OHMS

B-PS2-USB          VOLTAGE:   208. ( SEE LOW VOLTAGE REPORT )

B-PSC              E/Z:     11.575 KA AT  -72.22 DEG ( 250.00 MVA) X/R:      3.12
                   SYM*1.6:  18.520 KA      MOMENTARY BASED ON X/R: 13.028 KA
                   SYM*2.7:  31.252 KA      CREST BASED ON X/R:   22.348 KA
                   VOLTAGE: 12470.   EQUIV. IMPEDANCE=  0.1899 + J  0.5923 OHMS

B-PSC-USB          VOLTAGE:   480. ( SEE LOW VOLTAGE REPORT )
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T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-SB1	E/Z:	12.070 KA AT	-72.39 DEG (260.70 MVA)	X/R:	3.15
	SYM*1.6:	19.313 KA	MOMENTARY BASED ON X/R:	13.614 KA	
	SYM*2.7:	32.590 KA	CREST BASED ON X/R:	23.366 KA	
	VOLTAGE:	12470.	EQUIV. IMPEDANCE=	0.1805 + J 0.5685	OHMS
B-SB1-USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)		
B-SMC	E/Z:	10.465 KA AT	-66.71 DEG (226.03 MVA)	X/R:	2.32
	SYM*1.6:	16.744 KA	MOMENTARY BASED ON X/R:	11.143 KA	
	SYM*2.7:	28.256 KA	CREST BASED ON X/R:	18.629 KA	
	VOLTAGE:	12470.	EQUIV. IMPEDANCE=	0.2720 + J 0.6319	OHMS
B-SMC 2ND USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)		
B-SMC 2ND USB DS	E/Z:	10.406 KA AT	-66.39 DEG (224.76 MVA)	X/R:	2.29
	SYM*1.6:	16.650 KA	MOMENTARY BASED ON X/R:	11.054 KA	
	SYM*2.7:	28.097 KA	CREST BASED ON X/R:	18.444 KA	
	VOLTAGE:	12470.	EQUIV. IMPEDANCE=	0.2771 + J 0.6339	OHMS
B-SMC USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)		
B-SRTC-SB2	E/Z:	12.734 KA AT	-76.48 DEG (275.04 MVA)	X/R:	4.16
	SYM*1.6:	20.374 KA	MOMENTARY BASED ON X/R:	15.288 KA	
	SYM*2.7:	34.382 KA	CREST BASED ON X/R:	26.468 KA	
	VOLTAGE:	12470.	EQUIV. IMPEDANCE=	0.1322 + J 0.5497	OHMS
B-SRTC-SWBD1	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)		

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-SRTC-SWBD2	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-SRTC-SWBD3	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-SRTC-SWBD4	E/Z:	3.546 KA AT -80.82 DEG (25.55 MVA)	X/R: 6.18
	SYM*1.6:	5.674 KA	MOMENTARY BASED ON X/R: 4.656 KA
	SYM*2.7:	9.574 KA	CREST BASED ON X/R: 8.032 KA
	VOLTAGE:	4160.	EQUIV. IMPEDANCE= 0.1081 + J 0.6686 OHMS
B-SRTC-SWBD4 DS	E/Z:	12.633 KA AT -76.09 DEG (272.85 MVA)	X/R: 4.04
	SYM*1.6:	20.212 KA	MOMENTARY BASED ON X/R: 15.064 KA
	SYM*2.7:	34.108 KA	CREST BASED ON X/R: 26.071 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.1370 + J 0.5532 OHMS
B-SRTC-SWBD5	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-SRTC-USB1 PEF	E/Z:	12.649 KA AT -78.68 DEG (273.21 MVA)	X/R: 5.00
	SYM*1.6:	20.239 KA	MOMENTARY BASED ON X/R: 15.843 KA
	SYM*2.7:	34.153 KA	CREST BASED ON X/R: 27.428 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.1117 + J 0.5581 OHMS
CONTRIBUTIONS:	PGE-PREF	12.649 KA	ANG: -78.68
B-SRTC-USB2 ALT	E/Z:	12.938 KA AT -77.81 DEG (279.45 MVA)	X/R: 4.63
	SYM*1.6:	20.702 KA	MOMENTARY BASED ON X/R: 15.924 KA
	SYM*2.7:	34.934 KA	CREST BASED ON X/R: 27.580 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.1175 + J 0.5439 OHMS
CONTRIBUTIONS:	PGE-ALT	12.938 KA	ANG: -77.81
B-WHP	E/Z:	11.654 KA AT -72.91 DEG (251.72 MVA)	X/R: 3.25
	SYM*1.6:	18.647 KA	MOMENTARY BASED ON X/R: 13.236 KA
	SYM*2.7:	31.466 KA	CREST BASED ON X/R: 22.757 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.1815 + J 0.5905 OHMS

Feb 22, 2013 15:42:55
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THREE PHASE MOMENTARY DUTY PAGE 6

T H R E E P H A S E M O M E N T A R Y D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

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B-WHP-USB	VOLTAGE:	480.	(SEE LOW VOLTAGE REPORT)
B-XSB USB	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)
B-XSB USB DS	VOLTAGE:	208.	(SEE LOW VOLTAGE REPORT)
B-XSB-TX DS	E/Z:	6.655 KA AT -38.17 DEG (143.75 MVA)	X/R: 0.79
	SYM*1.6:	10.648 KA	MOMENTARY BASED ON X/R: 6.658 KA
	SYM*2.7:	17.969 KA	CREST BASED ON X/R: 9.585 KA
	VOLTAGE:	12470.	EQUIV. IMPEDANCE= 0.8505 + J 0.6685 OHMS

UNBALANCED MOMENTARY DUTY REPORT

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

LOCATION	VOLTAGE	FAULT TYPE	E/Z KA	X/R	EQUIVALENT IMPEDANCE (PU)	MOMENTARY E/Z * 1.6 @ 0.5 CYCLE	FAULT DUTIES
B-CH	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	11.03 10.20 9.55 11.48 (3.0 2.1	Z1= Z2= Z0= 9.40 GND RETURN KA)	0.4198 0.4198 0.5350	17.65 12.28 16.33 10.73
B-CH ATS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	11.04 10.21 9.56 11.49 (3.0 2.1	Z1= Z2= Z0= 9.41 GND RETURN KA)	0.4195 0.4195 0.5344	17.66 12.29 16.34 10.74
B-CH CHLR	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.91 10.05 9.45 11.32 (2.8 2.1	Z1= Z2= Z0= 9.23 GND RETURN KA)	0.4244 0.4244 0.5465	17.46 12.04 16.08 10.53
B-CH CHLR DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.97 10.12 9.50 11.40 (2.9 2.1	Z1= Z2= Z0= 9.31 GND RETURN KA)	0.4221 0.4221 0.5409	17.55 12.16 16.20 10.63
B-CH-NW USB DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.35 9.36 8.96 10.64 (2.2 1.7	Z1= Z2= Z0= 8.46 GND RETURN KA)	0.4473 0.4473 0.6031	16.56 10.95 14.97 9.59
B-CH-SUB 4A DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.59 9.66 9.17 10.91 (2.7 2.0	Z1= Z2= Z0= 8.80 GND RETURN KA)	0.4371 0.4371 0.5765	16.95 11.56 15.45 10.06
B-LE USB DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.36 9.37 8.97 10.65 (2.3 1.7	Z1= Z2= Z0= 8.48 GND RETURN KA)	0.4468 0.4468 0.6018	16.58 10.99 14.99 9.61
B-LH-TX DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	8.94 7.80 7.74 9.06 (1.2 1.0	Z1= Z2= Z0= 6.86 GND RETURN KA)	0.5178 0.5178 0.7599	14.31 8.99 12.48 7.81

UNBALANCED MOMENTARY DUTY REPORT

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

LOCATION	VOLTAGE	FAULT TYPE	E/Z KA	X/R	EQUIVALENT IMPEDANCE (PU)	MOMENTARY FAULT DUTIES E/Z * 1.6 @ 0.5 CYCLE
B-ML	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	11.17 10.36 9.67 11.70 (2.6 1.9	Z1= 0.4144 Z2= 0.4144 Z0= 0.5268 9.55 GND RETURN KA)	17.87 12.12 16.58 10.72
B-NH EAST	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	9.69 8.59 8.39 9.84 (1.8 1.4	Z1= 0.4779 Z2= 0.4779 Z0= 0.6732 7.66 GND RETURN KA)	15.50 9.99 13.75 8.70
B-NH WEST	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	9.90 8.83 8.57 10.09 (1.9 1.5	Z1= 0.4676 Z2= 0.4676 Z0= 0.6502 7.91 GND RETURN KA)	15.84 10.27 14.13 8.97
B-PS1-TX DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	9.49 8.37 8.22 9.60 (1.8 1.4	Z1= 0.4880 Z2= 0.4880 Z0= 0.6951 7.44 GND RETURN KA)	15.18 9.76 13.39 8.47
B-PS2-TX DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.47 9.49 9.06 10.78 (2.3 1.8	Z1= 0.4424 Z2= 0.4424 Z0= 0.5915 8.61 GND RETURN KA)	16.74 11.14 15.19 9.76
B-PSC	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	11.57 10.91 10.02 12.22 (3.1 2.2	Z1= 0.4000 Z2= 0.4000 Z0= 0.4890 10.19 GND RETURN KA)	18.52 13.03 17.45 11.50
B-SB1	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	12.07 11.56 10.45 12.94 (3.1 2.1	Z1= 0.3836 Z2= 0.3836 Z0= 0.4522 10.93 GND RETURN KA)	19.31 13.61 18.50 12.15
B-SMC	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.47 9.49 9.06 10.78 (2.3 1.8	Z1= 0.4424 Z2= 0.4424 Z0= 0.5915 8.61 GND RETURN KA)	16.74 11.14 15.19 9.76

Feb 22, 2013 15:42:55
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UNBALANCED MOMENTARY DUTY PAGE 3

UNBALANCED MOMENTARY DUTY REPORT

PRE FAULT VOLTAGE: 1.0000

MODEL TRANSFORMER TAPS: NO

LOCATION	VOLTAGE	FAULT TYPE	E/Z KA	X/R	EQUIVALENT IMPEDANCE (PU)	MOMENTARY E/Z * 1.6 @ 0.5 CYCLE	FAULT DUTIES
B-SMC 2ND USB DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	10.41 9.42 9.01 10.70 (2.3 1.7 8.53	Z1= Z2= Z0= GND RETURN KA)	0.4449 0.4449 0.5974	16.65 15.08 11.05 9.68
B-SRTC-SB2	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	12.73 12.55 11.03 13.89 (4.2 2.6 12.16	Z1= Z2= Z0= GND RETURN KA)	0.3636 0.3636 0.3981	20.37 20.07 15.29 13.61
B-SRTC-SWBD4	4160.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	3.55 3.66 3.07 3.60 (6.2 6.3 3.78	Z1= Z2= Z0= GND RETURN KA)	3.9138 3.9138 3.5565	5.67 5.85 4.66 4.82
B-SRTC-SWBD4 DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	12.63 12.39 10.94 13.74 (4.0 2.5 11.97	Z1= Z2= Z0= GND RETURN KA)	0.3665 0.3665 0.4056	20.21 19.83 15.06 13.40
B-SRTC-USB1 PREF	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	12.65 10.38 10.95 13.27 (5.0 2.1 8.49	Z1= Z2= Z0= GND RETURN KA)	0.3660 0.3660 0.6558	20.24 16.61 15.84 10.86
B-SRTC-USB2 ALT	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	12.94 12.87 11.21 14.20 (4.6 2.8 12.59	Z1= Z2= Z0= GND RETURN KA)	0.3578 0.3578 0.3817	20.70 20.59 15.92 14.15
B-WHP	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	11.65 11.02 10.09 12.33 (3.3 2.2 10.32	Z1= Z2= Z0= GND RETURN KA)	0.3973 0.3973 0.4816	18.65 17.63 13.24 11.67
B-XSB-TX DS	12470.	3P Duty: SLG DUTY: VOLTS LN/LN: LN/LN/GND:	6.66 5.61 5.76 6.53 (0.8 0.7 4.83	Z1= Z2= Z0= GND RETURN KA)	0.6957 0.6957 1.0948	10.65 8.97 6.66 5.61

M O M E N T A R Y D U T Y S U M M A R Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 SOLUTION METHOD : E/Z

BUS RECORD NO NAME	VOLTAGE L-L	* 3 KA	P H A S E * X/R	* * * SLG * * *	X/R
B-CH	12470.	12.278	2.96	10.732	2.14
B-CH ATS	12470.	12.289	2.96	10.742	2.14
B-CH CHLR	12470.	12.044	2.84	10.525	2.07
B-CH CHLR DS	12470.	12.157	2.90	10.625	2.11
B-CH-NW USB DS	12470.	10.953	2.23	9.589	1.71
B-CH-SUB 4A DS	12470.	11.556	2.67	10.063	2.00
B-LE USB DS	12470.	10.988	2.26	9.614	1.73
B-LH-TX DS	12470.	8.989	1.20	7.812	0.96
B-ML	12470.	12.121	2.59	10.725	1.88
B-NH EAST	12470.	9.986	1.81	8.700	1.44
B-NH WEST	12470.	10.274	1.93	8.969	1.51
B-PS1-TX DS	12470.	9.756	1.77	8.469	1.42
B-PS2-TX DS	12470.	11.143	2.32	9.759	1.76
B-PSC	12470.	13.028	3.12	11.496	2.17
B-SB1	12470.	13.614	3.15	12.152	2.13
B-SMC	12470.	11.143	2.32	9.759	1.76
B-SMC 2ND USB DS	12470.	11.054	2.29	9.675	1.74
B-SRTC-SB2	12470.	15.288	4.16	13.607	2.59
B-SRTC-SWBD4	4160.	4.656	6.18	4.820	6.29
B-SRTC-SWBD4 DS	12470.	15.064	4.04	13.401	2.54
B-SRTC-USB1 PREF	12470.	15.843	5.00	10.863	2.06
B-SRTC-USB2 ALT	12470.	15.924	4.63	14.151	2.78
B-WHP	12470.	13.236	3.25	11.669	2.25
B-XSB-TX DS	12470.	6.658	0.79	5.608	0.67

52 FAULTED BUSES, 99 BRANCHES, 2 CONTRIBUTIONS
 UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

B-CH E/Z: 11.029 KA AT -71.33 DEG (238.22 MVA) X/R: 2.96
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2090 + J 0.6184 OHMS
 CONTRIBUTIONS: B-CH ATS 11.029 KA ANG: -71.33

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 11.029 0.18 R
 TOTAL REMOTE: 11.029 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	11.029	11.029	11.029	11.029

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.027	1.000	1.000	1.000
DUTY (KA) :	11.330	11.029	11.029	11.029

B-CH ATS E/Z: 11.037 KA AT -71.34 DEG (238.38 MVA) X/R: 2.96
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2087 + J 0.6181 OHMS
 C-R499-2 C-R499 SPLICE 11.037 KA ANG: 108.66

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 11.037 0.18 R
 TOTAL REMOTE: 11.037 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	11.037	11.037	11.037	11.037

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.027	1.000	1.000	1.000
DUTY (KA) :	11.338	11.037	11.037	11.037

B-CH CHLR E/Z: 10.910 KA AT -70.59 DEG (235.63 MVA) X/R: 2.84
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2193 + J 0.6224 OHMS
 CONTRIBUTIONS: B-CH CHLR DS 10.910 KA ANG: -250.59

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.910 0.19 R
 TOTAL REMOTE: 10.910 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.910	10.910	10.910	10.910

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.026	1.000	1.000	1.000
DUTY (KA) :	11.191	10.910	10.910	10.910

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-CH CHLR DS E/Z: 10.968 KA AT -70.95 DEG (236.90 MVA) X/R: 2.90
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2142 + J 0.6205 OHMS
 CONTRIBUTIONS: B-CH 10.968 KA ANG: -70.95

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.968 0.19 R
 TOTAL REMOTE: 10.968 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.968	10.968	10.968	10.968

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.026	1.000	1.000	1.000
DUTY (KA) :	11.259	10.968	10.968	10.968

B-CH-EMER USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-CH-NW USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-CH-NW USB DS E/Z: 10.352 KA AT -65.85 DEG (223.58 MVA) X/R: 2.23
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2846 + J 0.6346 OHMS
 CONTRIBUTIONS: B-CH 10.352 KA ANG: -65.85

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.352 0.27 R
 TOTAL REMOTE: 10.352 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.352	10.352	10.352	10.352

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.018	1.000	1.000	1.000
DUTY (KA) :	10.539	10.352	10.352	10.352

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-CH-PNL B VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
 B-CH-PNL B DS VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
 B-CH-SE USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
 B-CH-SUB 4A VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
 B-CH-SUB 4A DS E/Z: 10.593 KA AT -69.46 DEG (228.80 MVA) X/R: 2.67
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2385 + J 0.6364 OHMS
 CONTRIBUTIONS: B-CH CHLR 10.593 KA ANG: -69.46

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.593 0.22 R
 TOTAL REMOTE: 10.593 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.593	10.593	10.593	10.593

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.024	1.000	1.000	1.000
DUTY (KA) :	10.844	10.593	10.593	10.593

B-LE USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-LE USB DS E/Z: 10.362 KA AT -66.15 DEG (223.81 MVA) X/R: 2.26
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2809 + J 0.6355 OHMS
 CONTRIBUTIONS: B-SMC 10.362 KA ANG: -66.15

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.362 0.27 R
 TOTAL REMOTE: 10.362 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.362	10.362	10.362	10.362

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.019	1.000	1.000	1.000
DUTY (KA) :	10.554	10.362	10.362	10.362

THREE PHASE INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

B-LH-TX DS E/Z: 8.942 KA AT -50.19 DEG (193.13 MVA) X/R: 1.20
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.5155 + J 0.6185 OHMS
 CONTRIBUTIONS: B-SB1 8.942 KA ANG: -50.19

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 8.942 0.50 R
 TOTAL REMOTE: 8.942 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	8.942	8.942	8.942	8.942

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.005	1.000	1.000	1.000
DUTY (KA) :	8.988	8.942	8.942	8.942

B-LH-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-ML E/Z: 11.171 KA AT -68.91 DEG (241.29 MVA) X/R: 2.59
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2319 + J 0.6013 OHMS
 CONTRIBUTIONS: B-PSC 11.171 KA ANG: -68.91

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 11.171 0.20 R
 TOTAL REMOTE: 11.171 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	11.171	11.171	11.171	11.171

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.023	1.000	1.000	1.000
DUTY (KA) :	11.425	11.171	11.171	11.171

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO

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B-ML-USB          VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )

B-NH EAST        E/Z: 9.688 KA AT -61.10 DEG ( 209.25 MVA) X/R: 1.81
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3591 + J 0.6506 OHMS
CONTRIBUTIONS: B-NH WEST 9.688 KA ANG: -61.10

GENERATOR NAME -- AT BUS --          KA  VOLTS PU  LOCAL/REMOTE
PGE-ALT          9.688 KA  NACD RATIO: 1.0000  9.688  0.36  R
TOTAL REMOTE: 9.688 KA

MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 9.688 9.688 9.688 9.688

MULT. FACT: 1.013 1.000 1.000 1.000
DUTY (KA) : 9.812 9.688 9.688 9.688

B-NH WEST        E/Z: 9.901 KA AT -62.57 DEG ( 213.84 MVA) X/R: 1.93
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3350 + J 0.6454 OHMS
CONTRIBUTIONS: B-CH 9.901 KA ANG: -62.57

GENERATOR NAME -- AT BUS --          KA  VOLTS PU  LOCAL/REMOTE
PGE-ALT          9.901 KA  NACD RATIO: 1.0000  9.901  0.33  R
TOTAL REMOTE: 9.901 KA

MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 9.901 9.901 9.901 9.901

MULT. FACT: 1.014 1.000 1.000 1.000
DUTY (KA) : 10.042 9.901 9.901 9.901

B-NH-USB EAST    VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )

B-NH-USB WEST    VOLTAGE: 208. ( SEE LOW VOLTAGE REPORT )

B-PS1-TX DS      E/Z: 9.488 KA AT -60.53 DEG ( 204.92 MVA) X/R: 1.77
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.3734 + J 0.6606 OHMS
CONTRIBUTIONS: B-NH WEST 9.488 KA ANG: -60.53

GENERATOR NAME -- AT BUS --          KA  VOLTS PU  LOCAL/REMOTE
PGE-ALT          9.488 KA  NACD RATIO: 1.0000  9.488  0.37  R
TOTAL REMOTE: 9.488 KA

MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 9.488 9.488 9.488 9.488

MULT. FACT: 1.012 1.000 1.000 1.000
DUTY (KA) : 9.604 9.488 9.488 9.488
  
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T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-PS1-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-PS2-TX DS E/Z: 10.465 KA AT -66.71 DEG (226.03 MVA) X/R: 2.32
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2720 + J 0.6319 OHMS
 CONTRIBUTIONS: B-CH 10.465 KA ANG: -66.71

GENERATOR NAME	-- AT BUS --		KA	VOLTS PU	LOCAL/REMOTE
PGE-ALT			10.465	0.26	R
TOTAL REMOTE:	10.465 KA	NACD RATIO:	1.0000		
	SYM2	SYM3	SYM5	SYM8	
MULT. FACT:	1.000	1.000	1.000	1.000	
DUTY (KA) :	10.465	10.465	10.465	10.465	
	TOT2	TOT3	TOT5	TOT8	
MULT. FACT:	1.019	1.000	1.000	1.000	
DUTY (KA) :	10.667	10.465	10.465	10.465	

B-PS2-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-PSC E/Z: 11.575 KA AT -72.22 DEG (250.00 MVA) X/R: 3.12
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1899 + J 0.5923 OHMS
 CONTRIBUTIONS: B-WHP 11.575 KA ANG: -72.22

GENERATOR NAME	-- AT BUS --		KA	VOLTS PU	LOCAL/REMOTE
PGE-ALT			11.575	0.14	R
TOTAL REMOTE:	11.575 KA	NACD RATIO:	1.0000		
	SYM2	SYM3	SYM5	SYM8	
MULT. FACT:	1.000	1.000	1.000	1.000	
DUTY (KA) :	11.575	11.575	11.575	11.575	
	TOT2	TOT3	TOT5	TOT8	
MULT. FACT:	1.029	1.000	1.000	1.000	
DUTY (KA) :	11.914	11.575	11.575	11.575	

Feb 22, 2013 15:42:55 THREE PHASE INTERRUPTING DUTY PAGE 7
 PSU - West Campus Loop
 Portland, OR
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T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-PSC-USB VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)

B-SB1 E/Z: 12.070 KA AT -72.39 DEG (260.70 MVA) X/R: 3.15
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1805 + J 0.5685 OHMS
 CONTRIBUTIONS: B-SRTC-USB2 AL 12.070 KA ANG: -72.39

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 12.070 0.11 R
 TOTAL REMOTE: 12.070 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	12.070	12.070	12.070	12.070

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.030	1.000	1.000	1.000
DUTY (KA) :	12.429	12.070	12.070	12.070

B-SB1-USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-SMC E/Z: 10.465 KA AT -66.71 DEG (226.03 MVA) X/R: 2.32
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2720 + J 0.6319 OHMS
 CONTRIBUTIONS: B-CH 10.465 KA ANG: -66.71

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.465 0.26 R
 TOTAL REMOTE: 10.465 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.465	10.465	10.465	10.465

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.019	1.000	1.000	1.000
DUTY (KA) :	10.667	10.465	10.465	10.465

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-SMC 2ND USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-SMC 2ND USB DS E/Z: 10.406 KA AT -66.39 DEG (224.76 MVA) X/R: 2.29
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.2771 + J 0.6339 OHMS
 CONTRIBUTIONS: B-SMC 10.406 KA ANG: -66.39

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 10.406 0.26 R
 TOTAL REMOTE: 10.406 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	10.406	10.406	10.406	10.406

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.019	1.000	1.000	1.000
DUTY (KA) :	10.602	10.406	10.406	10.406

B-SMC USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-SRTC-SB2 E/Z: 12.734 KA AT -76.48 DEG (275.04 MVA) X/R: 4.16
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1322 + J 0.5497 OHMS
 CONTRIBUTIONS: B-SRTC-USB-ATS 12.734 KA ANG: -76.48

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 12.734 0.03 R
 TOTAL REMOTE: 12.734 KA NACD RATIO: 1.0000

	SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000
DUTY (KA) :	12.734	12.734	12.734	12.734

	TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.042	1.000	1.000	1.000
DUTY (KA) :	13.274	12.734	12.734	12.734

T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-SRTC-SWBD1 VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)
 B-SRTC-SWBD2 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
 B-SRTC-SWBD3 VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)
 B-SRTC-SWBD4 E/Z: 3.546 KA AT -80.82 DEG (25.55 MVA) X/R: 6.18
 VOLTAGE: 4160. EQUIV. IMPEDANCE= 0.1081 + J 0.6686 OHMS
 BWY-SRTC-SWBD4 TX-SRTC-SWBD4 3.546 KA ANG: -80.82

GENERATOR NAME	-- AT BUS --	KA	VOLTS PU	LOCAL/REMOTE	
PGE-ALT		3.546	0.91	R	
TOTAL REMOTE:	3.546 KA	NACD RATIO: 1.0000			
		SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000	
DUTY (KA) :	3.546	3.546	3.546	3.546	
		TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.090	1.000	1.000	1.000	
DUTY (KA) :	3.866	3.546	3.546	3.546	

B-SRTC-SWBD4 DS E/Z: 12.633 KA AT -76.09 DEG (272.85 MVA) X/R: 4.04
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1370 + J 0.5532 OHMS
 CONTRIBUTIONS: B-SRTC-SB2 12.633 KA ANG: -76.09

GENERATOR NAME	-- AT BUS --	KA	VOLTS PU	LOCAL/REMOTE	
PGE-ALT		12.633	0.04	R	
TOTAL REMOTE:	12.633 KA	NACD RATIO: 1.0000			
		SYM2	SYM3	SYM5	SYM8
MULT. FACT:	1.000	1.000	1.000	1.000	
DUTY (KA) :	12.633	12.633	12.633	12.633	
		TOT2	TOT3	TOT5	TOT8
MULT. FACT:	1.041	1.000	1.000	1.000	
DUTY (KA) :	13.149	12.633	12.633	12.633	

Feb 22, 2013 15:42:55 THREE PHASE INTERRUPTING DUTY PAGE 10
 PSU - West Campus Loop
 Portland, OR
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T H R E E P H A S E I N T E R R U P T I N G D U T Y R E P O R T
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

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B-SRTC-SWBD5          VOLTAGE: 480. ( SEE LOW VOLTAGE REPORT )

B-SRTC-USB1 PREF      E/Z: 12.649 KA AT -78.68 DEG ( 273.21 MVA) X/R: 5.00
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1117 + J 0.5581 OHMS
CONTRIBUTIONS: PGE-PREF 12.649 KA ANG: -78.68

GENERATOR NAME -- AT BUS --          KA VOLTS PU LOCAL/REMOTE
PGE-PREF                               12.649 0.00 R
TOTAL REMOTE: 12.649 KA NACD RATIO: 1.0000

      SYM2  SYM3  SYM5  SYM8
MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 12.649 12.649 12.649 12.649

      TOT2  TOT3  TOT5  TOT8
MULT. FACT: 1.053 1.000 1.000 1.000
DUTY (KA) : 13.319 12.649 12.649 12.649

B-SRTC-USB2 ALT      E/Z: 12.938 KA AT -77.81 DEG ( 279.45 MVA) X/R: 4.63
VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1175 + J 0.5439 OHMS
CONTRIBUTIONS: PGE-ALT 12.938 KA ANG: -77.81

GENERATOR NAME -- AT BUS --          KA VOLTS PU LOCAL/REMOTE
PGE-ALT                               12.938 0.00 R
TOTAL REMOTE: 12.938 KA NACD RATIO: 1.0000

      SYM2  SYM3  SYM5  SYM8
MULT. FACT: 1.000 1.000 1.000 1.000
DUTY (KA) : 12.938 12.938 12.938 12.938

      TOT2  TOT3  TOT5  TOT8
MULT. FACT: 1.048 1.000 1.000 1.000
DUTY (KA) : 13.564 12.938 12.938 12.938
  
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THREE PHASE INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

B-WHP E/Z: 11.654 KA AT -72.91 DEG (251.72 MVA) X/R: 3.25
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.1815 + J 0.5905 OHMS
 CONTRIBUTIONS: B-SRTC-USB2 AL 11.654 KA ANG: -72.91

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 11.654 0.13 R
 TOTAL REMOTE: 11.654 KA NACD RATIO: 1.0000

MULT. FACT:	SYM2	SYM3	SYM5	SYM8
DUTY (KA) :	11.654	11.654	11.654	11.654

MULT. FACT:	TOT2	TOT3	TOT5	TOT8
DUTY (KA) :	12.015	11.654	11.654	11.654

B-WHP-USB VOLTAGE: 480. (SEE LOW VOLTAGE REPORT)

B-XSB USB VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-XSB USB DS VOLTAGE: 208. (SEE LOW VOLTAGE REPORT)

B-XSB-TX DS E/Z: 6.655 KA AT -38.17 DEG (143.75 MVA) X/R: 0.79
 VOLTAGE: 12470. EQUIV. IMPEDANCE= 0.8505 + J 0.6685 OHMS
 CONTRIBUTIONS: B-SB1 6.655 KA ANG: -38.17

GENERATOR NAME -- AT BUS -- KA VOLTS PU LOCAL/REMOTE
 PGE-ALT 6.655 0.69 R
 TOTAL REMOTE: 6.655 KA NACD RATIO: 1.0000

MULT. FACT:	SYM2	SYM3	SYM5	SYM8
DUTY (KA) :	6.655	6.655	6.655	6.655

MULT. FACT:	TOT2	TOT3	TOT5	TOT8
DUTY (KA) :	6.655	6.655	6.655	6.655

UNBALANCED INTERRUPTING DUTY REPORT

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-CH	3P Duty:	11.03	3.0	SYM2:	1.00	1.00	11.03 10.20
	VOLTS: 12470.0 SLG:	10.20	2.1	SYM3:	1.00	1.00	11.03 10.20
	NACD: 1.000 LN/LN:	9.55		SYM5:	1.00	1.00	11.03 10.20
	LN/LN/GND:	11.48		SYM8:	1.00	1.00	11.03 10.20
	GND RETURN:	9.40		TOT2:	1.03	1.02	11.33 10.38
	Z1 (PU):	0.41979		TOT3:	1.00	1.00	11.03 10.20
	Z2 (PU):	0.41979		TOT5:	1.00	1.00	11.03 10.20
	Z0 (PU):	0.53505		TOT8:	1.00	1.00	11.03 10.20
B-CH ATS	3P Duty:	11.04	3.0	SYM2:	1.00	1.00	11.04 10.21
	VOLTS: 12470.0 SLG:	10.21	2.1	SYM3:	1.00	1.00	11.04 10.21
	NACD: 1.000 LN/LN:	9.56		SYM5:	1.00	1.00	11.04 10.21
	LN/LN/GND:	11.49		SYM8:	1.00	1.00	11.04 10.21
	GND RETURN:	9.41		TOT2:	1.03	1.02	11.34 10.39
	Z1 (PU):	0.41951		TOT3:	1.00	1.00	11.04 10.21
	Z2 (PU):	0.41951		TOT5:	1.00	1.00	11.04 10.21
	Z0 (PU):	0.53439		TOT8:	1.00	1.00	11.04 10.21
B-CH CHLR	3P Duty:	10.91	2.8	SYM2:	1.00	1.00	10.91 10.05
	VOLTS: 12470.0 SLG:	10.05	2.1	SYM3:	1.00	1.00	10.91 10.05
	NACD: 1.000 LN/LN:	9.45		SYM5:	1.00	1.00	10.91 10.05
	LN/LN/GND:	11.32		SYM8:	1.00	1.00	10.91 10.05
	GND RETURN:	9.23		TOT2:	1.03	1.02	11.19 10.21
	Z1 (PU):	0.42439		TOT3:	1.00	1.00	10.91 10.05
	Z2 (PU):	0.42439		TOT5:	1.00	1.00	10.91 10.05
	Z0 (PU):	0.54650		TOT8:	1.00	1.00	10.91 10.05
B-CH CHLR DS	3P Duty:	10.97	2.9	SYM2:	1.00	1.00	10.97 10.12
	VOLTS: 12470.0 SLG:	10.12	2.1	SYM3:	1.00	1.00	10.97 10.12
	NACD: 1.000 LN/LN:	9.50		SYM5:	1.00	1.00	10.97 10.12
	LN/LN/GND:	11.40		SYM8:	1.00	1.00	10.97 10.12
	GND RETURN:	9.31		TOT2:	1.03	1.02	11.26 10.29
	Z1 (PU):	0.42213		TOT3:	1.00	1.00	10.97 10.12
	Z2 (PU):	0.42213		TOT5:	1.00	1.00	10.97 10.12
	Z0 (PU):	0.54088		TOT8:	1.00	1.00	10.97 10.12

UNBALANCED INTERRUPTING DUTY REPORT

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-CH-NW USB DS	3P Duty:	10.35	2.2	SYM2:	1.00	1.00	10.35 9.36
	VOLTS: 12470.0	SLG:	9.36	1.7	SYM3:	1.00	1.00 10.35 9.36
	NACD: 1.000	LN/LN:	8.96		SYM5:	1.00	1.00 10.35 9.36
		LN/LN/GND:	10.64		SYM8:	1.00	1.00 10.35 9.36
		GND RETURN:	8.46	TOT2:	1.02	1.01	10.54 9.46
		Z1 (PU):	0.44727	TOT3:	1.00	1.00	10.35 9.36
		Z2 (PU):	0.44727	TOT5:	1.00	1.00	10.35 9.36
		Z0 (PU):	0.60308	TOT8:	1.00	1.00	10.35 9.36
B-CH-SUB 4A DS	3P Duty:	10.59	2.7	SYM2:	1.00	1.00	10.59 9.66
	VOLTS: 12470.0	SLG:	9.66	2.0	SYM3:	1.00	1.00 10.59 9.66
	NACD: 1.000	LN/LN:	9.17		SYM5:	1.00	1.00 10.59 9.66
		LN/LN/GND:	10.91		SYM8:	1.00	1.00 10.59 9.66
		GND RETURN:	8.80	TOT2:	1.02	1.02	10.84 9.80
		Z1 (PU):	0.43706	TOT3:	1.00	1.00	10.59 9.66
		Z2 (PU):	0.43706	TOT5:	1.00	1.00	10.59 9.66
		Z0 (PU):	0.57651	TOT8:	1.00	1.00	10.59 9.66
B-LE USB DS	3P Duty:	10.36	2.3	SYM2:	1.00	1.00	10.36 9.37
	VOLTS: 12470.0	SLG:	9.37	1.7	SYM3:	1.00	1.00 10.36 9.37
	NACD: 1.000	LN/LN:	8.97		SYM5:	1.00	1.00 10.36 9.37
		LN/LN/GND:	10.65		SYM8:	1.00	1.00 10.36 9.37
		GND RETURN:	8.48	TOT2:	1.02	1.01	10.55 9.48
		Z1 (PU):	0.44681	TOT3:	1.00	1.00	10.36 9.37
		Z2 (PU):	0.44681	TOT5:	1.00	1.00	10.36 9.37
		Z0 (PU):	0.60179	TOT8:	1.00	1.00	10.36 9.37
B-LH-TX DS	3P Duty:	8.94	1.2	SYM2:	1.00	1.00	8.94 7.80
	VOLTS: 12470.0	SLG:	7.80	1.0	SYM3:	1.00	1.00 8.94 7.80
	NACD: 1.000	LN/LN:	7.74		SYM5:	1.00	1.00 8.94 7.80
		LN/LN/GND:	9.06		SYM8:	1.00	1.00 8.94 7.80
		GND RETURN:	6.86	TOT2:	1.01	1.00	8.99 7.82
		Z1 (PU):	0.51778	TOT3:	1.00	1.00	8.94 7.80
		Z2 (PU):	0.51778	TOT5:	1.00	1.00	8.94 7.80
		Z0 (PU):	0.75992	TOT8:	1.00	1.00	8.94 7.80

UNBALANCED INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI 3 PHASE	AC/DC SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG	
B-ML	3P Duty:	11.17	2.6	SYM2:	1.00	1.00	11.17 10.36	
	VOLTS: 12470.0	SLG:	10.36	1.9	SYM3:	1.00	1.00 11.17 10.36	
	NACD: 1.000	LN/LN:	9.67		SYM5:	1.00	1.00 11.17 10.36	
		LN/LN/GND:	11.70		SYM8:	1.00	1.00 11.17 10.36	
		GND RETURN:	9.55		TOT2:	1.02	1.01 11.42 10.51	
		Z1 (PU):	0.41445		TOT3:	1.00	1.00 11.17 10.36	
		Z2 (PU):	0.41445		TOT5:	1.00	1.00 11.17 10.36	
		Z0 (PU):	0.52682		TOT8:	1.00	1.00 11.17 10.36	
	B-NH EAST	3P Duty:	9.69	1.8	SYM2:	1.00	1.00	9.69 8.59
		VOLTS: 12470.0	SLG:	8.59	1.4	SYM3:	1.00	1.00 9.69 8.59
NACD: 1.000		LN/LN:	8.39		SYM5:	1.00	1.00 9.69 8.59	
		LN/LN/GND:	9.84		SYM8:	1.00	1.00 9.69 8.59	
		GND RETURN:	7.66		TOT2:	1.01	1.01 9.81 8.66	
		Z1 (PU):	0.47789		TOT3:	1.00	1.00 9.69 8.59	
		Z2 (PU):	0.47789		TOT5:	1.00	1.00 9.69 8.59	
		Z0 (PU):	0.67316		TOT8:	1.00	1.00 9.69 8.59	
B-NH WEST		3P Duty:	9.90	1.9	SYM2:	1.00	1.00	9.90 8.83
		VOLTS: 12470.0	SLG:	8.83	1.5	SYM3:	1.00	1.00 9.90 8.83
	NACD: 1.000	LN/LN:	8.57		SYM5:	1.00	1.00 9.90 8.83	
		LN/LN/GND:	10.09		SYM8:	1.00	1.00 9.90 8.83	
		GND RETURN:	7.91		TOT2:	1.01	1.01 10.04 8.91	
		Z1 (PU):	0.46763		TOT3:	1.00	1.00 9.90 8.83	
		Z2 (PU):	0.46763		TOT5:	1.00	1.00 9.90 8.83	
		Z0 (PU):	0.65019		TOT8:	1.00	1.00 9.90 8.83	
	B-PS1-TX DS	3P Duty:	9.49	1.8	SYM2:	1.00	1.00	9.49 8.37
		VOLTS: 12470.0	SLG:	8.37	1.4	SYM3:	1.00	1.00 9.49 8.37
NACD: 1.000		LN/LN:	8.22		SYM5:	1.00	1.00 9.49 8.37	
		LN/LN/GND:	9.60		SYM8:	1.00	1.00 9.49 8.37	
		GND RETURN:	7.44		TOT2:	1.01	1.01 9.60 8.44	
		Z1 (PU):	0.48800		TOT3:	1.00	1.00 9.49 8.37	
		Z2 (PU):	0.48800		TOT5:	1.00	1.00 9.49 8.37	
		Z0 (PU):	0.69510		TOT8:	1.00	1.00 9.49 8.37	

UNBALANCED INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	AC/DC FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-PS2-TX DS	3P Duty:	10.47	2.3	SYM2:	1.00	1.00	10.47 9.49
	VOLTS: 12470.0 SLG:	9.49	1.8	SYM3:	1.00	1.00	10.47 9.49
	NACD: 1.000 LN/LN:	9.06		SYM5:	1.00	1.00	10.47 9.49
	LN/LN/GND:	10.78		SYM8:	1.00	1.00	10.47 9.49
	GND RETURN:	8.61		TOT2:	1.02	1.01	10.67 9.61
	Z1 (PU):	0.44242		TOT3:	1.00	1.00	10.47 9.49
	Z2 (PU):	0.44242		TOT5:	1.00	1.00	10.47 9.49
	Z0 (PU):	0.59150		TOT8:	1.00	1.00	10.47 9.49
B-PSC	3P Duty:	11.57	3.1	SYM2:	1.00	1.00	11.57 10.91
	VOLTS: 12470.0 SLG:	10.91	2.2	SYM3:	1.00	1.00	11.57 10.91
	NACD: 1.000 LN/LN:	10.02		SYM5:	1.00	1.00	11.57 10.91
	LN/LN/GND:	12.22		SYM8:	1.00	1.00	11.57 10.91
	GND RETURN:	10.19		TOT2:	1.03	1.02	11.91 11.10
	Z1 (PU):	0.40000		TOT3:	1.00	1.00	11.57 10.91
	Z2 (PU):	0.40000		TOT5:	1.00	1.00	11.57 10.91
	Z0 (PU):	0.48898		TOT8:	1.00	1.00	11.57 10.91
B-SB1	3P Duty:	12.07	3.1	SYM2:	1.00	1.00	12.07 11.56
	VOLTS: 12470.0 SLG:	11.56	2.1	SYM3:	1.00	1.00	12.07 11.56
	NACD: 1.000 LN/LN:	10.45		SYM5:	1.00	1.00	12.07 11.56
	LN/LN/GND:	12.94		SYM8:	1.00	1.00	12.07 11.56
	GND RETURN:	10.93		TOT2:	1.03	1.02	12.43 11.76
	Z1 (PU):	0.38358		TOT3:	1.00	1.00	12.07 11.56
	Z2 (PU):	0.38358		TOT5:	1.00	1.00	12.07 11.56
	Z0 (PU):	0.45217		TOT8:	1.00	1.00	12.07 11.56
B-SMC	3P Duty:	10.47	2.3	SYM2:	1.00	1.00	10.47 9.49
	VOLTS: 12470.0 SLG:	9.49	1.8	SYM3:	1.00	1.00	10.47 9.49
	NACD: 1.000 LN/LN:	9.06		SYM5:	1.00	1.00	10.47 9.49
	LN/LN/GND:	10.78		SYM8:	1.00	1.00	10.47 9.49
	GND RETURN:	8.61		TOT2:	1.02	1.01	10.67 9.61
	Z1 (PU):	0.44242		TOT3:	1.00	1.00	10.47 9.49
	Z2 (PU):	0.44242		TOT5:	1.00	1.00	10.47 9.49
	Z0 (PU):	0.59150		TOT8:	1.00	1.00	10.47 9.49

UNBALANCED INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	AC/DC FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-SMC 2ND USB DS	3P Duty:	10.41	2.3	SYM2:	1.00	1.00	10.41 9.42
	VOLTS: 12470.0 SLG:	9.42	1.7	SYM3:	1.00	1.00	10.41 9.42
	NACD: 1.000 LN/LN:	9.01		SYM5:	1.00	1.00	10.41 9.42
	LN/LN/GND:	10.70		SYM8:	1.00	1.00	10.41 9.42
	GND RETURN:	8.53		TOT2:	1.02	1.01	10.60 9.54
	Z1 (PU):	0.44492		TOT3:	1.00	1.00	10.41 9.42
	Z2 (PU):	0.44492		TOT5:	1.00	1.00	10.41 9.42
	Z0 (PU):	0.59738		TOT8:	1.00	1.00	10.41 9.42
B-SRTC-SB2	3P Duty:	12.73	4.2	SYM2:	1.00	1.00	12.73 12.55
	VOLTS: 12470.0 SLG:	12.55	2.6	SYM3:	1.00	1.00	12.73 12.55
	NACD: 1.000 LN/LN:	11.03		SYM5:	1.00	1.00	12.73 12.55
	LN/LN/GND:	13.89		SYM8:	1.00	1.00	12.73 12.55
	GND RETURN:	12.16		TOT2:	1.04	1.02	13.27 12.83
	Z1 (PU):	0.36359		TOT3:	1.00	1.00	12.73 12.55
	Z2 (PU):	0.36359		TOT5:	1.00	1.00	12.73 12.55
	Z0 (PU):	0.39814		TOT8:	1.00	1.00	12.73 12.55
B-SRTC-SWBD4	3P Duty:	3.55	6.2	SYM2:	1.00	1.00	3.55 3.66
	VOLTS: 4160.0 SLG:	3.66	6.3	SYM3:	1.00	1.00	3.55 3.66
	NACD: 1.000 LN/LN:	3.07		SYM5:	1.00	1.00	3.55 3.66
	LN/LN/GND:	3.60		SYM8:	1.00	1.00	3.55 3.66
	GND RETURN:	3.78		TOT2:	1.09	1.09	3.87 4.00
	Z1 (PU):	3.91381		TOT3:	1.00	1.00	3.55 3.66
	Z2 (PU):	3.91381		TOT5:	1.00	1.00	3.55 3.66
	Z0 (PU):	3.55645		TOT8:	1.00	1.00	3.55 3.66
B-SRTC-SWBD4 DS	3P Duty:	12.63	4.0	SYM2:	1.00	1.00	12.63 12.39
	VOLTS: 12470.0 SLG:	12.39	2.5	SYM3:	1.00	1.00	12.63 12.39
	NACD: 1.000 LN/LN:	10.94		SYM5:	1.00	1.00	12.63 12.39
	LN/LN/GND:	13.74		SYM8:	1.00	1.00	12.63 12.39
	GND RETURN:	11.97		TOT2:	1.04	1.02	13.15 12.67
	Z1 (PU):	0.36650		TOT3:	1.00	1.00	12.63 12.39
	Z2 (PU):	0.36650		TOT5:	1.00	1.00	12.63 12.39
	Z0 (PU):	0.40563		TOT8:	1.00	1.00	12.63 12.39

UNBALANCED INTERRUPTING DUTY REPORT
 PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

LOCATION	FAULT TYPE	E/Z KA	X/R	ANSI AC/DC DECREMENT 3 PHASE	FACT. SLG	INTERRUPTING DUTIES (KA) 3 PHASE	SLG
B-SRTC-USB1 PREF	3P Duty:	12.65	5.0	SYM2:	1.00	1.00	12.65 10.38
	VOLTS: 12470.0 SLG:	10.38	2.1	SYM3:	1.00	1.00	12.65 10.38
	NACD: 1.000 LN/LN:	10.95		SYM5:	1.00	1.00	12.65 10.38
	LN/LN/GND:	13.27		SYM8:	1.00	1.00	12.65 10.38
	GND RETURN:	8.49		TOT2:	1.05	1.02	13.32 10.55
	Z1 (PU):	0.36602		TOT3:	1.00	1.00	12.65 10.38
	Z2 (PU):	0.36602		TOT5:	1.00	1.00	12.65 10.38
	Z0 (PU):	0.65583		TOT8:	1.00	1.00	12.65 10.38
B-SRTC-USB2 ALT	3P Duty:	12.94	4.6	SYM2:	1.00	1.00	12.94 12.87
	VOLTS: 12470.0 SLG:	12.87	2.8	SYM3:	1.00	1.00	12.94 12.87
	NACD: 1.000 LN/LN:	11.21		SYM5:	1.00	1.00	12.94 12.87
	LN/LN/GND:	14.20		SYM8:	1.00	1.00	12.94 12.87
	GND RETURN:	12.59		TOT2:	1.05	1.03	13.56 13.19
	Z1 (PU):	0.35784		TOT3:	1.00	1.00	12.94 12.87
	Z2 (PU):	0.35784		TOT5:	1.00	1.00	12.94 12.87
	Z0 (PU):	0.38166		TOT8:	1.00	1.00	12.94 12.87
B-WHP	3P Duty:	11.65	3.3	SYM2:	1.00	1.00	11.65 11.02
	VOLTS: 12470.0 SLG:	11.02	2.2	SYM3:	1.00	1.00	11.65 11.02
	NACD: 1.000 LN/LN:	10.09		SYM5:	1.00	1.00	11.65 11.02
	LN/LN/GND:	12.33		SYM8:	1.00	1.00	11.65 11.02
	GND RETURN:	10.32		TOT2:	1.03	1.02	12.02 11.22
	Z1 (PU):	0.39727		TOT3:	1.00	1.00	11.65 11.02
	Z2 (PU):	0.39727		TOT5:	1.00	1.00	11.65 11.02
	Z0 (PU):	0.48157		TOT8:	1.00	1.00	11.65 11.02
B-XSB-TX DS	3P Duty:	6.66	0.8	SYM2:	1.00	1.00	6.66 5.61
	VOLTS: 12470.0 SLG:	5.61	0.7	SYM3:	1.00	1.00	6.66 5.61
	NACD: 1.000 LN/LN:	5.76		SYM5:	1.00	1.00	6.66 5.61
	LN/LN/GND:	6.53		SYM8:	1.00	1.00	6.66 5.61
	GND RETURN:	4.83		TOT2:	1.00	1.00	6.66 5.61
	Z1 (PU):	0.69567		TOT3:	1.00	1.00	6.66 5.61
	Z2 (PU):	0.69567		TOT5:	1.00	1.00	6.66 5.61
	Z0 (PU):	1.09475		TOT8:	1.00	1.00	6.66 5.61

I N T E R R U P T I N G D U T Y S U M M A R Y R E P O R T

PRE FAULT VOLTAGE: 1.0000
 MODEL TRANSFORMER TAPS: NO
 NACD OPTION: INTERPOLATED

BUS RECORD NO NAME	VOLTAGE L-L	NACD RATIO	* 3 P H A S E * E/Z KA	X/R	* * * S L G * * * E/Z KA	X/R
B-CH	12470.	1.000	11.029	2.96	10.204	2.14
B-CH ATS	12470.	1.000	11.037	2.96	10.213	2.14
B-CH CHLR	12470.	1.000	10.910	2.84	10.050	2.07
B-CH CHLR DS	12470.	1.000	10.968	2.90	10.125	2.11
B-CH-NW USB DS	12470.	1.000	10.352	2.23	9.357	1.71
B-CH-SUB 4A DS	12470.	1.000	10.593	2.67	9.657	2.00
B-LE USB DS	12470.	1.000	10.362	2.26	9.370	1.73
B-LH-TX DS	12470.	1.000	8.942	1.20	7.801	0.96
B-ML	12470.	1.000	11.171	2.59	10.364	1.88
B-NH EAST	12470.	1.000	9.688	1.81	8.592	1.44
B-NH WEST	12470.	1.000	9.901	1.93	8.831	1.51
B-PS1-TX DS	12470.	1.000	9.488	1.77	8.370	1.42
B-PS2-TX DS	12470.	1.000	10.465	2.32	9.493	1.76
B-PSC	12470.	1.000	11.575	3.12	10.907	2.17
B-SB1	12470.	1.000	12.070	3.15	11.562	2.13
B-SMC	12470.	1.000	10.465	2.32	9.493	1.76
B-SMC 2ND USB DS	12470.	1.000	10.406	2.29	9.423	1.74
B-SRTC-SB2	12470.	1.000	12.734	4.16	12.546	2.59
B-SRTC-SWBD4	4160.	1.000	3.546	6.18	3.657	6.29
B-SRTC-SWBD4 DS	12470.	1.000	12.633	4.04	12.395	2.54
B-SRTC-USB1 PREF	12470.	1.000	12.649	5.00	10.379	2.06
B-SRTC-USB2 ALT	12470.	1.000	12.938	4.63	12.870	2.78
B-WHP	12470.	1.000	11.654	3.25	11.017	2.25
B-XSB-TX DS	12470.	1.000	6.655	0.79	5.607	0.67

52 FAULTED BUSES, 99 BRANCHES, 2 CONTRIBUTIONS
 UNBALANCED FAULTS REQUESTED

*** SHORT CIRCUIT STUDY COMPLETE ***

C. APPENDIX C – UTILITY CORRESPONDENCE

See email from Mr. Tom Riddle with Portland General Electric stating available fault current and source impedance information on the attached sheets.

Moore, Matthew A

From: Moore, Matthew A
Sent: Wednesday, February 20, 2013 1:19 PM
To: Moore, Matthew A
Subject: West Loop Util Info

From: **Thomas Riddle** <Tom.Riddle@pgn.com>
Date: Wed, Jan 16, 2013 at 11:35 AM
Subject: FW: Request for Information - PSU Arc Flash
To: "Quinn Soifer (soiferq@pdx.edu)" <soiferq@pdx.edu>

Hi Quinn,

Here is the information for Eaton's question 1&3. As I stated in my e-mail yesterday the Market Center Building is in PP&L's territory, as also confirmed by PGE engineering.

1) Values haven't significantly changed.

PSU Science II BLDG	12.47KV Primary Fault Current & System Impedance					
	3- Phase Fault Current	Line-to- Ground Fault Current	R1 (Ω)	X1 (Ω)	R0 (Ω)	X0 (Ω)
Preferred Source (Switch 1815)	12,649	10,379	0.1117	0.5581	0.6837	0.7567
Alt Source (Switch 1998)	12,937	12,870	0.1175	0.5439	0.3328	0.4914

2) Confirmed – 1600 SW 4th PP&L service territory.

3) Recommend Eaton/PSU field verify or make assumptions.

If needed, we would gladly meet with you and Eaton to discuss this information and as engineering mentioned in question #3, they would recommend field verification.

Thanks Quinn, and I hope this information answers the questions. If a meeting is needed, or you feel field verification is required, please work through me and I will set it up.

Tom Riddle

Key Customer Manager

Portland General Electric

121 SW Salmon Street

3WTCBR07

Portland, Oregon 97201

Office: [503-464-7637](tel:503-464-7637)

Cell: [503-969-9344](tel:503-969-9344)

tom.riddle@pgn.com

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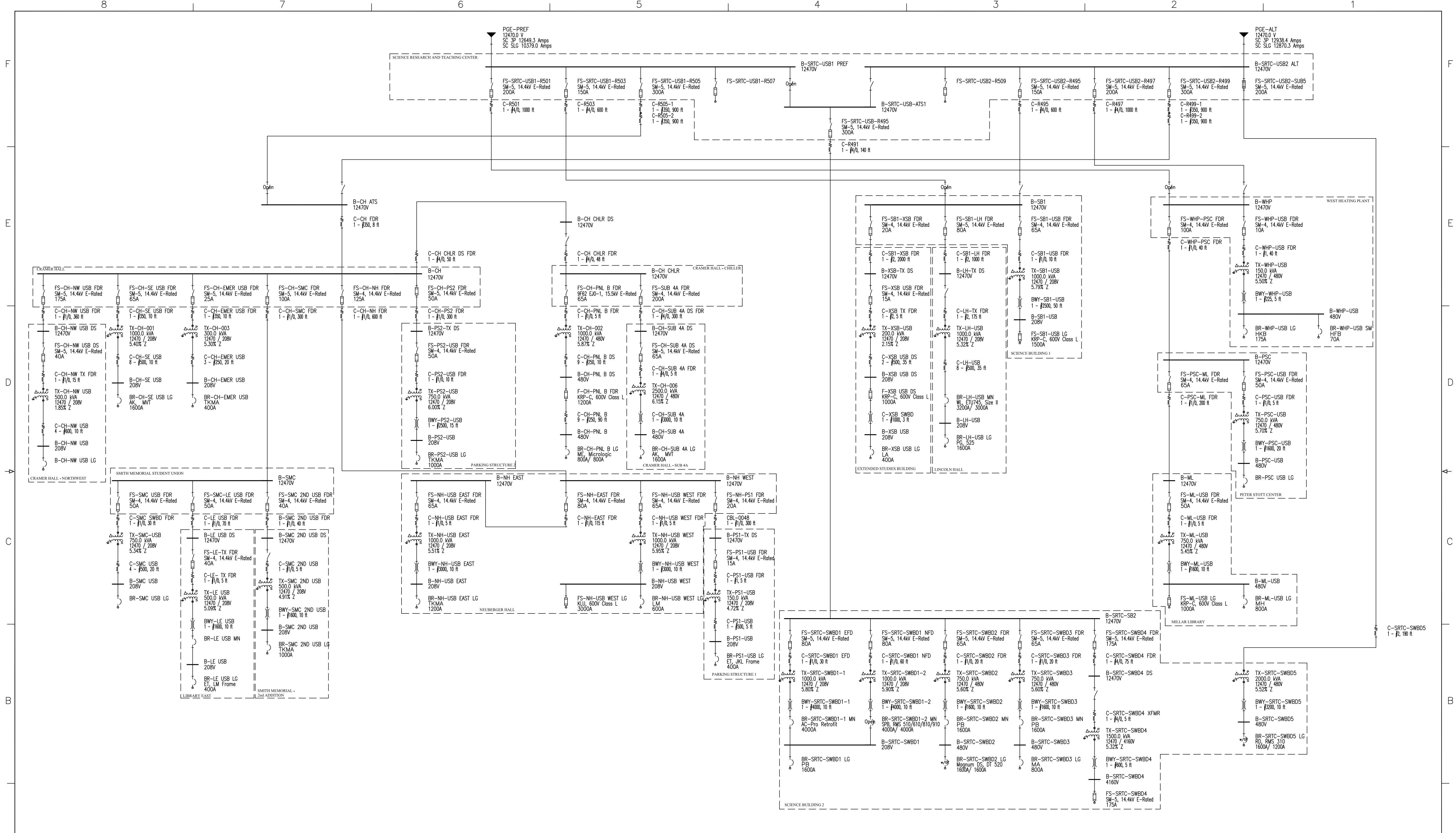
Quinn Soifer, P.E.
Facilities Engineer

soiferq@pdx.edu

503-725-4316

D. APPENDIX D – ONE-LINE DIAGRAM

See power system study one-line diagram on the attached sheet.



01	REVISION	THE INFORMATION ON THIS DOCUMENT WAS CREATED BY EATON ELECTRICAL. IT WAS DISCLOSED IN CONFIDENCE AND IS ONLY TO BE USED FOR THE PURPOSE IN WHICH IT WAS SUPPLIED.		DFTR	MAM	DATE	2-20-13	EATON Electrical Services & Systems	
				ENGR	MAM	DATE	2-20-13	TITLE PORTLAND STATE UNIVERSITY WEST CAMPUS LOOP	
				SCALE	NONE		TYPE POWER SYSTEM STUDY		ONE LINE
		CAD FILENAME	PRODUCT CODE	REVISION			G.O.	DWG	SHEET
		SSF-0269	U0160	01			ESE0008353	SSF-0269	1 OF 01